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LIBRO II – ANEJO Nº 16 RED DE ALCANTARILLADO

Hoja de control de calidad

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1. Introducción y configuración general

El presente documento recoge los cálculos justificativos de la estrategia de drenaje propuesta para el proyecto de urbanización del sector Grao. La actuación de urbanización incluye la construcción de múltiples elementos, incluyendo viales, rotondas, nuevas zonas verdes, aparcamientos, entre otros. La propuesta establece una estrategia de drenaje basada en la utilización mixta de drenaje convencional y Sistemas Urbanos de Drenaje Sostenible en los espacios que lo permiten, siguiendo de este modo las directrices impulsadas por la Guía Básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de Valencia.

La siguiente figura muestra la geometría en planta de la actuación, que limita al norte con la calle Juan Verdeguer, al oeste las vías de ADIF y con la avenida de Francia, y al este con Av. Ing. Manuel Soto.

Figura 1. Planta de la actuación propuesta.

La estrategia de drenaje de aguas pluviales propuesta pretende paliar los problemas que se plantean hoy en día en el drenaje urbano, donde el avance de la urbanización y, en consecuencia, de la impermeabilización del suelo, están teniendo importantes efectos en el ciclo hidrológico natural. La desaparición de la vegetación y el sellado del terreno provocan un aumento de los volúmenes de escorrentía, acompañado de un aumento de los caudales pico y una reducción del tiempo de respuesta hidrológico.

Esta circunstancia, acompañada del actual contexto de cambio climático, donde las precipitaciones extremas son cada vez más recurrentes, está causando que se requieran infraestructuras de drenaje cada vez de mayores dimensiones, y que se produzcan importantes vertidos que pueden tener consecuencias en los medios receptores.

En este contexto, se presentan los Sistemas Urbanos de Drenaje Sostenible (SUDS), que son sistemas de drenaje alternativos concebidos como complemento a los tradicionales que, a diferencia de estos, permiten la gestión en origen de la escorrentía urbana replicando los procesos hidrológicos naturales, y quedando integrados en el paisaje urbano. Esta actuación en origen, infiltrando, evapotranspirando o almacenando tanta agua de lluvia como sea posible, permite gestionar el volumen o caudal de escorrentía antes de que llegue a suponer un problema.

Además, buscan beneficios a nivel social, económico y de la biodiversidad, adquiriendo una dimensión poliédrica y multidisciplinar.

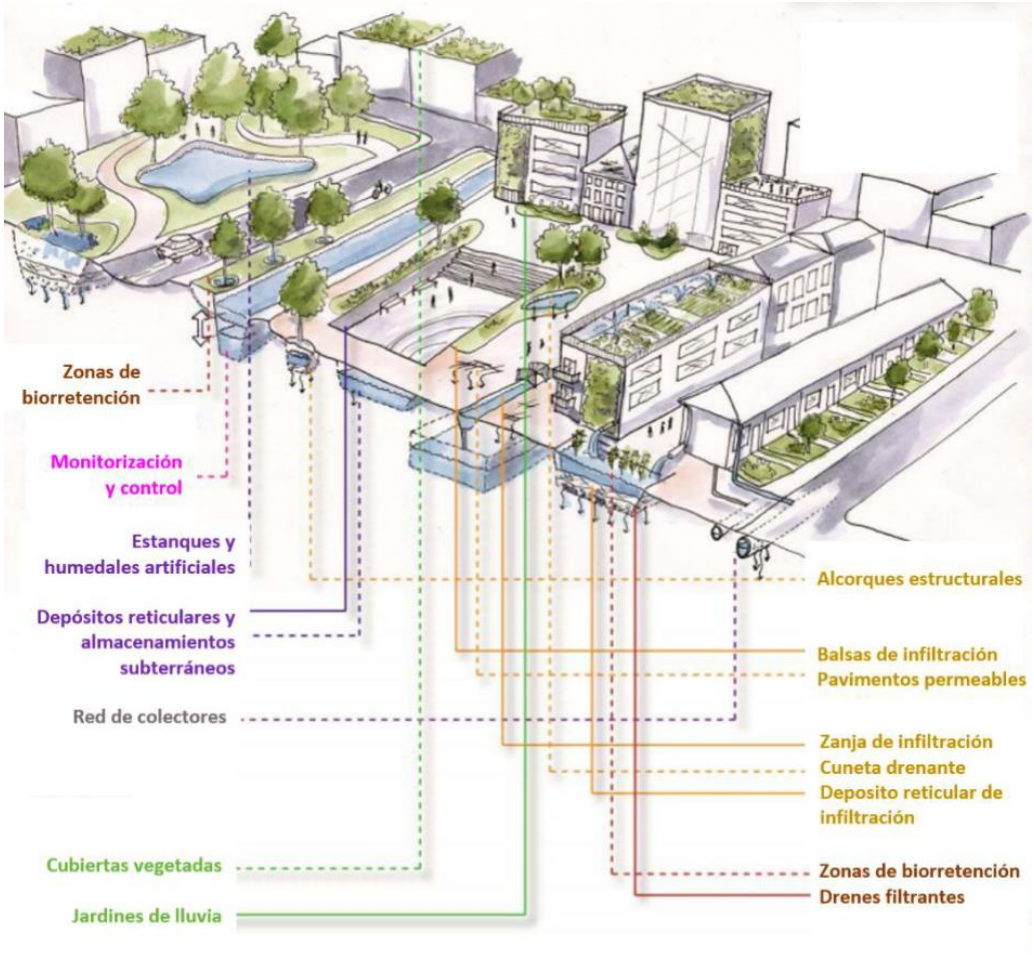


Figura 2. SUDS integrados en la ciudad. Fuente: Guía Básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de Valencia.

De este modo, desde el punto de vista hidrológico, los SUDS persiguen tres objetivos fundamentales:

- Reducir los volúmenes totales de escorrentía vertidos mediante la infiltración, la evapotranspiración o el almacenamiento para otros usos.
- Mejorar la calidad de las escorrentías proporcionando tratamiento a través de la fitorremediación y/o la filtración (procesos biológicos y físicos).
- Laminar los caudales pico para evitar la sobrecarga de las redes, gracias al almacenamiento temporal en espacios superficiales o subterráneos.

2. Antecedentes

2.1. Contexto normativo

2.1.1. Directiva (UE) 2024/3019 sobre tratamiento de las aguas residuales urbanas

La directiva europea del 27 de Noviembre de 2024 establece las siguientes ideas al respecto de la utilización de infraestructura verde y azul (SUDS) en detrimento de la infraestructura gris (drenaje convencional):

> *"Dada la preferencia por las infraestructuras e inversiones verdes y azules, la construcción de nuevas infraestructuras grises solo debe contemplarse cuando sea absolutamente necesario. [...] Se prevé que tales desbordamientos y escorrentías aumenten debido a los efectos combinados de la urbanización y el cambio progresivo del régimen de lluvias vinculado al cambio climático. [...] Las soluciones para reducir esta fuente de contaminación deben definirse a nivel local, teniendo en cuenta las condiciones locales específicas"*

2.1.2. Reglamento del Dominio Público Hidráulico

La última actualización del Reglamento del Dominio Público Hidráulico (RDPH), realizada en el Real Decreto 665/2023, destaca que:

> *"La actividad urbanizadora es una de las actuaciones antrópicas más impactantes sobre el DPH, puesto que la impermeabilización del terreno y las actividades urbanas, entre otras presiones, tienen un relevante impacto sobre el ciclo hidrológico, de forma que el agua de lluvia en los entornos urbanos que llega al terreno debe protegerse, evitando su contaminación [...]".*

Por ello, en **se incentiva la utilización de SUDS**, fomentándolos como principal estrategia de gestión en origen de la escorrentía pluvial. Además, incluye mención y definición específica de estos sistemas:

> "*Son elementos superficiales, permeables, preferiblemente vegetados, integrantes de la estructura urbana-hidrológica-paisajística y previos al sistema de saneamiento. Están destinados a filtrar, retener, transportar, acumular, reutilizar e infiltrar al terreno el agua de lluvia, de forma que no degraden e incluso restauren la calidad del agua que gestionan."*

De manera concreta, **la inclusión de SUDS es requerida** por el RDPH, que en su Art. 126.ter. punto 7 especifica que:

> "*Las nuevas urbanizaciones, polígonos industriales y desarrollos urbanísticos en general, deberán introducir sistemas de drenaje sostenible, tales como superficies y acabados permeables, de forma que el eventual incremento del riesgo de inundación se mitigue. A tal efecto, el expediente del desarrollo urbanístico deberá incluir un estudio hidrológico-hidráulico que lo justifique."*

En cuanto a criterios de diseño, el RDPH en su Anexo XI, Punto 5.2, identifica la precipitación diaria asociada al percentil 80 como un primer umbral para evaluar el rendimiento de un sistema:

> "*Por tal motivo se establece como precipitación de cálculo indicativa para el análisis del rendimiento hidráulico del sistema de saneamiento la precipitación diaria en la serie de estudio no superada el 80% de los días en que la precipitación es superior a 1 mm ($P_{d,80\%}$), y se obtendrá a partir de los datos*

reales y estudios pluviométricos existentes con series diarias obtenidos de la Agencia Estatal de Meteorología (AEMET), de los Sistemas Automáticos de Información Hidrológica (SAIH) de los organismos de cuenca y de otras fuentes de datos de precipitaciones existentes."

Por último, en el Artículo 259 quinquies, se establecen una serie de medidas a disponer para cumplir con determinados objetivos de rendimiento hidráulico:

"Medidas preventivas destinadas a evitar la entrada de la escorrentía urbana en los sistemas colectores, incluidas las medidas de fomento de la retención natural del agua o de la recogida de aguas pluviales, y las medidas de aumento de los espacios verdes o de limitación de las superficies impermeables en las aglomeraciones."

"Otras medidas adicionales, [...] priorizando los sistemas urbanos de drenaje sostenible, tales como cubiertas ecológicas, jardines verticales, pavimentos permeables, jardines de lluvia, sumideros filtrantes y canales permeables, favoreciendo así la biodiversidad."

2.1.3. Ordenanza de saneamiento de la ciudad de Valencia

La Ordenanza de saneamiento de la ciudad de Valencia, redactada en 2015, indica lo siguiente en cuanto al diseño de pluviales:

"El caudal de diseño necesario para el dimensionamiento de un tramo de colector depende del tipo de red en el que se encuentre: pluviales, residuales o unitaria. Para colectores de pluviales y unitarios se utilizará el caudal de diseño de aguas pluviales correspondiente a una precipitación de 25 años de período de retorno y, por tanto, será necesario un estudio hidrológico [...]."

El nivel de protección adoptado para las aguas pluviales es el correspondiente a un periodo de retorno de 25 años. La razón fundamental de este valor, que podría considerarse elevado para una red de drenaje urbano, es la especial característica de los chubascos extremos mediterráneos, con muy bajas intensidades para bajos periodos de retorno, pero muy altas para periodos de retorno medios y altos. Un diseño con un nivel de riesgo tradicional produciría demasiado frecuentemente graves insuficiencias en la red.

Asimismo, la Ordenanza indica que se fomentarán los SUDS para la gestión de aguas pluviales e insta a que se utilicen en ámbitos de nueva urbanización y en zonas de poca densidad de edificación dentro de su apartado 2.5 "Uso de Sistemas de Drenaje Sostenible":

"De acuerdo con la normativa vigente en la Comunitat Valenciana sobre prevención del riesgo de inundación, se fomentará el uso de Sistemas de Drenaje Sostenible para la gestión del drenaje de aguas pluviales. Por lo tanto, la presente normativa insta a que se utilicen este tipo de soluciones en ámbitos de nueva urbanización y en zonas de poca densidad de edificación como por ejemplo las pedanías de la ciudad.

Los nuevos proyectos de urbanización incorporarán, en la medida de lo posible, medidas para fomentar la infiltración en las superficies de los aparcamientos, viales, centro de glorietas, medianas ajardinadas, alcorques y jardines. Se propone en ese sentido el uso de soluciones como los

pavimentos permeables o el rebaje de los bordillos de las aceras en aquellas situaciones en que se pueda redirigir la escorrentía superficial hacia zonas donde se facilite su infiltración (alcorques, zonas verdes, etc.) sin perjuicio del uso de todas aquellas soluciones que se engloban en este conjunto de técnicas."

2.1.4. Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València

La *Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València*, disponible para descarga libre, además de realizar una introducción al drenaje sostenible, resume las características más relevantes de las distintas tipologías de SUDS y propone criterios de diseño específicos que tienen en cuenta los condicionantes particulares de la ciudad de Valencia.

En la guía se establecen unos criterios de dimensionamiento de SUDS en base a la tipología urbana. Para actuaciones de tipo edificación abierta y grandes vías con medianas ajardinadas, la guía indica que los SUDS deben dimensionarse con un volumen mínimo equivalente al V_{80} (consultar apartado 3.2.3). Este criterio quedaría también alineado con las pautas marcadas por el Reglamento del Dominio Público Hidráulico.

Figura 3. Portada de la Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València.

2.1.5. Borrador de la Guía para la elaboración de Planes Integrales de Gestión del Sistema de Saneamiento

Esta guía, de próxima publicación, sirve como soporte del RDPH en la elaboración de los Planes Integrales de Gestión del Sistema de Saneamiento. En este ámbito, la guía indica en su introducción:

> *"Así, en los nuevos desarrollos, el sistema en su conjunto bien sea separativo o unitario, debe presentar un volumen de almacenamiento suficiente para limitar los caudales de escorrentía vertidos fuera del ámbito de actuación para las precipitaciones de diseño (cuyos periodos de retorno suelen comprenderse entre los 10 y los 25 años en España [...])".*

Del mismo modo, relativo al cálculo del rendimiento hidráulico, la guía indica lo siguiente:

> *"Las aguas de escorrentía pluvial asociadas a los entornos urbanos deben ser objeto de protección en sí mismas, evitando en la medida de lo posible su contaminación y primando el respeto al ciclo hidrológico natural. Se priorizarán las medidas preventivas frente a las correctivas, actuando en origen con el empleo de técnicas de drenaje urbano sostenible e infraestructuras verdes, fomentando el tratamiento en origen de la escorrentía pluvial y su infiltración, además de fomentar el aprovechamiento de aguas pluviales y la reutilización de las aguas grises".*

2.1.6. Autorización de vertidos de aguas pluviales en cauces de la CHJ

La Confederación Hidrográfica del Júcar, para la solicitud de autorización de vertidos de aguas pluviales en cauces de Dominio Público Hidráulico, indica que:

> *"Para nuevas urbanizaciones, polígonos industriales y desarrollos urbanísticos en general, deberá tener en cuenta que:*
>
> > *Se deberán introducir sistemas de drenaje sostenibles (SUDS), tales como superficies y acabados permeables, de forma que el eventual incremento del riesgo de inundación se mitigue. A tal efecto, el expediente del desarrollo urbanístico deberá incluir un estudio hidrológico-hidráulico que lo justifique (Art. 126. Ter. Punto 7 del Reglamento del Dominio Público Hidráulico).*
> >
> > *A este respecto deberán introducir la utilización de SUDS y/o balsas/tanques de tormentas para laminar la avenida asociada a T = 15 años sin que varie el hidrograma del cauce aguas abajo del punto de vertido. Es decir, que no se vea afectado el caudal pico circulante por el cauce donde se vierta, en comparación con la situación de la zona natural (no urbanizada), debiendo justificarlo mediante un Estudio hidrológico-hidráulico, en el que se recoja, al menos, planos de la cuenca de aporte y de la cuenca hidrográfica del cauce afectado, cálculo del caudal de aguas pluviales a verter, y justificación del diámetro de tubería adoptado (el diámetro de las conducciones de vertido de aguas pluviales al cauce no deberá sobredimensionarse).*
> >
> > *Dicho estudio deberá contener un comparativo que justifique que no se varía el hidrograma del cauce aguas abajo del punto de vertido para la avenida asociada a T = 15 años."*

2.2. Descripción de la infraestructura de saneamiento existente

Actualmente, en el ámbito del proyecto existe una red de drenaje independiente con la finalidad de dar servicio al antiguo circuito de fórmula uno.

La red cuenta con varios tramos de colectores con la finalidad de resolver el problema de drenaje superficial de la pista como de la zona de paddocks y aparcamientos.

La red existente no cumple las necesidades propias del nuevo proyecto urbanístico a desarrollarse en un futuro y cuyas obras de urbanización se definen en este proyecto.

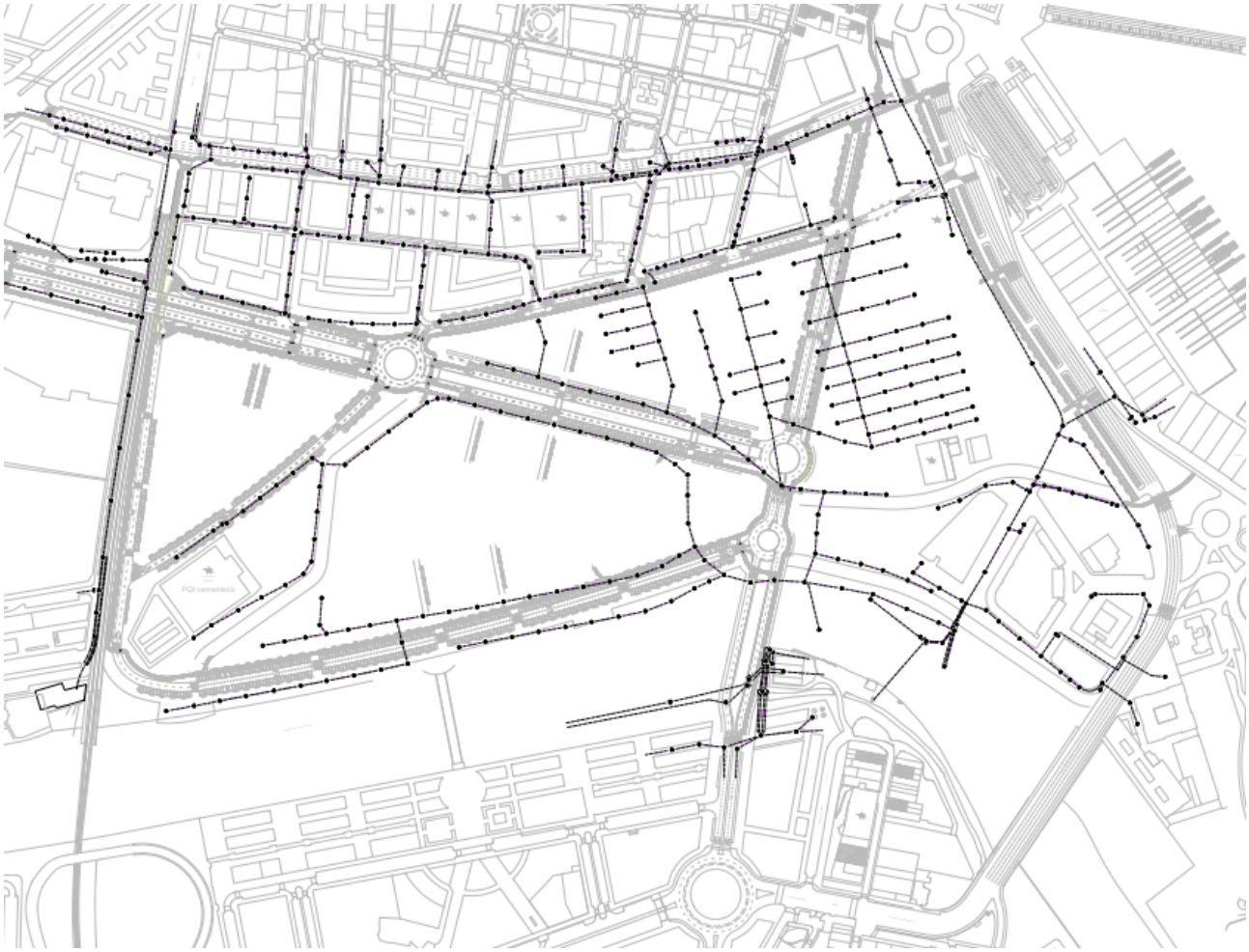


Figura 4. Planta de situación de las redes existentes tanto dentro del ámbito como en su entorno.

2.3. Hidrogeología y geotecnia

Dada la propuesta de implementación de SUDS y la posibilidad de promover la infiltración en el ámbito de la urbanización se examina la información analizada en el estudio geológico-geotécnico, como punto de partida para el estudio de la permeabilidad y del nivel freático en el área. Para más información, referir al Estudio Geotécnico.

En general, en el futuro sector urbano del Grao, predominan materiales de tipo limoso, depositados en la llanura de inundación del río, entre los que aparecen intercalados niveles de arena y grava, que señalan las sucesivas posiciones de los canales del río. Otros niveles arenosos constituyen barras paralelas a antiguas líneas de costa que se forman en la desembocadura.

Se consideran seis estratos conformados por:

- Formación R: Rellenos antrópicos
- Formación A: Arcillas limosas negras
- Formación B: Arenas grisáceas
- Formación C: Arcillas limosas y limos arcillosos marrones.

- Formación D: Arenas limosas con niveles de grava
- Formación E: Gravas en matriz arenosa.

Las investigaciones realizadas conllevan seis campañas de ensayos diferentes, mostradas en diferentes colores, que se pueden observar en la siguiente figura. Los sondeos y las calicatas se discretizan por medio de un círculo y un cuadrado respectivamente, separados en cuatro cuadrantes.

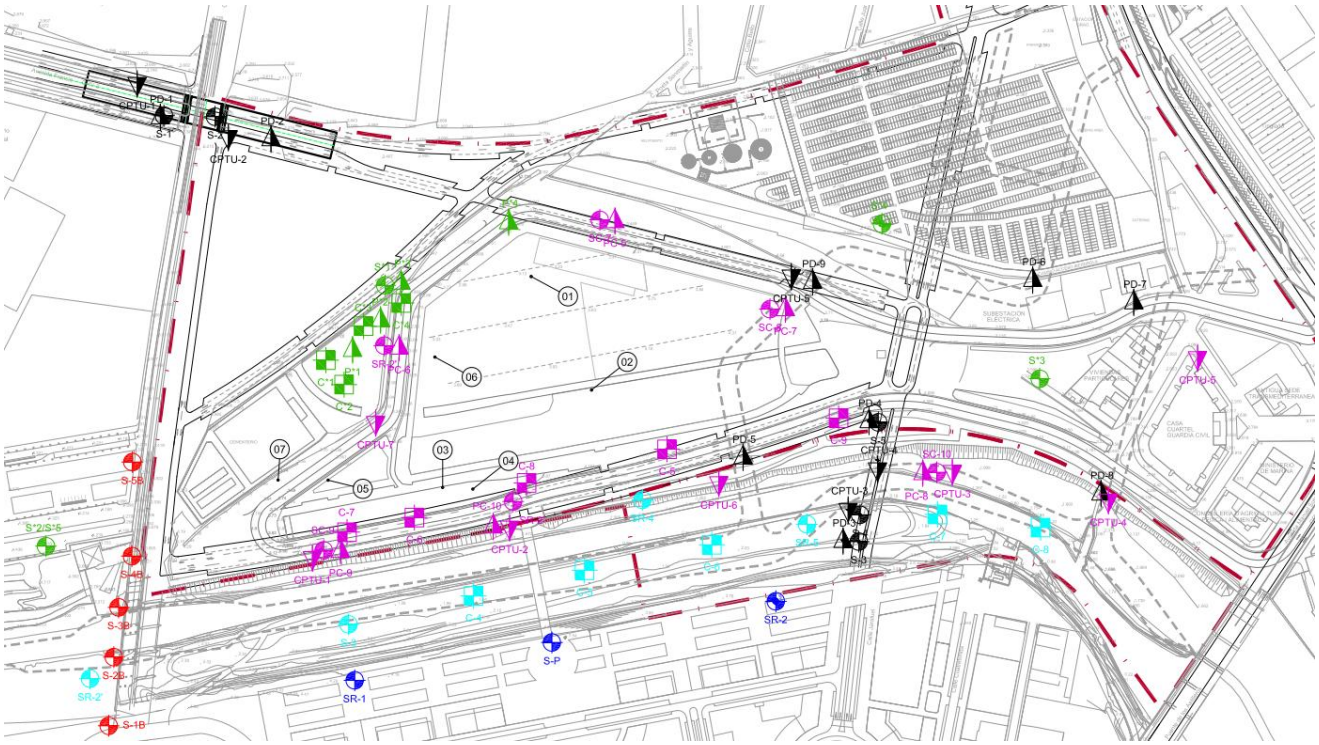


Figura 5. Planta de situación de la investigación geológico-geotécnica. Fuente: Estudio Geotécnico.

Las primeras calicatas realizadas (2007, verde) muestran una grava mal graduada, en general en matriz arcillosa limosa, hasta unos 0,5-1,0 m de profundidad; mientras que las calicatas realizadas en septiembre de 2007 (rosa); muestran rellenos en torno a 2,0 m de gravas y limos de color marrón y baja plasticidad. En capas inferiores se detecta la formación A de arcillas limosas y cierto grado de contaminación por hidrocarburos.

En cuanto a la presencia de nivel freático, se detecta la presencia de nivel freático en tres sondeos, variando entre 1,5 m de profundidad en la zona de las Moreras, y alrededor de 3,0 m en los sondeos ubicados en el entorno de la avenida de Francia.

El análisis continuo del nivel freático a lo largo de un período de tres meses, en tres sondeos situados a la altura del futuro puente sobre las vías del tren y en margen izquierda del río, muestran un nivel de agua entre las cotas absolutas +0,00 m y +1,00 m, que se corresponde con lo observado en la bibliografía.

2.4. Hidrología e inundabilidad

También es importante conocer si el ámbito de estudio se encuentra en una zona con riesgo de inundación fluvial, dada su proximidad al antiguo cauce del río Turia.

De acuerdo con el Sistema Nacional de Cartografía de Zonas Inundables (SNCZI) del Ministerio de Transición Ecológica y Reto Demográfico, las zonas con peligrosidad de inundación fluvial para el periodo de retorno de hasta 100 años son gestionadas por el nuevo cauce del río Turia. En cambio, para el periodo de retorno de 500 años, parte del antiguo cauce del río Turia se inunda; no obstante, la zona de estudio queda fuera de la mancha de inundación (Figura 6).

Cabe destacar que esta zona será sometida a un futuro desarrollo que se espera mantenga o mejore las condiciones de inundabilidad que el SNCZI indica.

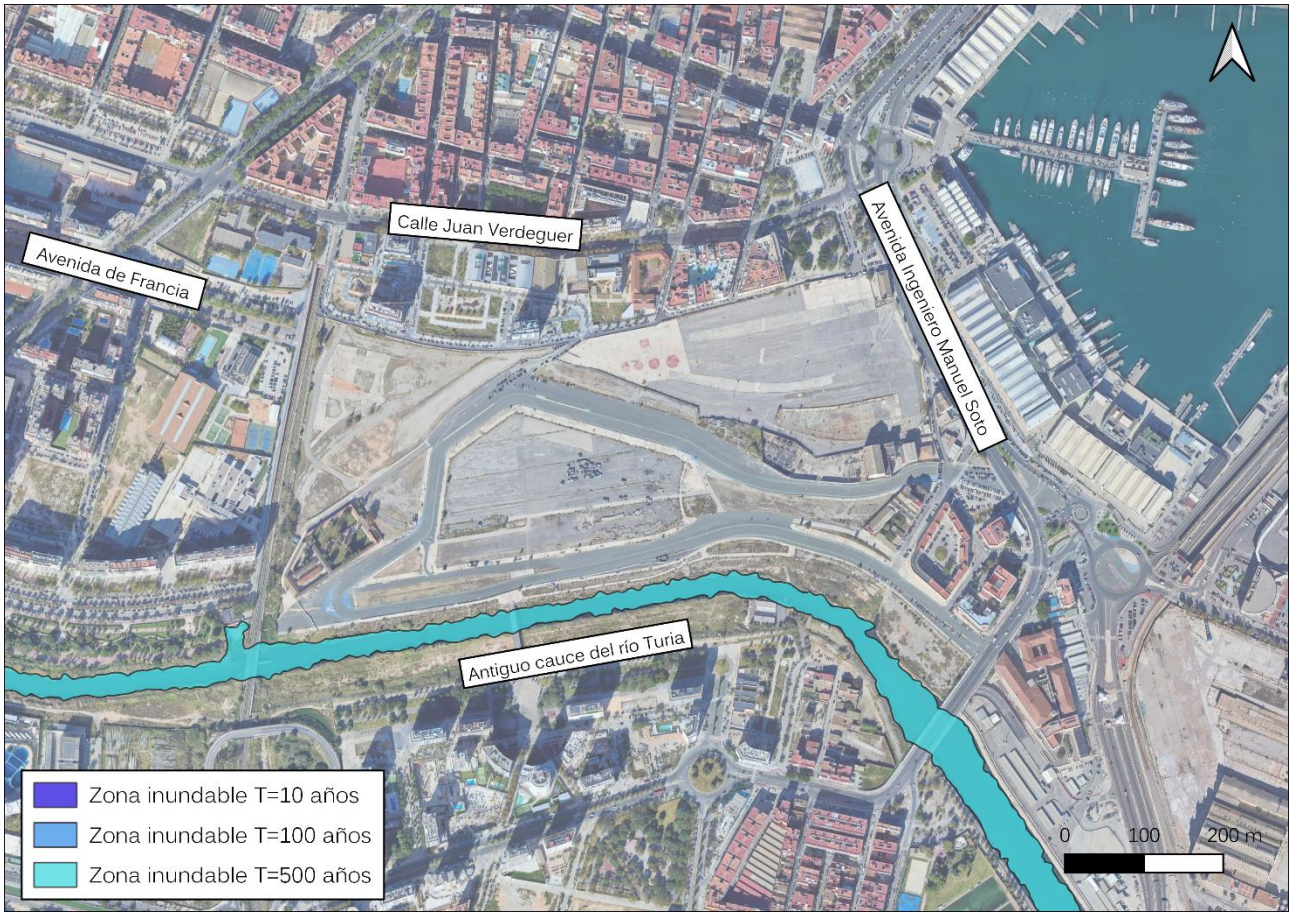


Figura 6. Zonas con peligrosidad de inundación fluvial para distintos períodos de retorno en el sector Grao.

3. Criterios y Parámetros de Diseño

3.1. Selección de los criterios de diseño

Para el dimensionamiento hidráulico del sistema de colectores, la Ordenanza Municipal y Normativa para obras de Saneamiento de la ciudad de Valencia, propone tres operaciones: conocer el caudal de diseño, dimensionar los colectores para dicho caudal y comprobar las velocidades de circulación máximas y mínimas, y la línea de energía.

En el caso de colectores pluviales y unitarios, se empleará un caudal de diseño correspondiente a una precipitación de 25 años de período de retorno.

3.2. Selección de datos pluviométricos

El conocimiento de la pluviometría local constituye una pieza fundamental para poder optimizar los diseños. Valencia presenta un clima mediterráneo típico (Csa, según la clasificación climática de Köppen), con inviernos suaves y veranos calurosos. Las precipitaciones se distribuyen de manera irregular a lo largo del año, concentrándose especialmente entre septiembre y mayo. En cuanto a los acumulados anuales, en promedio, tienden a estar próximos a los 450 mm.

3.2.1. Curva IDF

La Ordenanza Municipal y Normativa para obras de Saneamiento de la ciudad de Valencia propone una curva IDF para período de retorno 25 años, a emplear en la Ciudad de Valencia, que presenta la siguiente expresión:

$$I = 157{,}2 - 2{,}645 \cdot d + 0{,}02662 \cdot d^2 - 0{,}0001122 \cdot d^3$$

Donde:

- d: duración de la lluvia en minutos.
- I: intensidad de la lluvia en mm/h.

Cabe destacar que dicha normativa establece que "sólo es recomendable su utilización para duraciones entre 10 y 99 minutos. Si el tiempo de concentración fuese inferior a 10 minutos se adoptará como duración de la lluvia la de 10 minutos. En caso contrario, la duración es la del tiempo de concentración".

3.2.2. Lluvias de diseño para drenaje

La distribución temporal de la lluvia se ha llevado a cabo según el método de los bloques alternos, cuya hipótesis fundamental es asumir, para cualquier intervalo de tiempo, la intensidad media más desfavorable. El proceso de cálculo de la tormenta por bloques alternos, para un periodo de retorno determinado se describe a continuación.

En primer lugar, se fijan n intervalos de tiempo de duración Δt, de manera que la duración total de la tormenta sea igual a n Δt. Seguidamente, se obtienen, a partir de la curva IDF empleada, las intensidades de precipitación correspondientes a cada una de las duraciones, i(KΔt).

El valor de intensidad correspondiente a cada uno de los n bloques que conforman la tormenta se define de la siguiente forma:

$$b_1 = i(\Delta t), \ldots, \frac{b_1 + b_2}{2} = i(2\Delta t), \ldots, \frac{\sum_{j=1}^{k-1} b_j}{k} = i(k\Delta t)$$

Por lo que despejando la intensidad correspondiente a un bloque k, resulta:

$$b_k = ki(k\Delta t) - \sum_{j=1}^{k-1} b_j$$

Finalmente, los bloques se reordenan en una secuencia temporal de manera que la intensidad máxima ocurra en el centro de la tormenta y que los demás bloques queden en orden de intensidad decreciente alternativamente a derecha e izquierda del bloque central. Para reproducir el "efecto pared" típico de las tormentas torrenciales mediterráneas, la distribución de los bloques será tal que la rama ascendente del hietograma sea más pronunciada que la descendente.

La duración de la tormenta se ha establecido en 18 horas, y el intervalo Δt se toma de 10 minutos, inferior al tiempo de concentración de la cuenca considerada. El hietograma resultante es el que se recoge en la siguiente figura, habiendo sido suavizado los bloques mediante splines de orden 2. Esta tormenta es por tanto el input directo de precipitación en el modelo Infoworks.

t(h)	I(mm/h)	P(mm)
0.17	109.64	18.3
0.33	91.52	30.5
0.50	78.66	39.3
0.67	69.04	46.0
0.83	61.57	51.3
1.00	55.60	55.6
1.17	50.71	59.2
1.33	46.63	62.2
1.50	43.18	64.8
1.67	40.21	67.0
1.83	37.64	69.0
2.00	35.38	70.8
2.17	33.39	72.3
2.33	31.62	73.8
2.50	30.03	75.1
2.67	28.59	76.2
2.83	27.29	77.3
3.00	26.11	78.3

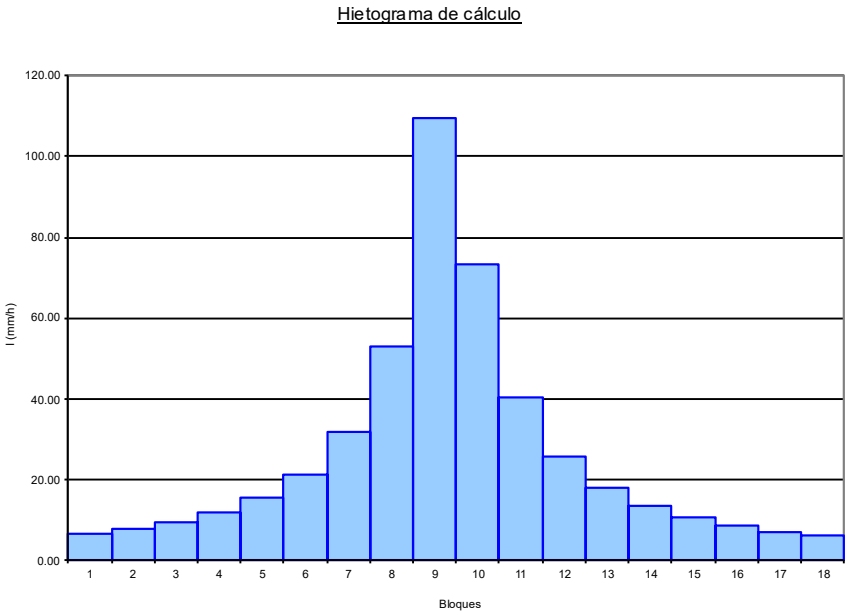


Figura 7. Resultado de la determinación del hietograma de cálculo..

3.2.3. Lluvias de diseño para la modelización de SUDS

Para la modelización de SUDS, es habitual el empleo de lluvias uniformes con hietograma rectangular, es decir, cuya intensidad se mantiene constante durante la duración de la tormenta. De este modo, se obtiene la siguiente tabla de eventos de diseño, donde se incluye intensidad, duración y volumen de escorrentía generado:

Tabla 1. Curvas IDF de acuerdo con la Ordenanza Municipal.

Tiempo (min)	10	15	20	30	45	60	75	90
Intensidad (mm/h)	133,3	123,1	114,1	98,8	81,9	70,1	61,2	53
Volumen (mm)	22,2	30,8	38	49,4	61,4	70,1	76,5	79,5

3.2.4. Percentiles volumétricos de precipitación

En el diseño de SUDS, tal y como se detallará más adelante, es habitual emplear los percentiles volumétricos de precipitación para realizar un diseño preliminar. Estos percentiles establecen un umbral de precipitación que no es superado por un determinado porcentaje de los días lluviosos de un año. Por ejemplo, el V_{80} define un volumen de precipitación tal que, por promedio estadístico, no es superado en el 80 % de los días lluviosos de un año tipo.

A partir de la información pluviométrica de las distintas estaciones pluviométricas del Ciclo Integral del Agua, la Guía Básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de Valencia establece los siguientes volúmenes de precipitación diaria acumulada para los percentiles más relevantes, destacándose en negrita en la Tabla 2 el percentil V_{80}, que constituirá uno de los pilares de los criterios de diseño, como se detallará más adelante.

Tabla 2. Percentiles de precipitación para la ciudad de Valencia.
Fuente: Guía Básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de Valencia.

ESTACIÓN	V_{98}	V_{95}	V_{90}	V_{85}	V_{80}	V_{75}	V_{70}	V_{60}
Valor promedio	116	60	37	27	20	16	12	8

Por otro lado, se ha estudiado el percentil correspondiente al caudal natural para T25, esto es, el volumen de retención necesario, para reducir los caudales resultantes desde una situación parcial o completamente impermeable (actual y futura) hasta una solución similar a la existente antes de la urbanización (zona verde y/o permeable).

Para ello, tomando la intensidad de lluvia máxima de la curva IDF indicada en la ordenanza y aplicándole un multiplicador en función de la diferencia de coeficientes de escorrentía, obtenemos un percentil asociado al caudal natural de 70 mm.

3.3. Selección de criterios de diseño de SUDS

3.3.1. Control de cantidad

Uno de los aspectos claves en la definición de la estrategia de drenaje consiste en establecer las limitaciones que se impondrán a los vertidos fuera del ámbito.

De acuerdo con el estudio y análisis realizado en el apartado 2.3, se descarta la infiltración debido a la pobre calidad de los suelos existentes (rellenos, estratos arcillosos limosos muy impermeables, y cierta presencia de contaminación en capas inferiores), y por ello, se propone la laminación como medida para gestionar los caudales punta de los eventos lluviosos.

De este modo, se buscará retener en los SUDS, el mayor volumen de escorrentía posible para así limitar al máximo posible los vertidos y tener el menor impacto en el medio receptor, siguiendo la siguiente jerarquía de drenaje:

1. Descarga al canal del antiguo cauce.
2. Descarga a la red de saneamiento unitaria municipal.

Para los vertidos al cauce, se tratará de laminar y tratar en origen las escorrentías asociadas; mientras que en las descargas a la red de saneamiento, la atenuación será importante para mejorar la resiliencia de la red.

Siguiendo las directrices recibidas por el Ciclo Integral del Agua, las indicaciones establecidas en la *Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València* y la Autorización de vertidos de aguas pluviales de la Confederación Hidrográfica del Júcar, se obtienen las siguientes ideas al respecto de criterios de vertido:

- Laminación hasta caudal natural o preurbanizado (para período de retorno 15 años) para los vertidos al canal del antiguo cauce.
- Laminación hasta un percentil volumétrico.
    - La Guía indica unos criterios de diseño para actuaciones a nivel de sector de un percentil 80 en edificación abierta, y un percentil 95 en parques y jardines.

Tomando estas indicaciones se proponen los siguientes criterios de diseño en el control de la calidad.

- Las zonas cuya escorrentía se descargue al canal del antiguo cauce, se diseñarán para un volumen de laminación y tratamiento que permita que el caudal vertido sea el caudal natural de período de retorno 25 años, utilizando de este modo el mismo período de retorno que marca la Ordenanza.
- Las zonas cuya escorrentía se descargue a la red de saneamiento convencional, se diseñarán como mínimo, de acuerdo con los criterios establecidos por la guía, esto es, percentil 80 edificación abierta y percentil 95 para parques y jardines; implementando mayores volúmenes en aquellas zonas aptas para ello.

3.3.2. Control de calidad

De acuerdo con el Capítulo 6 de la *Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València,* los tipos de SUDS que se utilicen deben tener en cuenta los usos del suelo en la cuenca vertiente, de modo que se asegure que se está proporcionando a las escorrentías un tratamiento suficiente, de acuerdo con el potencial contaminante de la cuenca.

Para realizar una estimación del potencial contaminante y de la capacidad de tratamiento de cada tipología de SUDS, se empleará la metodología de Índices de Mitigación, desarrollada originalmente por The SuDS Manual (Woods-Ballards et al., 2015), y que viene recogida en la Guía.

Para cada una de las subcuencas del sistema, deberá identificarse su potencial contaminante, de acuerdo con las descripciones de la Tabla 3. Seguidamente, se deberá comprobar que la tipología de SUDS propuesta presenta un índice de mitigación igual o superior a la peligrosidad de la cuenca, de acuerdo con la Tabla 4.

Tabla 3. Índices de peligrosidad de contaminación en función de los usos del suelo.
Fuente: Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València (2ª Edición).

Uso del suelo	Nivel de riesgo de contaminación	Sólidos suspendidos totales	Metales pesados	Hidrocarburos
Tejados o cubiertas en una atmósfera limpia.	Bajo	0,2	0,2	0,05
Tejados o cubiertas en una atmósfera contaminada (Industrial y Terciario).	Medio	0,3	0,2-0,8	0,05
Caminos o viales con intensidades de tráfico muy débiles. Pistas deportivas. Zonas impermeables de uso lúdico. Zonas de aparcamiento residenciales. Espacios comunes de zonas residenciales de menos de 50 viviendas. Zonas de estacionamiento con poca renovación.	Bajo	0,5	0,4	0,4
Mercados al aire libre. Zonas comerciales peatonales. Zonas de estacionamiento con renovación media. Zonas residenciales con poco tráfico. Zonas industriales sin contaminantes peligrosos. Viales de capacidad media y baja. Aeródromos de baja intensidad de tráfico. Áreas agropecuarias sin uso de sustancias contaminantes.	Medio	0,7	0,6	0,7
Zonas peatonales o industriales de alta densidad de tráfico. Zonas de estacionamiento de alta renovación. Áreas con alto tráfico de vehículos. Aeródromos con alta intensidad de tráfico. Áreas industriales de acopio que manejen sustancias contaminantes. Áreas vinculadas a EDARs o de tratamiento de RSU. Áreas de actividad agropecuaria con uso de sustancias contaminantes.	Alto	0,8	0,8	0,9

Tabla 4. Índices de mitigación de contaminación en función de la tipología de SUDS.
Fuente: Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València (2ª Edición).

Tipología SUDS	Sólidos suspendidos totales	Metales pesados	Hidrocarburos
Cubiertas vegetadas	0,4	0,4	0,4
Jardines de lluvia	0,6	0,5	0,6
Áreas de biorretención	0,8	0,8	0,8
Balsas de detención	0,5	0,5	0,6
Balsas de infiltración (**)	0,6	0,5	0,6
Cunetas vegetadas	0,5	0,6	0,6
Alcorques estructurales	0,6	0,5	0,6
Pavimentos permeables	0,7	0,6	0,7
Drenes filtrantes	0,5***	0,4	0,4
Zanjas y pozos de infiltración	0,5***	0,4	0,4
Depósitos reticulares	*	*	*
Humedales artificiales y estanques	0,8	0,8	0,8

** Por sí mismos, no ofrecen tratamiento, dependen del sistema complementario en la entrada*
*** Considerando que dispone de una capa de vegetación densa sobre un sustrato de 300 mm de profundidad. En caso de no disponer de vegetación, el rendimiento se reduce a 0,4-0,3-0,3*
**** Siempre que se incluya un geotextil superficial, tal y como se indica en las secciones propuestas.*

Del análisis de las tablas anteriores se desprende que los SUDS basados en la biorremediación o la filtración a través de material granular (como las áreas de biorretención o los pavimentos permeables) presentan un potencial de tratamiento superior a otras técnicas.

Para asegurar un adecuado tratamiento de las escorrentías, además de seleccionar la tipología de SUDS más conveniente, deben comprobarse una serie de criterios:

- Para aquellos SUDS, con una función importante de retención y sedimentación (SUDS con medio filtrante como jardines de lluvia o áreas de biorretención), debe asegurarse que el volumen de retención sea suficiente para poder almacenar y tratar íntegramente los episodios lluviosos más frecuentes, y proporcionar tratamiento a las primeras aguas de todos los episodios lluviosos, que son las que suelen presentar una carga contaminante más elevada. Siguiendo las recomendaciones de la Confederación Hidrográfica del Júcar y de la *Guía básica para el Diseño de Sistemas Urbanos*

de Drenaje Sostenible en la Ciudad de València, los SUDS deberán ser capaces de almacenar y tratar en origen un volumen mínimo correspondiente al percentil V_{80}.

- Para otros SUDS, con una función de filtración principal (SUDS con medios granulares como pavimentos permeables o zanjas filtrantes), el concepto de volumen de retención se ve sustituido por intensidad de tratamiento, dado que este es proporcionado por el paso de la escorrentía a través del paquete de medio granular. Se define el criterio de Intensidad de Tratamiento como el umbral de intensidad por debajo del cual queda el X % del volumen de lluvia generado.

3.4. Selección de otros parámetros

3.4.1. Coeficientes de escorrentía

Se utilizarán los siguientes coeficientes de escorrentía, de acuerdo con la Ordenanza de Saneamiento, para estimar las superficies impermeables equivalentes de cada subcuenca:

Tabla 5. Coeficientes de escorrentía propuestos.

Uso del suelo	C
Impermeable	0,95
Edificación	0,85
Permeable	0,30

3.4.2. Coeficiente de rugosidad

Se utilizarán los siguientes coeficientes de rugosidad, de acuerdo con la Ordenanza de Saneamiento, para estimar la rugosidad de cada material. Los valores son conservadores para tener en cuenta el incremento de rugosidad con el tiempo debido a incrustaciones, y la existencia de pozos de registro, alineaciones no rectas, cambios de dirección, etc.

Tabla 6. Coeficientes de rugosidad.

Uso del suelo	C
Hormigón	0,015
Materiales plásticos	0,011

Para el caso de los tubos perforados situados dentro del cuerpo de los pavimentos permeables, se empleará un coeficiente de rugosidad de 0,015 para tener en cuenta la influencia de las perforaciones en la rugosidad del elemento.

3.4.3. Diámetros mínimos de tuberías

De acuerdo con la Ordenanza de Saneamiento, para evitar obstrucciones y facilitar las labores de limpieza se emplearán los siguientes diámetros mínimos.

Tabla 7. Diámetros mínimos de tubería

Tipo colector	Diámetro interior aproximado (mm)
Unitario	335
Pluviales	335
Residuales	335
Acometida domiciliaria	263
Albañales	209

Para el caso de los tubos perforados situados dentro del cuerpo de los pavimentos permeables y los jardines de lluvia, se emplearán tubos perforados de diámetro nominal 110 mm.

3.4.4. Velocidades máximas y mínimas

Se limitará la velocidad máxima para evitar daños por fricción, y las velocidades mínimas para evitar la sedimentación de los sólidos arrastrados en suspensión, de acuerdo con los valores dictados por la Ordenanza.

Tabla 8. Velocidades máximas y mínimas

Red	Caudal	Velocidad máxima (m/s)	Velocidad mínima (m/s)
Pluviales	Q_{25}	4	1,2
Residuales	Q_R	3	0,8
Unitario	Q_{25}	4	1,2
	Q_R	-	0,4

3.4.5. Distancia máxima entre pozos

De acuerdo con la Ordenanza de Saneamiento, la distancia máxima recomendada en alineaciones rectas entre pozos de registro es de 25 m.

Tabla 9. Distancia máxima entre pozos de registro.

Diámetro nominal colector (mm)	Diámetro interior del pozo (cm)	Distancia máxima recomendada en alineaciones rectas (m)
400 < D < 1500	100-150	25

3.4.6. Tiempo de vaciado de los SUDS

Con el propósito de que los SUDS estén disponibles para gestionar tormentas sucesivas y evitar la proliferación de mosquitos o malos olores, siguiendo la Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València, se establece que el tiempo de vaciado de los SUDS no debe ser superior a 48 horas.

3.4.7. Nivel freático

En caso de detectarse presencia de nivel freático, la *Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València* recomienda guardar una distancia superior a 1 metro entre la superficie freática y la base del SUDS, especialmente cuando la base de los SUDS sea permeable.

3.4.8. Infraestructuras existentes

Los SUDS pueden ocupar un espacio tanto en superficie como bajo tierra, por lo que deben vigilarse las afecciones a otras infraestructuras existentes. La infiltración puede afectar a las cimentaciones de edificaciones existentes, por lo que debe guardarse una distancia prudencial entre las mismas y aquellos SUDS que evacuen las aguas mediante la infiltración.

La *Guía básica para el Diseño de Sistemas Urbanos de Drenaje Sostenible en la Ciudad de València* recomienda guardar una distancia de 3 m respecto a las cimentaciones de edificaciones existentes, pudiéndose reducir esta distancia hasta 1 m para aquellos SUDS que solo gestionan la escorrentía propia.

Además de los cimientos, es relevante tener en cuenta la ubicación de servicios de electricidad, saneamiento, telefonía, gas, fibra óptica, etc. existentes en las zonas donde se pretenden emplazar SUDS. Estos servicios deben ser identificados, de modo que el diseño de la actuación tenga en cuenta su ubicación y se puedan seleccionar las técnicas SUDS más adecuadas en cada caso.

3.4.9. Porosidad de materiales

Para el cálculo del volumen de almacenamiento en las diferentes tipologías de SUDS, se emplearán los siguientes índices de huecos:

- Acumulación en superficie: n = 1,00.
- Acumulación en material granular drenante (gravas): n = 0,35.
- Acumulación en medios filtrantes y suelos vegetales: n=0,15.

4. Estrategia de saneamiento y drenaje propuesta

4.1. Introducción

La estrategia de saneamiento y drenaje propuesta para el proyecto de las obras de urbanización del sector Grao, contempla la utilización de una estrategia mixta de drenaje convencional y drenaje sostenible para el control de la calidad y la cantidad de las escorrentías.

De forma mayoritaria, los viales, las plazas de aparcamiento, las superficies impermeables de las parcelas y las rotondas serán gestionadas mediante drenaje convencional, con el uso de pozos e imbornales o canaletas. En cambio, la escorrentía generada en parques y jardines, y zonas verdes de viarios, se drenarán con el uso de drenaje sostenible. Una descripción más detallada de esta separación se muestra en el Apartado 4.3.2.

La red de unitaria de saneamiento y drenaje convencional se conectará a la red unitaria ya existente, empleando los pozos y colectores existentes, en tanto sea posible. Por otro lado, la red de drenaje sostenible contará con almacenamiento superficial para la gestión de las tormentas frecuentes y descargas reguladas por medio de tuberías de desagüe y aliviaderos. Estas descargas se realizarán al canal del antiguo cauce del río Turia, en aquellas zonas donde se disponga de cota suficiente. En el resto de zonas, las descargas de los SUDS se realizarán a la red convencional, proporcionando cierta laminación y mejorando la resiliencia de la misma. Como se ha comentado en el Apartado 2.3, la estrategia de drenaje propuesta descarta la infiltración por motivos de permeabilidad.

En el caso de las descargas al canal del antiguo cauce, la estrategia se centrará en el tratamiento de la escorrentía previo al vertido, para lo cual se diseñarán sistemas que favorezcan el filtrado de la escorrentía a través de capas de medio filtrante, medio granular y geotextiles, hasta alcanzar un tubo dren y de aquí conectar con la red de colectores que dirija el agua hacia el cauce.

De acuerdo con lo establecido en el Apartado 3.3.1, se propone que el vertido a cauce no sea mayor que el que se generaba previo a la urbanización de la zona.

4.2. Descripción de las técnicas SUDS propuestas

Las técnicas SUDS propuestas en este proyecto utilizarán las zonas verdes previstas, para la instalación de jardines de lluvia; y en las zonas de aparcamiento más cercanas al cauce, la utilización de pavimentos permeables. En las grandes zonas verdes del sector, se instalarán una serie de balsas cuyo funcionamiento será idéntico al de un jardín de lluvia, pero de mayores dimensiones. Ambas opciones, contaran con sistemas de desagüe y de rebose que permitan trasegar y laminar las escorrentías, previo a la descarga a la red de colectores convencional. En el caso de la zona más cercana al canal del antiguo cauce, se realizarán descargas por gravedad.

A continuación, se describen las técnicas de drenaje sostenible propuestas:

4.2.1. Jardines de lluvia

Los jardines de lluvia son áreas ajardinadas deprimidas respecto a las zonas impermeables circundantes, de modo que pueden recibir y almacenar superficialmente escorrentías. Estas escorrentías se filtran a través de un medio filtrante, habitualmente formado por arenas y tierra vegetal, que sirve de soporte para el crecimiento de las plantas (Figura 8).

Su objetivo es la recogida la escorrentía generada en el viario y otras superficies impermeables de manera que entren en las áreas de biorretención para su laminación, tratamiento y posterior vertido a la red de pluviales.

Los jardines de lluvia disponen de espesores de medio filtrante entre 0,3 y 0,5 m y sirven para la gestión escorrentías procedentes de zonas peatonales o cubiertas

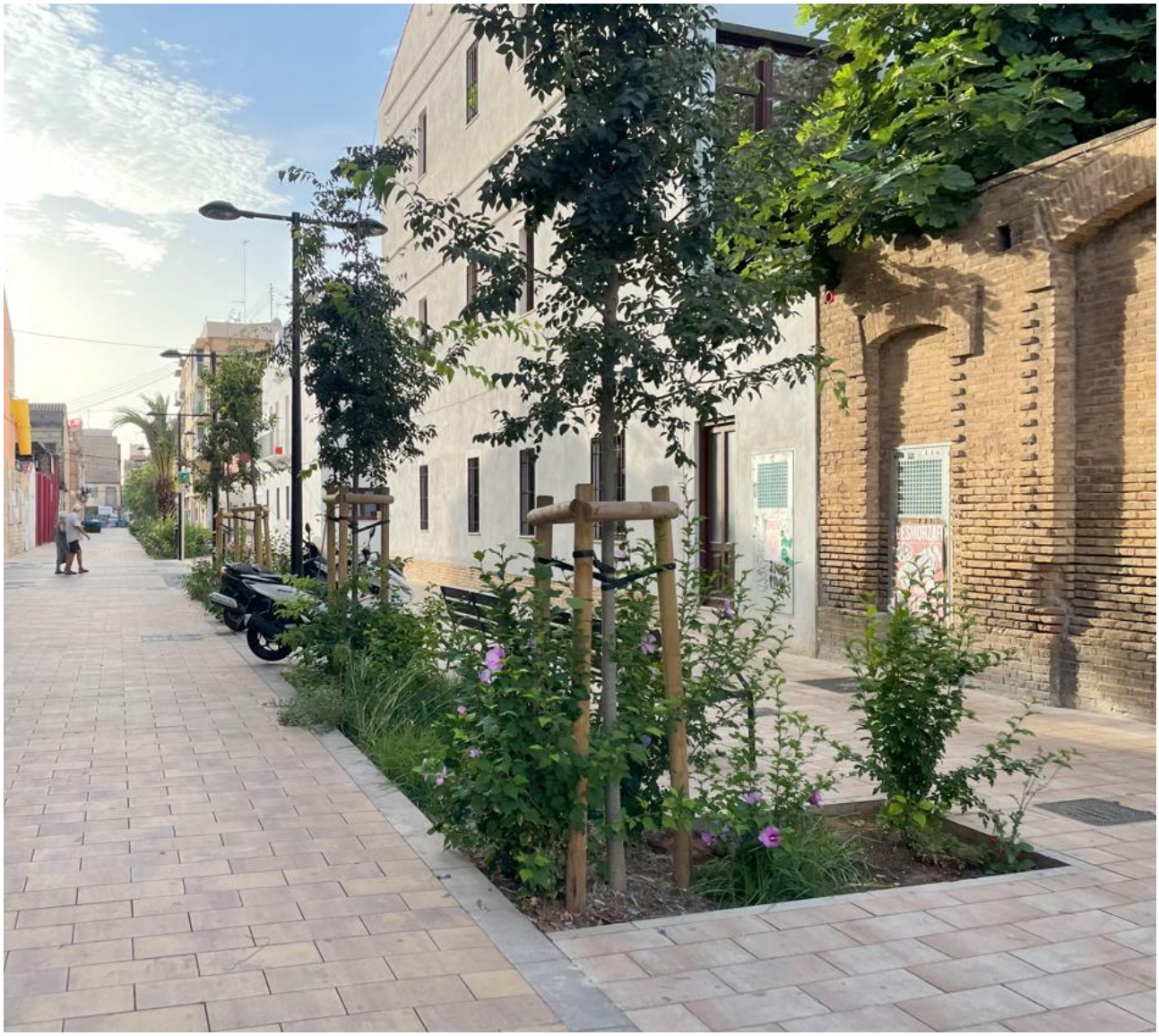


Figura 8. Jardín de lluvia, en el barrio del Cabañal, Valencia.

La siguiente figura muestra una sección transversal ejemplo para los jardines de lluvia en el proyecto:

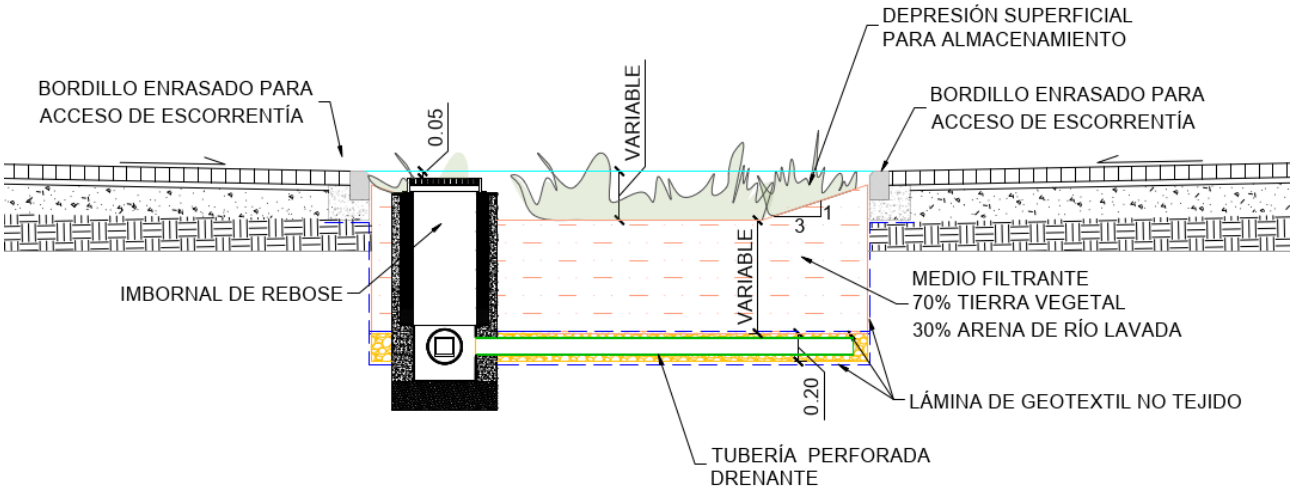


Figura 9. Sección transversal ejemplo para los jardines de lluvia.

4.2.2. Áreas de biorretención

Similar a los jardines de lluvia, las áreas de biorretención son visualmente idénticas a los jardines de lluvia. Su principal diferencia radica en que son capaces de gestionar escorrentías procedentes de la red viaria, incrementando el espesor del medio filtrante (habitualmente entre entre 0,8 y 1 m).

De este modo, son capaces de proporcionar un tratamiento mayor sobre la escorrentía, mejorando los indicadores cualitativos de la escorrentía saliente.

Figura 10. Área de biorretención, en el barrio de la Rochapea, Pamplona.

4.2.3. Pavimentos permeables

Los pavimentos permeables son un tipo de pavimento que permite la filtración del agua de lluvia hacia las capas subsuperficiales. Esta agua se almacena temporalmente bajo el pavimento y puede infiltrarse en el suelo, ser drenada de manera controlada o en algunos casos, ser utilizada y almacenada para su reaprovechamiento.

Los pavimentos permeables se clasifican en varios tipos en función de si el paso de la escorrentía se produce a través de toda su superficie (pavimentos porosos), o a través de juntas permeables (sistema de malla/geocelda o pavimentos permeables por juntas).

Figura 11. Pavimento permeable por junta, en el estadio Metropolitano de Madrid.

Se propone en este proyecto el uso de pavimentos permeables por junta, que están compuestos por bloques de materiales impermeables, cuya disposición crea huecos que permiten que el agua se filtre a las capas inferiores. Estos huecos se suelen rellenar con un gravillín, que proporciona permeabilidad y la capacidad de filtración.

Los pavimentos permeables son adaptables y pueden utilizarse en diversas ubicaciones, como aceras, calles y aparcamientos. Estos sistemas captan la escorrentía en origen, pero también pueden captar la escorrentía de áreas impermeables adyacentes. Se recomienda que la proporción entre pavimento permeable y superficie impermeable no sea mayor de 1:2. El mantenimiento es muy importante para evitar que los sedimentos obstruyan los poros que permiten el paso del agua.

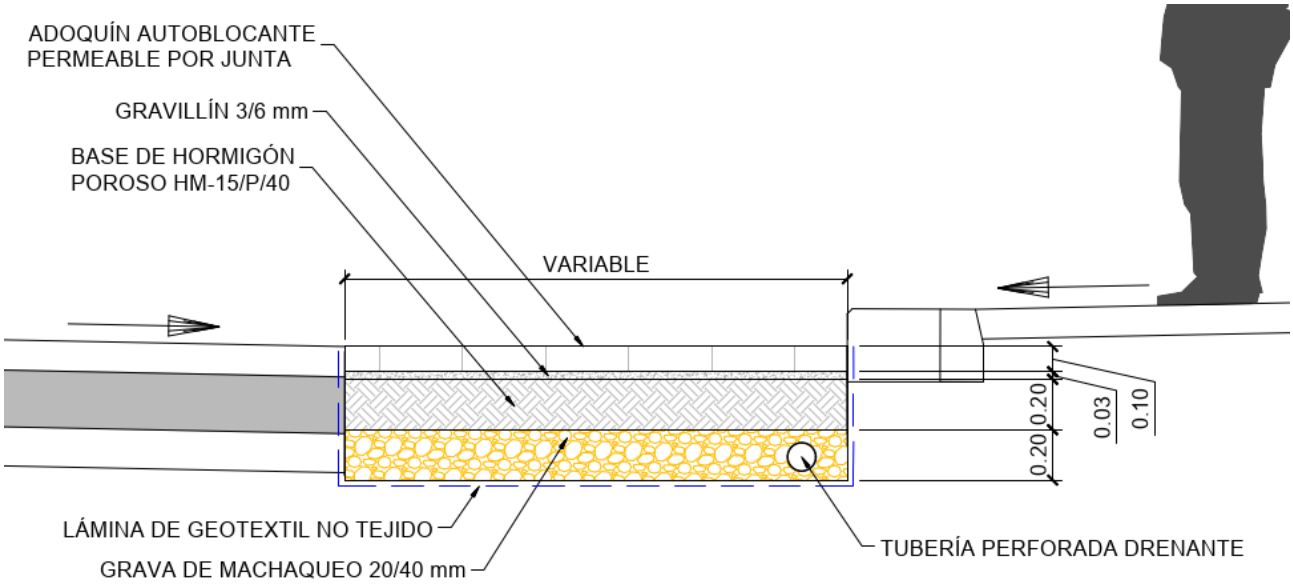


Figura 12. Sección transversal ejemplo para los pavimentos permeables.

4.3. Descripción del sistema de saneamiento y drenaje propuesto

Como se ha comentado anteriormente,

La red proyectada adopta una configuración mixta, combinando:

- Red de saneamiento unitaria convencional para las zonas edificadas, dotacionales y viales.
- Sistemas urbanos de drenaje sostenible (SUDS) en zonas verdes.
- Depósito de retención de tormentas (previsto por el Ciclo Integral del Agua del Ayuntamiento de Valencia, aunque su diseño no está incluido en este proyecto de urbanización), con impulsión al cauce del Turia para control de descargas en tiempo de lluvia (DSU). Para este último se ha trazado un flujo de los ramales principales hacia la ubicación del futuro depósito de retención de tormentas.

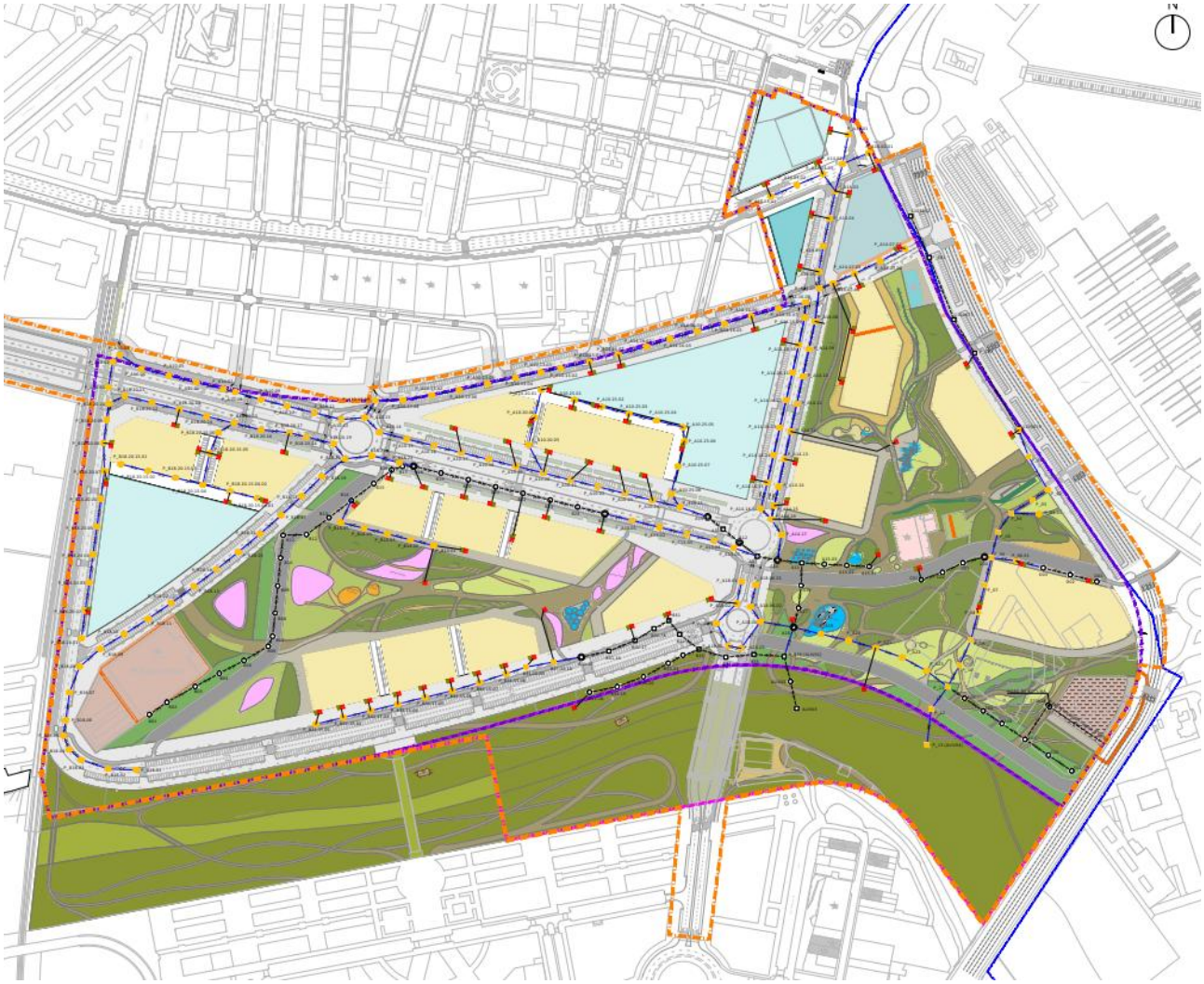


Figura 13. Sistemas de drenaje propursto

4.3.1. Servicios afectados: modificación de la infraestructura unitaria de saneamiento y drenaje final del sector Moreras e impulsión de la EBAR Cantarranas

4.3.1.1. Descripción del sistema

En la zona sur del Sector El Grao se localiza el tramo final del saneamiento y drenaje por gravedad procedente del Sector Moreras, así como las canalizaciones de impulsión asociadas a la Estación de Bombeo de Aguas Residuales (EBAR) de Cantarranas.

Dentro del presente proyecto de ejecución de las obras de urbanización del Sector Grao, se contempla la construcción de una estructura de paso sobre el antiguo cauce del río Turia, destinada a conectar los sectores del Grao y Moreras. Las cimentaciones de esta estructura, en su margen correspondiente al Sector

Moreras, interfieren directamente con las infraestructuras de saneamiento, drenaje y bombeo actualmente existentes, tal como se observa en la imagen adjunta.

Figura 14. Sistemas de drenaje del sector Moreras e impulsión EBAR Cantarranas.

Con el fin de evitar dicha interferencia, se proyecta la modificación de:

- La estructura final del sistema unitario de saneamiento y drenaje por gravedad del Sector Moreras.
- Las canalizaciones de impulsión del sistema de bombeo procedente de la EBAR de Cantarranas.

a. Drenaje por gravedad

El tramo final del actual saneamiento del Sector Moreras se compone de cuatro tuberías en paralelo de diámetro DN1300 que descargan en una arqueta de 8,50 x 3,20 m. Desde esta primera arqueta parten dos tuberías DN2000 que vierten a una segunda arqueta de 6,50 x 4,70 m. A partir de esta segunda arqueta, el sistema continúa mediante una estructura de vertido al nuevo cauce del río Turia, cuya geometría exacta se desconoce. Por otro lado, desde dicha arqueta final también parte el colector de aguas residuales por gravedad en dirección este.

b. Impulsión de la EBAR de Cantarranas

El sistema de impulsión está compuesto por dos conducciones:

- Una tubería de fibrocemento DN 1000 situada al norte (actualmente fuera de servicio).
- Una tubería de fundición dúctil DN700 situada al sur, que se encuentra en servicio.

Ambas conducciones discurren parcialmente en paralelo. En el arranque de la impulsión existen dos arquetones de dimensiones 4,40 x 3,80 m (uno por línea), que alojan sendos caudalímetros. A continuación de éstos, se encuentran dos arquetas de 2,80 x 2,80 m en cada línea, donde se ubican las ventosas correspondientes. Para regular el caudal por cada una de las canalizaciones existe una válvula de reparto al inicio de la impulsión, situada a la salida de la EBAR.

4.3.1.2. Afecciones y actuaciones proyectadas

a. Afecciones a los sistemas de drenaje e impulsión existentes

Las cimentaciones de la nueva estructura de paso afectan tanto a las arquetas del sistema de drenaje por gravedad localizadas junto a la EBAR de Cantarranas, como a las canalizaciones de impulsión y los arquetones que albergan los caudalímetros de las propias líneas.

Para evitar la interferencia entre la cimentación de la nueva estructura proyectada y los sistemas de drenaje existentes se proyecta el desplazamiento hacia el este de las arquetas de 8,50 x 3,20 m y 6,50 x 4,70 m del drenaje por gravedad y la ejecución de dos nuevos tramos de canalizaciones de impulsión, adaptados al nuevo trazado, tal como se muestra en la imagen correspondiente.

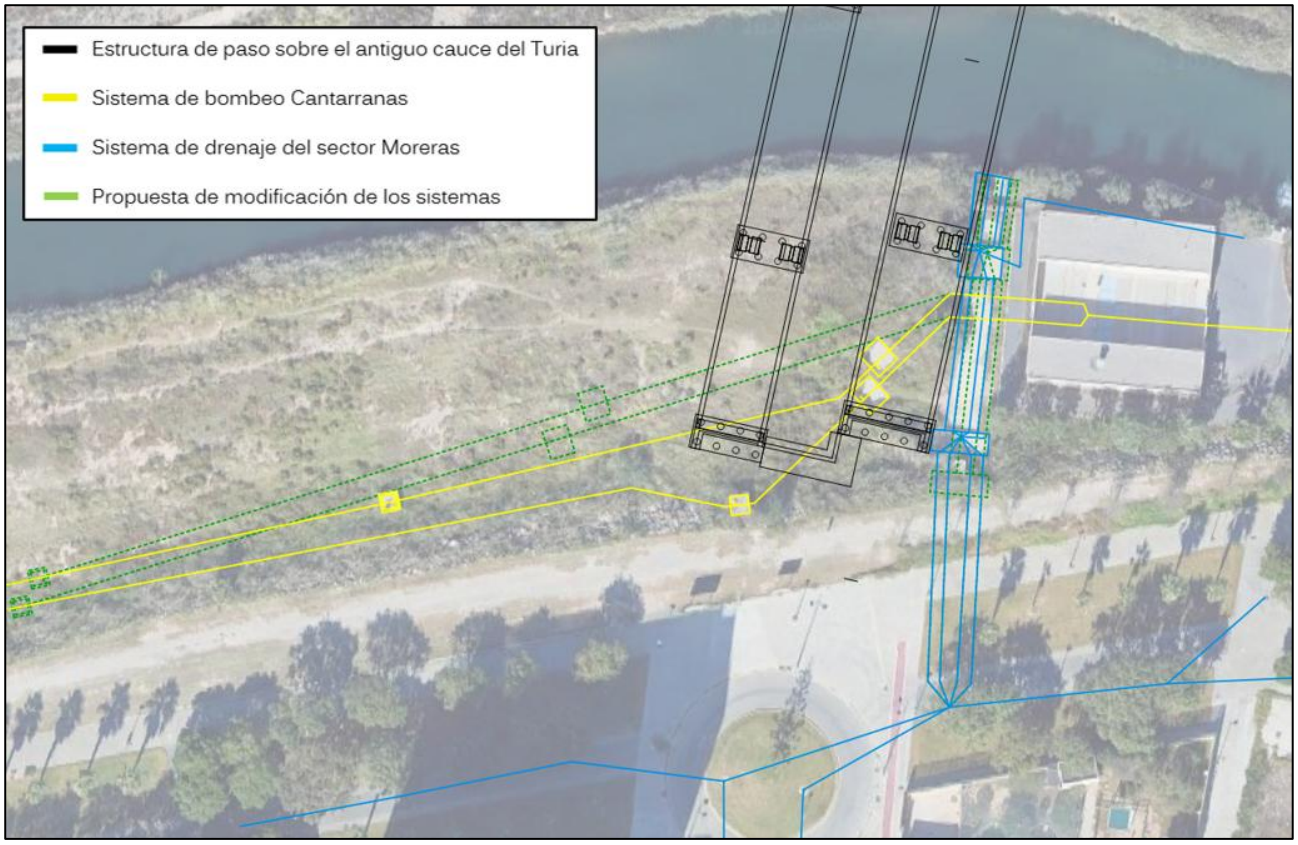


Figura 15. Propuesta de actuación sobre los sistemas de drenaje Sector Moreras e impulsión EBAR Cantarranas

b. Procedimiento de ejecución de la actuación

El proceso constructivo se ha planificado en fases sucesivas, con el objetivo de garantizar la continuidad del servicio de saneamiento durante las obras, minimizar las afecciones al entorno y permitir una ejecución segura y ordenada.

a. Sustitución del tramo final del drenaje por gravedad del Sector Moreras

1 Desvío provisional del caudal de aguas residuales

La primera actuación consistirá en el desvío del caudal de aguas residuales que actualmente discurre por gravedad desde la primera arqueta (8,60 x 3,60 m) hacia la canalización existente en dirección este. Este desvío se realizará mediante medios provisionales de bombeo o canalizaciones temporales, permitiendo liberar de caudal las dos conducciones DN2000, la segunda arqueta (6,50 x 4,70 m) y la estructura de vertido al cauce del Turia.

2 Ejecución de la nueva segunda arqueta y estructura de vertido

Una vez liberadas las conducciones DN2000 y la segunda arqueta, se procederá a su demolición y a la ejecución de la nueva arqueta de dimensiones 6,00 x 4,20 m, así como de una nueva estructura de vertido. Dado que no se dispone de datos exactos sobre la estructura de vertido existente, esta se ejecutará replicando sus dimensiones y configuración actuales.

3 Nuevo desvío hacia la nueva segunda arqueta

Finalizada la nueva segunda arqueta, se procederá a desviar el caudal residual desde el pozo situado aguas arriba de la primera arqueta hacia esta nueva arqueta de 6,00 x 4,20 m. Este desvío permitirá liberar la primera arqueta para su reubicación.

4 Ejecución de la nueva primera arqueta y de las canalizaciones DN2000

Con la primera arqueta fuera de servicio, se llevará a cabo su demolición y la ejecución de la nueva arqueta (8,60 x 3,60 m) en la ubicación prevista, más próxima al camino de servicio. Para ello será necesario recortar y desviar las cuatro canalizaciones existentes que vierten a esta arqueta, adaptándolas a la nueva geometría y posición. Posteriormente se ejecutarán las nuevas conducciones DN2000 de conexión entre la primera y la segunda arqueta.

5 Retirada de las instalaciones provisionales

Una vez completadas las actuaciones sobre el drenaje por gravedad, se procederá a la retirada de los sistemas provisionales empleados para el desvío del caudal.

b. Renovación de las líneas de impulsión de la EBAR de Cantarranas

1 Ejecución de la nueva línea de impulsión norte (fibrocemento fuera de servicio)

Se iniciará la intervención sobre la línea de impulsión norte, actualmente fuera de servicio y ejecutada en fibrocemento DN1000. Esta tubería será retirada conforme al protocolo específico para materiales con

amianto, según lo establecido en el Real Decreto 396/2006. La retirada deberá ser realizada por una empresa especializada inscrita en el RERA, previa aprobación del Plan de Trabajo con Riesgo por Amianto (PTRA).

Posteriormente se ejecutará la nueva canalización de FD DN1000, junto con las correspondientes arquetas para la instalación del caudalímetro y la ventosa, que serán trasladados desde los elementos antiguos.

La unión entre la nueva conducción de FD y el tramo de fibrocemento existente se realizará mediante una manga de unión especial tipo Gibault, o equivalente. Esta unión permite conectar conducciones de distintos materiales y tolerancias mediante una abrazadera de cierre mecánico con junta de elastómero, asegurando la estanqueidad del conjunto sin necesidad de realizar uniones por soldadura o encolado.

2 Puesta en servicio de la línea norte y liberación de la línea sur

Una vez finalizada la línea de impulsión norte, se procederá a su puesta en servicio utilizando la válvula de reparto existente en la EBAR de Cantarranas para derivar el caudal a dicha línea, permitiendo así dejar fuera de servicio la línea de impulsión sur.

3 Renovación de la línea de impulsión sur

Liberada la línea de impulsión sur, se ejecutará su sustitución completa por una nueva conducción de fundición dúctil DN700, incluyendo la renovación de las arquetas de caudalímetro y ventosa. Al igual que en la línea norte, se procederá a instalar el equipamiento hidráulico existente (caudalímetro y ventosa) en las nuevas arquetas.

4.3.1.3. Consideraciones especiales para la canalización de fibrocemento

La sustitución del tramo afectado de la tubería de fibrocemento DN1000 requiere la aplicación de medidas específicas de seguridad debido a la presencia de amianto en su composición. Al tratarse de un residuo peligroso, su retirada deberá cumplir lo establecido en el **Real Decreto 396/2006**, por el que se regulan las disposiciones mínimas de seguridad y salud aplicables a los trabajos con riesgo de exposición al amianto.

Será obligatorio contratar una empresa especializada e inscrita en el **Registro de Empresas con Riesgo por Amianto (RERA)**, la cual deberá elaborar y tramitar ante la autoridad laboral competente el correspondiente **Plan de Trabajo con Riesgo por Amianto (PTRA)**.

La nueva conducción, proyectada en **fundición dúctil DN1000**, sustituirá únicamente el tramo afectado de la tubería de fibrocemento. El resto de la conducción existente se mantendrá en servicio, por lo que será necesario prever una **unión especial de transición** entre ambos materiales.

4.3.2. Descripción del sistema de drenaje sostenible

En la siguiente figura se presenta una distribución de zonas, para el análisis de la aplicación de drenaje sostenible en cada una de las áreas. Se proporciona a su vez, un breve resumen discretizado de la gestión de la escorrentía en cada zona:

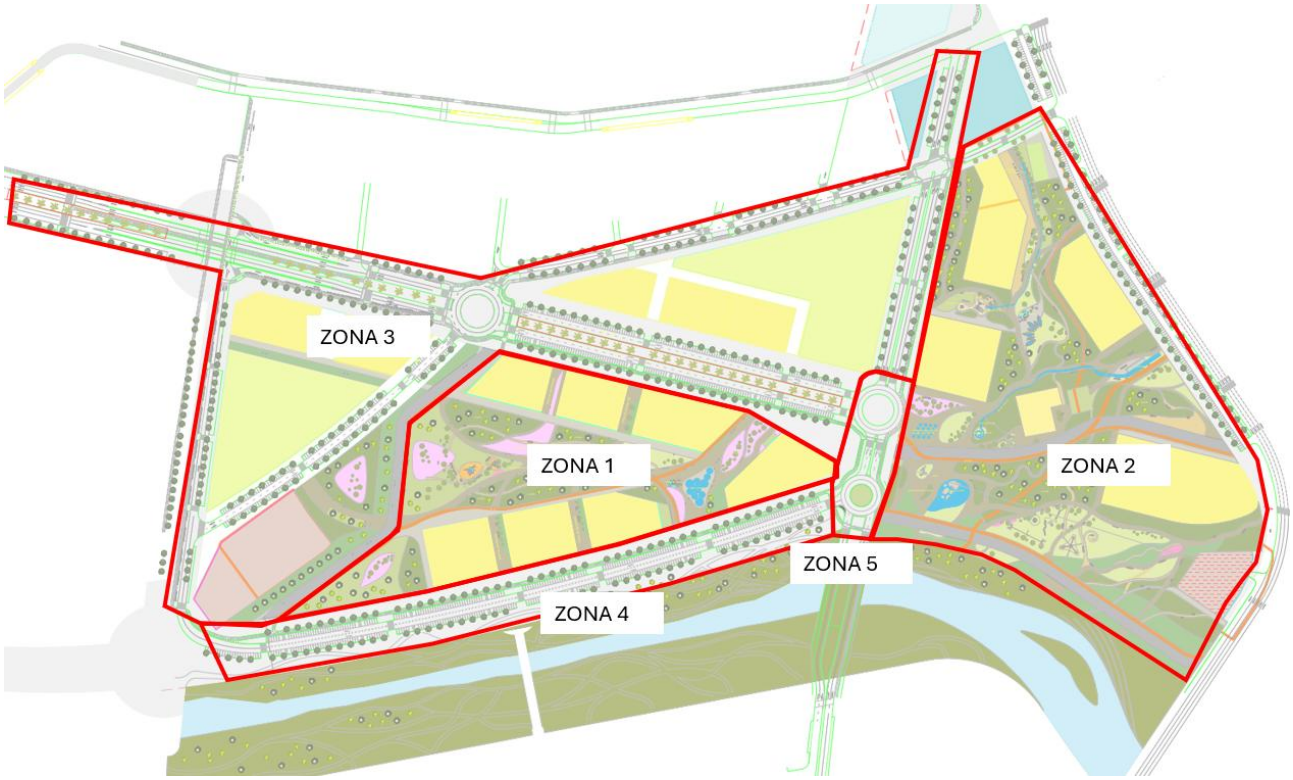


Figura 16. Distribución de zonas con aplicación de drenaje convencional y drenaje sostenible.

1. Se propone la implantación de una serie de jardines de lluvia situados en el interior de la zona verde, que permitan la gestión de la escorrentía generada en toda su superficie. Esta serie de jardines proporcionará laminación y tratamiento de las escorrentías generadas, favoreciendo el filtrado de las aguas a través de un medio filtrante y un medio granular, previo al vertido al cauce. Los vertidos al cauce quedan limitados al caudal natural. Por otro lado, el drenaje convencional en Zona 1 se encargará de la gestión de la escorrentía procedente de todas las parcelas y de las zonas de vial situadas al oeste y al norte de esta zona.

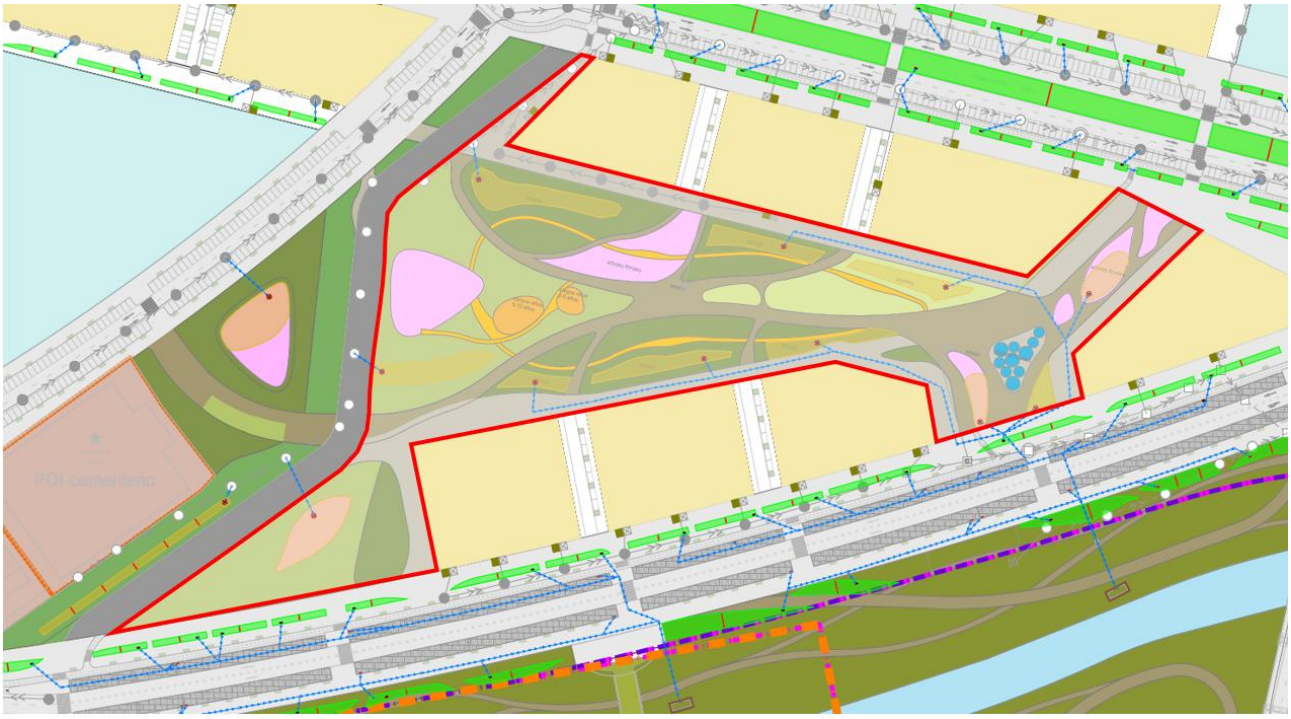


Figura 17. Aplicación de SUDS en Zona 1.

2. Se propone la implantación de una serie de jardines de lluvia situados en el interior de la zona verde, que permitan la gestión de la escorrentía generada en la propia superficie. Estos jardines proporcionarán una atenuación de los caudales pico mediante el almacenamiento superficial y la retención de la escorrentía en los sustratos, previo al vertido a la red convencional, dado que no se dispone de cota suficiente para el vertido al cauce por gravedad. Al mismo tiempo, su configuración contribuye al riego pasivo de las especies vegetales que estén situadas en su interior, reduciendo los caudales que alcanzan el unitario. La red convencional dispone de redes por los viales principales y de un tanque de tormentas situado en la parte sur, previo a su bombeo ubicado en el lado contrario respecto al canal del cauce, que posteriormente impulsa a la depuradora de Pinedo.

Figura 18. Aplicación de SUDS en Zona 2.

3. Se propone el uso de la mediana central de la nueva Avenida de Francia para la gestión de la escorrentía propia y una serie de jardines de lluvia corridos en las aceras, para la recogida de la escorrentía que se genera tanto en las aceras como en el carril bici. Esta recogida favorecerá el riego pasivo de las especies aquí localizadas, mientras que el agua acumulada en el sustrato contribuye a disminuir los caudales que alcanzan el unitario. Dado que se trata de una superficie de firme existente, que se pretende mantener; la escorrentía generada en la calzada se recogerá mediante imbornales y canaletas. Debido a las cotas propuestas, no es factible la conexión con el cauce, y los desagües conectarán a la red convencional que circula por debajo de los viales. Por limitaciones espaciales del proyecto, el resto de los viales y parcelas impermeables no dispondrán de drenaje sostenible y se aplicarán técnicas de drenaje convencional en su gestión.

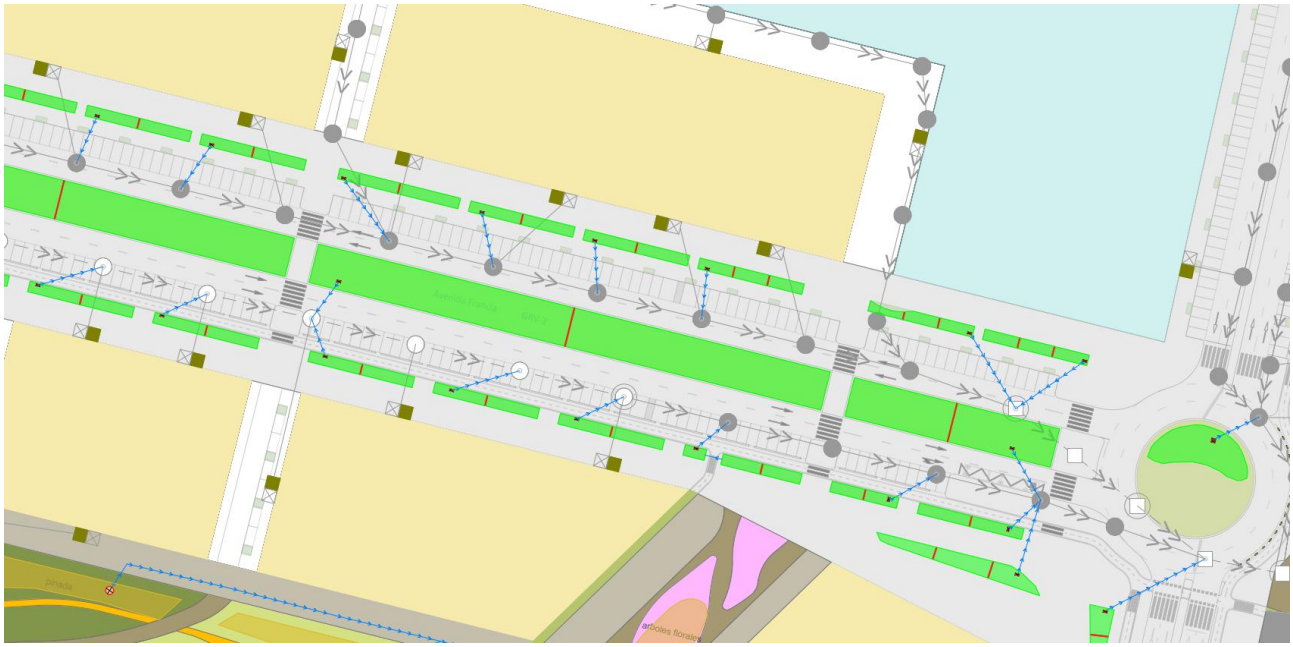


Figura 19. Aplicación de SUDS en Zona 3.

4. Se propone la implantación de pavimento permeable en las zonas de aparcamiento, y de parterres corridos en las aceras, para la gestión y el tratamiento adecuado de la escorrentía que se produce en toda la zona 4, incluyendo viales. Pese al cometido general de tratar de conservar el firme existente en la medida de lo posible, la actuación en esta sección se considera prioritaria, dado que las cotas son favorables para el vertido al cauce existente. De este modo, se promueve la desconexión de una parte importante de la escorrentía de la red convencional, reduciendo los costes posteriores de bombeo y de tratamiento.

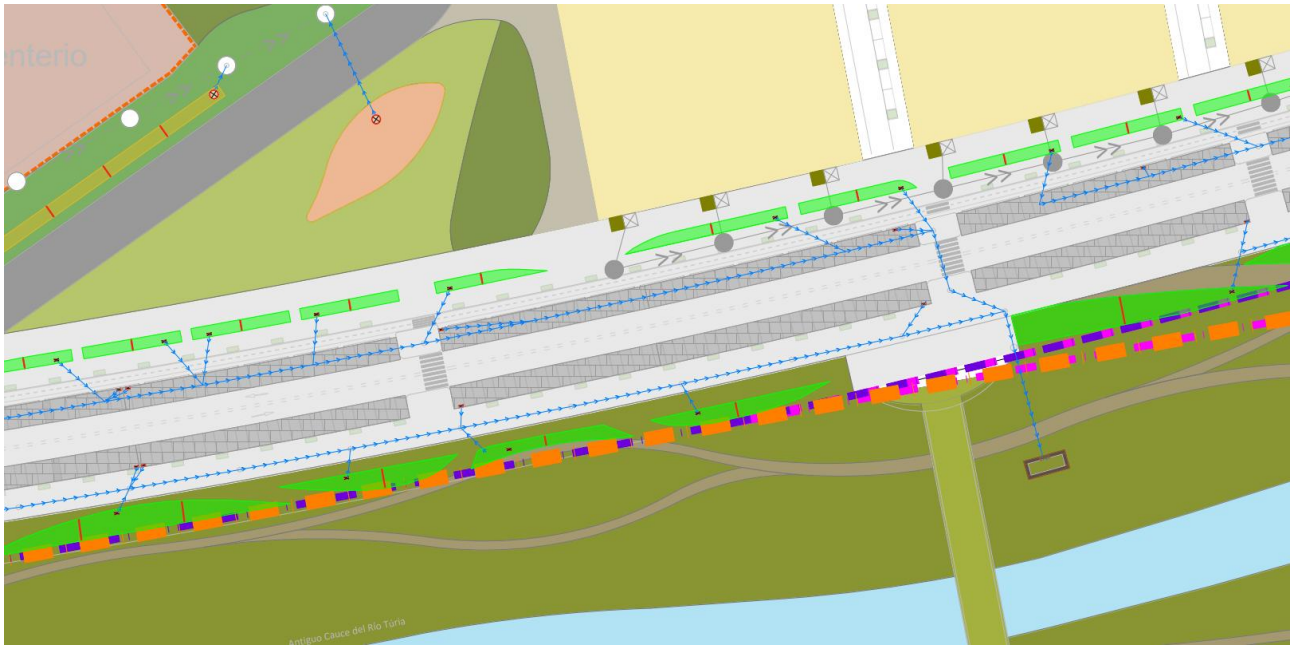


Figura 20. Aplicación de SUDS en Zona 4.

5. Se propone la implantación de un área de biorretención en la parte interior de la rotonda norte, que permita la gestión de la escorrentía procedente de viario. La rotonda de la zona sur se gestionará mediante drenaje convencional ya que no ha sido posible realizar un cambio en las pendientes de esta (hacia el centro), de forma que se gestionen de manera adecuada los entronques de los viales entrantes y salientes. Este SUDS, proporciona atenuación y tratamiento de la escorrentía contribuyendo al riego pasivo de las especies vegetales, y reduciendo el volumen de escorrentía que alcanza la red convencional, mediante la retención en el sustrato.

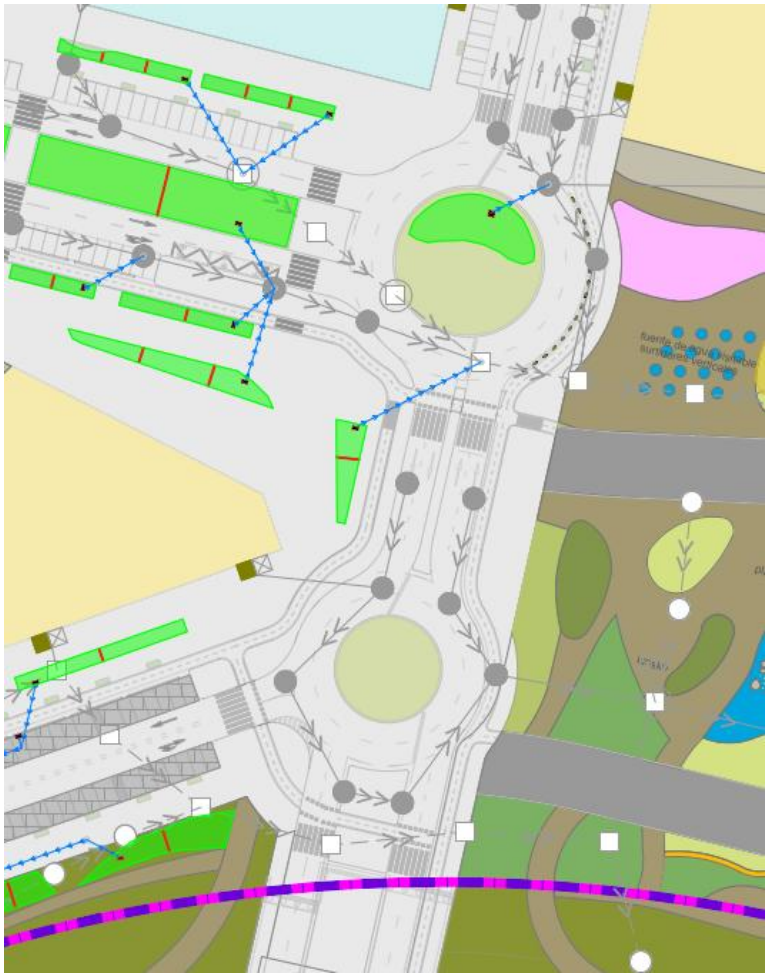


Figura 21. Aplicación de SUDS en Zona 5.

4.3.3. Descripción del sistema unitario de saneamiento y drenaje convencional

La red de saneamiento unitaria convencional proyectada incorpora los colectores existentes en el ámbito en lo posible, pues debe adaptarse a la nueva urbanización propuesta. Se propone una red con un esquema ramificado, organizado en ramales principales, que canalizan los caudales hacia los puntos de vertido definidos, y ramales secundarios, encargados de recoger las aportaciones distribuidas de la urbanización y conducirlas hasta los principales.

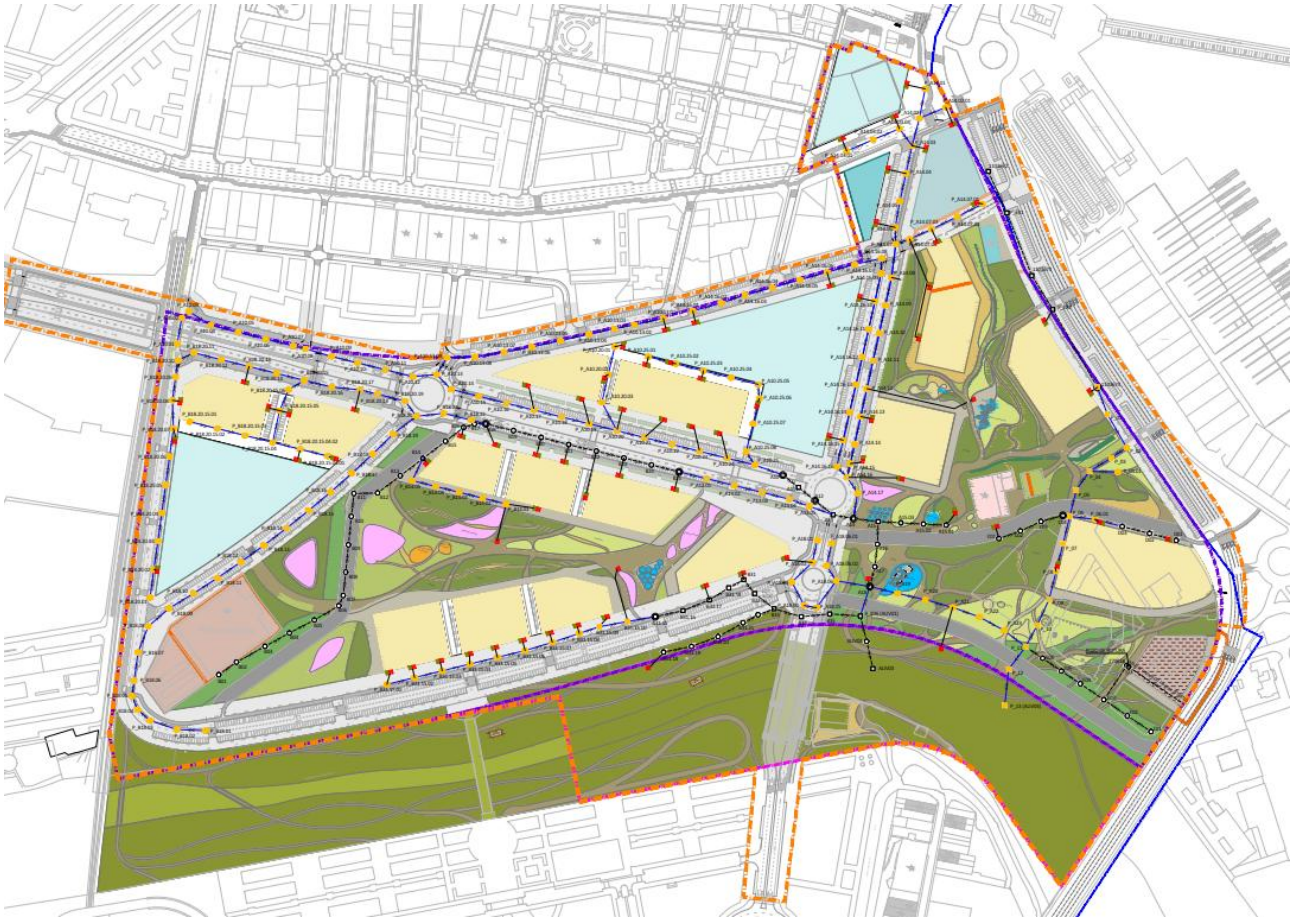


Figura 22. Red de colectores unitarios para la urbanización propuesta en el Sector Grao.

Los ramales unitarios integran el drenaje tanto de aguas residuales como de pluviales, con prioridad en la evacuación de éstas últimas mediante dispositivos de captación puntual (sumideros tipo Valencia, arquetas de clapeta) distribuidos en las zonas bajas de la topografía. Además, para cada una de las parcelas edificables previstas en la ordenación propuesta para la urbanización se han propuesto tres acometidas a la red de saneamiento general, de modo que se facilite la conexión en el futuro cuando estos edificios se diseñen. También se han incorporado acometidas en las parcelas dotacionales y en las zonas verdes en aquellos puntos en los que se prevé la instalación de quioscos o aseos públicos.

Los ramales secundarios de la red propuesta recogen las escorrentías de las distintas subcuencas generadas por superficies pavimentadas, cubiertas, viales y zonas dotacionales. Están conectados transversalmente a los ramales principales y discurren, por lo general, por el interior de los viales secundarios. Estas conducciones presentan diámetros menores (normalmente 400–600 mm en PVC o PEAD corrugado) y han sido diseñadas para condiciones de caudal medio y caudal punta, considerando un coeficiente de escorrentía medio de 0,85.

Cada ramal principal ha sido definido con sección uniforme (generalmente de tipo circular) y cotas adaptadas al relieve y al futuro trazado urbano, asegurando pendientes mínimas compatibles con velocidades autolimpiantes y evitando, en la medida de lo posible, sobrecargas en la red. Los ramales A y B

concentran la mayor parte del caudal del sector, habiéndose dispuesto pozos de registro con interdistancias aproximadas de 25 metros, facilitando su inspección y mantenimiento.

Los ramales principales están formados por conducciones de mayor diámetro y capacidad hidráulica, diseñadas para transportar los caudales máximos generados bajo condiciones de tormenta de diseño con un período de retorno de 25 años, según la Normativa para obras de saneamiento y drenaje urbano del Ayuntamiento de Valencia (2015). Estas conducciones recorren los ejes viales estructurantes (Avenida de Francia, Alameda y calle Ejército Español) y desembocan en puntos de vertido estratégicos, como el aliviadero existente o la estación de bombeo de Cantarranas.

La red unitaria proyectada considera un funcionamiento tal que, en un evento de tormenta, el exceso de caudal irá derivado a un depósito de tormenta que se ubicará al final de la red. Este depósito cumplirá con la función de retener las aguas en exceso. Esta conexión se realizará a través de un aliviadero ubicado en el actual pozo P_11 (que deberá ser modificado).

Un depósito anti-DSU, también conocido como depósito/tanque de tormenta, es una infraestructura diseñada para almacenar las primeras aguas pluviales, que suelen ser las más contaminadas, evitando que lleguen a ríos o sistemas de saneamiento. Su objetivo principal es prevenir la contaminación y reducir el riesgo de inundaciones.

Tanto el depósito de tormentas, como sus aliviaderos y sistema de impulsión, se encuentran incluidos en un proyecto aparte. En el presente proyecto, el pozo de conexión P_11 no contempla la conexión al depósito.

5. Cálculo y modelización del sistema de saneamiento y drenaje

5.1. Modelización de los SUDS

La modelización de los SUDS se ha realizado teniendo en cuenta los siguientes objetivos:

- Aquellos SUDS que conectan con el canal del antiguo cauce, deben garantizar un nivel de tratamiento suficiente de la escorrentía, al tiempo que reducen el caudal pico para garantizar vertidos controlados al cauce. Por ello, se modelarán de forma que su volumen de almacenamiento garantice que el vertido al cauce se produzca a caudal natural.
- Aquellos SUDS que conecten con la red de colectores, deben reducir los caudales pico que alcanzan el sistema, para ayudar a mejorar su funcionamiento y proporcionar una mayor resiliencia. Se utilizará el almacenamiento superficial, la retención en sustratos y el riego pasivo, como mecanismos para la reducción de estos caudales. Por ello, se modelarán para un percentil volumétrico mínimo de V_{80}, si bien, se optarán por volúmenes mayores en aquellas zonas que lo permitan.

5.1.1. Predimensionamiento

Como primer paso en el diseño de los SUDS deberá comprobarse que los tipos de SUDS seleccionados poseen una capacidad de remediación suficiente para tratar debidamente las aguas que reciban,

especialmente, en aquellas zonas donde se produce un vertido a cauce. Para ello se empleará el método de los índices previamente introducido en el apartado 3.3.2

Tabla 10. Índices de peligrosidad de contaminación en función de los usos del suelo para los principales usos considerados en la actuación.

Uso del suelo	Riesgo de contaminación	SST	M	HC
Tejados o cubiertas en una atmósfera limpia.	Bajo	0,2	0,2	0,05
Caminos o viales con intensidades de tráfico muy débiles. Zonas de aparcamiento residenciales. Espacios comunes de zonas residenciales de menos de 50 viviendas. Zonas de estacionamiento con poca renovación.	Bajo	0,5	0,4	0,4
Zonas de estacionamiento con renovación media. Zonas residenciales con poco tráfico.	Medio	0,7	0,6	0,7
SST: Sólidos suspendidos totales. M: Metales pesados. HC: Hidrocarburos				

Tabla 11. Índices de mitigación de contaminación en función de la tipología de SUDS para los principales usos considerados en la actuación.

Tipología SUDS	SST	M	HC
Jardines de lluvia	0,6	0,5	0,6
Áreas de biorretención	0,8	0,8	0,8
Pavimentos permeables	0,7	0,6	0,7

Se puede observar que los SUDS escogidos, son capaces de gestionar la peligrosidad de las zonas consideradas en la actuación.

Seguidamente, se establece un criterio de diseño para el predimensionamiento basado en los percentiles volumétricos. Este criterio permite de un modo simplificado, obtener los volúmenes de almacenamiento necesarios en los SUDS a partir de la cuenca que van a gestionar. Empleando los percentiles volumétricos previamente introducidos en el apartado 3.2.3, se puede obtener un volumen de almacenamiento necesario para gestionar determinado percentil, y trasladarlo a una ocupación de área necesaria.

Teniendo en cuenta la pendiente existente, se pueden ajustar las superficies de los SUDS, para asegurar que el volumen que pueden almacenar es suficiente para la gestión del percentil considerado.

La Tabla 12 resume los cálculos realizados y muestra los volúmenes asociados a los percentiles volumétricos que debe contener cada uno de los SUDS atendiendo a su cuenca vertiente. En función de la geometría de los parterres (depresión superficial útil entre 20 y 30 cm), pendiente longitudinal, taludes y represas necesarias, se obtiene una estimación del volumen de escorrentía que son capaces de almacenar en superficie. En todos los casos se obtiene valores superiores al V_{80}, mientras que, en las zonas verdes y amplias, se busca dimensionar para reducir el caudal saliente al caudal natural.

Tabla 12. Volumen de almacenamiento necesario para cada subcuenca y disponible en cada SUDS propuesto.

Ref. SUDS	Superficie impermeable equivalente (m^2)	V_{80}	V_{90}	V_{95}	V_{Qnat}	Volumen total (m^3)
			SUDS en viales			
JLL1	298,1	**6,0**	11,0	17,9	21,0	**8,2**
JLL2	347,7	**7,0**	12,9	20,9	24,5	**6,8**
JLL3	459,6	**9,2**	17,0	27,6	32,4	**9,6**
JLL4	311,6	**6,2**	11,5	18,7	21,9	**9,6**
JLL5	314,7	**6,3**	11,6	18,9	22,2	**9,6**
JLL6	384,6	**7,7**	14,2	23,1	27,1	**10,8**
JLL7	361,6	**7,2**	13,4	21,7	25,5	**9,6**
JLL8	311,7	**6,2**	11,5	18,7	21,9	**9,6**
JLL9	314,6	**6,3**	11,6	18,9	22,1	**9,6**
JLL10	366,8	**7,3**	13,6	22,0	25,8	**8,3**
JLL11	649,7	13,0	**24,0**	39,0	45,7	**36,0**
JLL12	270,5	**5,4**	10,0	16,2	19,0	**6,0**
JLL13	149,9	3,0	**5,5**	9,0	10,6	**6,4**
JLL14	219,7	4,4	**8,1**	13,2	15,5	**9,6**
JLL15	248,0	5,0	**9,2**	14,9	17,5	**9,6**
JLL16	248,0	5,0	**9,2**	14,9	17,5	**9,6**
JLL17	248,0	5,0	**9,2**	14,9	17,5	**9,6**
JLL18	317,7	**6,4**	11,8	19,1	22,4	**9,6**
JLL19	248,0	5,0	**9,2**	14,9	17,5	**9,6**
JLL20	248,0	5,0	**9,2**	14,9	17,5	**9,6**
JLL21	176,0	**3,5**	6,5	10,6	12,4	**6,3**
JLL22	754,7	**15,1**	27,9	45,3	53,1	**16,3**
JLL23	486,1	**9,7**	18,0	29,2	34,2	**13,2**
JLL24	355,6	**7,1**	13,2	21,3	25,0	**13,0**
JLL25	261,9	**5,2**	9,7	15,7	18,4	**7,8**
JLL26	260,2	**5,2**	9,6	15,6	18,3	**8,6**
JLL27	260,0	**5,2**	9,6	15,6	18,3	**8,6**
JLL28	293,2	**5,9**	10,8	17,6	20,6	**8,6**
JLL29	428,0	8,6	15,8	25,7	30,1	**7,6**
JLL30	523,7	**10,5**	19,4	31,4	36,9	**11,6**
JLL31	340,8	**6,8**	12,6	20,4	24,0	**9,6**
JLL32	338,0	**6,8**	12,5	20,3	23,8	**9,6**
JLL33	295,0	**5,9**	10,9	17,7	20,8	**9,6**

JLL34	306,1	**6,1**	11,3	18,4	21,6	**9,6**
JLL35	582,5	**11,6**	21,6	34,9	41,0	**13,6**
JLL36	690,2	**13,8**	25,5	41,4	48,6	**13,9**
JLL37	461,3	**9,2**	17,1	27,7	32,5	**11,1**
JLL38	375,3	**7,5**	13,9	22,5	26,4	**10,6**
JLL39	561,2	11,2	**20,8**	33,7	39,5	**23,1**
JLL40	941,1	18,8	**34,8**	56,5	66,3	**38,2**
JLL41	562,1	**11,2**	20,8	33,7	39,6	**17,6**
JLL42	472,9	**9,5**	17,5	28,4	33,3	**14,3**
JLL43	580,1	**11,6**	21,5	34,8	40,8	**14,5**
JLL44	788,0	**15,8**	29,2	47,3	55,5	**28,6**
JLL45	535,7	**10,7**	19,8	32,1	37,7	**15,7**
JLL46	486,5	9,7	**18,0**	29,2	34,2	**28,7**
JLL47	710,2	**14,2**	26,3	42,6	50,0	**18,8**
JLL48	636,6	12,7	**23,6**	38,2	44,8	**25,7**
JLL49	529,5	**10,6**	19,6	31,8	37,3	**11,4**
JLL50	380,0	7,6	**14,1**	22,8	26,8	**17,8**
JLL55	139,5	2,8	5,2	8,4	**9,8**	**30,5**
JLL56	335,3	6,7	12,4	20,1	**23,6**	**31,6**
JLL57	306,3	6,1	11,3	18,4	**21,6**	**31,6**
JLL58	162,8	3,3	6,0	9,8	**11,5**	**15,8**
JLL59	684,3	13,7	**25,3**	41,1	48,2	**28,6**
JLL60	242,1	**4,8**	9,0	14,5	17,0	**7,9**
JLL61	225,6	**4,5**	8,3	13,5	15,9	**7,4**
JLL62	269,3	**5,4**	10,0	16,2	19,0	**6,8**
JLL63	260,9	**5,2**	9,7	15,7	18,4	**6,8**
JLL64	266,7	**5,3**	9,9	16,0	18,8	**6,8**
JLL65	229,7	**4,6**	8,5	13,8	16,2	**4,7**
ZBIO1	2.778,1	**55,6**	102,8	166,7	195,6	**66,4**

Ref. SUDS	Superficie impermeable equivalente (m^2)	V_{80}	V_{90}	V_{95}	V_{Qnat}	Volumen total (m^3)
			SUDS en zonas verdes amplias			
BJLL1	1.328,6	26,6	49,2	79,7	**93,5**	**113,2**
BJLL2	1.084,2	21,7	40,1	65,1	**76,3**	**81,0**
BJLL3	413,7	8,3	15,3	24,8	**29,1**	**32,8**

BJLL4	804,9	16,1	29,8	48,3	**56,7**	**297,9**
BJLL5	506,7	10,1	18,7	30,4	**35,7**	**187,9**
BJLL6	406,2	8,1	15,0	24,4	**28,6**	**48,8**
BJLL7	298,2	6,0	11,0	17,9	**21,0**	**25,1**
BJLL8	642,8	12,9	23,8	38,6	**45,3**	**183,1**
BJLL9	735,9	14,7	27,2	44,2	**51,8**	**230,7**
BJLL10	665,1	13,3	24,6	39,9	**46,8**	**177,0**
BJLL11	1.814,4	36,3	67,1	108,9	**127,7**	**526,1**
BJLL12	473,7	9,5	17,5	28,4	**33,3**	**188,8**
BJLL13	1.518,0	30,4	56,2	91,1	**106,9**	**483,6**
BJLL14	976,7	19,5	36,1	58,6	**68,8**	**408,4**
BJLL15	1.458,3	29,2	54,0	87,5	**102,7**	**287,9**
BJLL16	898,8	18,0	33,3	53,9	**63,3**	**279,5**
BJLL17	376,2	7,5	13,9	22,6	**26,5**	**69,9**
BJLL18	994,8	19,9	36,8	59,7	**70,0**	**172,0**
BJLL19	883,2	17,7	32,7	53,0	**62,2**	**279,2**
BJLL20	835,2	16,7	30,9	50,1	**58,8**	**110,8**
BJLL21	1.772,1	35,4	65,6	106,3	**124,8**	**142,0**
BJLL22	2.599,6	52,0	96,2	**156,0**	183,0	**171,0**
BJLL23	1.071,3	21,4	39,6	64,3	**75,4**	**86,5**
BJLL24	993,3	19,9	36,8	59,6	**69,9**	**91,5**
BJLL25	835,2	16,7	30,9	50,1	**58,8**	**121,0**
BJLL26	1.808,4	36,2	66,9	108,5	**127,3**	**186,6**
BJLL27	449,1	9,0	16,6	26,9	**31,6**	**31,7**

En el caso de los pavimentos permeables, el predimensionamiento responde a un criterio de intensidades de tratamiento como se establece en el apartado 3.3.2. De acuerdo con la intensidad máxima del evento de T25 según la Ordenanza, y la permeabilidad máxima del pavimento permeable establece, del lado de la seguridad, una relación 2:1 que establece que una parte de pavimento permeable puede drenar hasta dos partes de zona impermeable.

Tabla 13. Relación cuenca impermeable frente a cuenca de pavimento permeable propuesto.

Elemento SUDS	Cuenca Impermeable (m^2)	Cuenca Pavimento Permeable (m^2)	Relación
PP1	586,47	216,33	1,7
PP2	847,42	307,70	1,8
PP3-1	622,70	234,10	1,7
PP3-2	824,12	307,80	1,7

PP4	906,47	312,50	1,9
PP5-1	886,41	346,10	1,6
PP5-2	351,25	121,80	1,9
PP6-1	686,46	255,00	1,7
PP6-2	618,24	245,50	1,5
PP7	427,48	220,70	0,9
PP8	608,58	304,00	1,0
PP9-1	449,16	233,70	0,9
PP9-2	610,20	307,90	1,0
PP10	664,08	312,20	1,1
PP11-1	649,76	349,80	0,9
PP11-2	258,49	118,40	1,2
PP12	966,58	501,00	0,9

5.1.2. Dimensionamiento y cálculo

Si bien, el predimensionamiento de los SUDS permite realizar un primer tanteo de los volúmenes de almacenamiento, es necesario de desarrollar un modelo hidrológico-hidráulico que permita analizar el desempeño de los elementos de drenaje con un mayor grado de detalle. Para ello, se utilizan herramientas de modelación matemática del comportamiento hidrológico-hidráulico del sistema de drenaje propuesto.

Con este objetivo, se empleará el software especializado en drenaje sostenible InfoDrainage (Autodesk), que es la evolución más reciente del programa MicroDrainage, muy utilizado en el Reino Unido, y que ha sufrido un proceso de desarrollo y transformación con el paso del tiempo.

El programa utiliza las ecuaciones hidráulicas e hidrológicas tradicionales (Manning, onda dinámica, acumulación y lavado de contaminantes, etc.) para simular el comportamiento de la escorrentía en cuencas urbanas. Además, la herramienta permite definir a nivel de detalle cada uno de los SUDS propuestos, de modo que se reproduzcan las condiciones de proyecto. Adicionalmente, este software permite una buena integración con herramientas CAD, lo que permite importar y exportar información de manera eficiente, y contribuye a generar modelos que representen adecuadamente la realidad geométrica de la propuesta. Además, ofrece una interfaz gráfica eficiente de visualización de datos, y permite la exportación de resultados en múltiples formatos.

Para la construcción del modelo se irán introduciendo progresivamente en el programa los distintos elementos que componen la estrategia de drenaje para buscar que este pueda reproducir el comportamiento global del sistema cuando se ve sometido a distintos escenarios. Esencialmente el modelo se compone de cuencas drenantes, estructuras de control (SUDS), tuberías y pozos de registro, que presentan un gran número de parámetros (dimensiones, cotas, porosidades...) para buscar que su comportamiento se ajuste al del elemento finalmente construido.

En primer lugar, se introducen en el modelo las subcuencas en las que se ha subdivido el aparcamiento para determinar que superficie será drenada por cada uno de los elementos de la estrategia de drenaje. Además de indicar su geometría 2D se introducen los coeficientes de escorrentía considerados en los criterios de diseño para cada tipo de superficie.

Una vez definidas las subcuencas, se introduce en el modelo la geometría de los distintos tramos de pavimento permeable, jardines de lluvia, y áreas de biorretención numerándolos de acuerdo con la planta mostrada en el plano UR2717-PC-DR-508011-HE-Drenaje_planta-D01. A continuación, para cada uno de los SUDS deberán introducirse una serie de parámetros que permitirán al programa conocer como es la sección transversal de los sistemas propuestos y poder reproducir su comportamiento adecuadamente. Dichos parámetros se introducen mediante la interfaz gráfica que se presenta en la Figura 23, la cual presenta un ejemplo de los parámetros requeridos para un área de biorretención. En primera instancia se definen las dimensiones y características físicas de los SUDS (área, cotas, taludes, porosidad, etc.), buscando en todos los casos que dicha definición geométrica de las estructuras reproduzca fidedignamente las secciones constructivas del proyecto. Cabe destacar que el programa es capaz de leer automáticamente las cotas de la superficie del terreno y establecer adecuadamente las pendientes longitudinales de los elementos, si previamente se ha introducido un modelo digital de elevaciones.

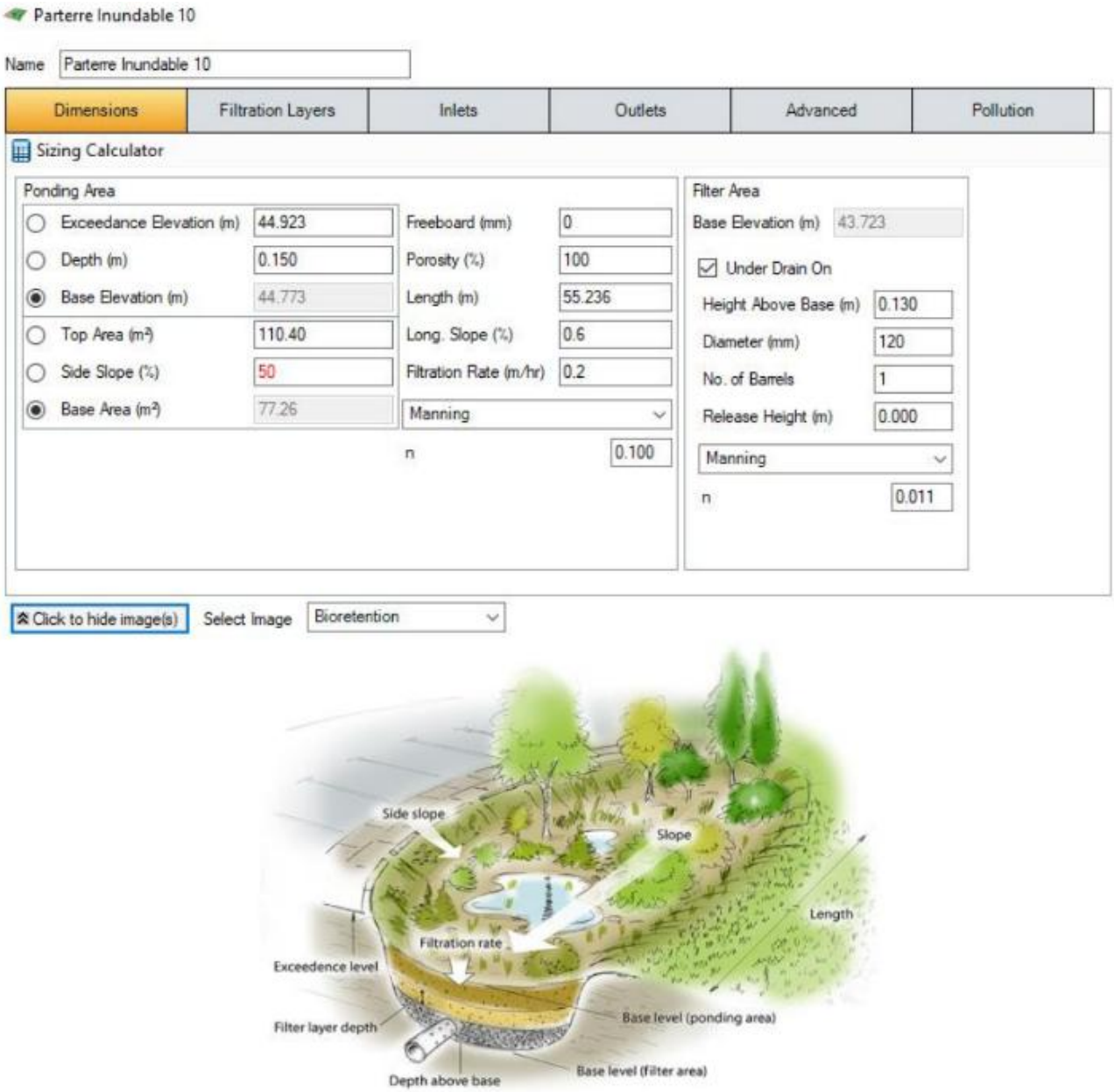


Figura 23. Ejemplo de interfaz de introducción de parámetros de diseño de un área de biorretención en InfoDrainage.

En paralelo al diseño de los SUDS; deben definirse las redes de colectores que conectan las salidas y los reboses de los SUDS hasta el vertido el cauce, o su conexión con la red de drenaje convencional. InfoDrainage también permite el diseño de redes de colectores, así como facilitar su visualización en forma de perfiles longitudinales dinámicos.

A modo de ejemplo, se muestra el perfil longitudinal del ramal 5.X situado en la zona 4 (ver apartado 4.3.2). que recoge los tubos dren y reboses del pavimento permeable y los jardines de lluvia situados en esa zona. Para él, se emplea tubería de PEAD corrugado con diámetro nominal entre 400 mm y 600 mm. Como criterio general, se ha empleado una distancia mínima a clave de tubería de 1 m y una pendiente mínima del 0,4 %.

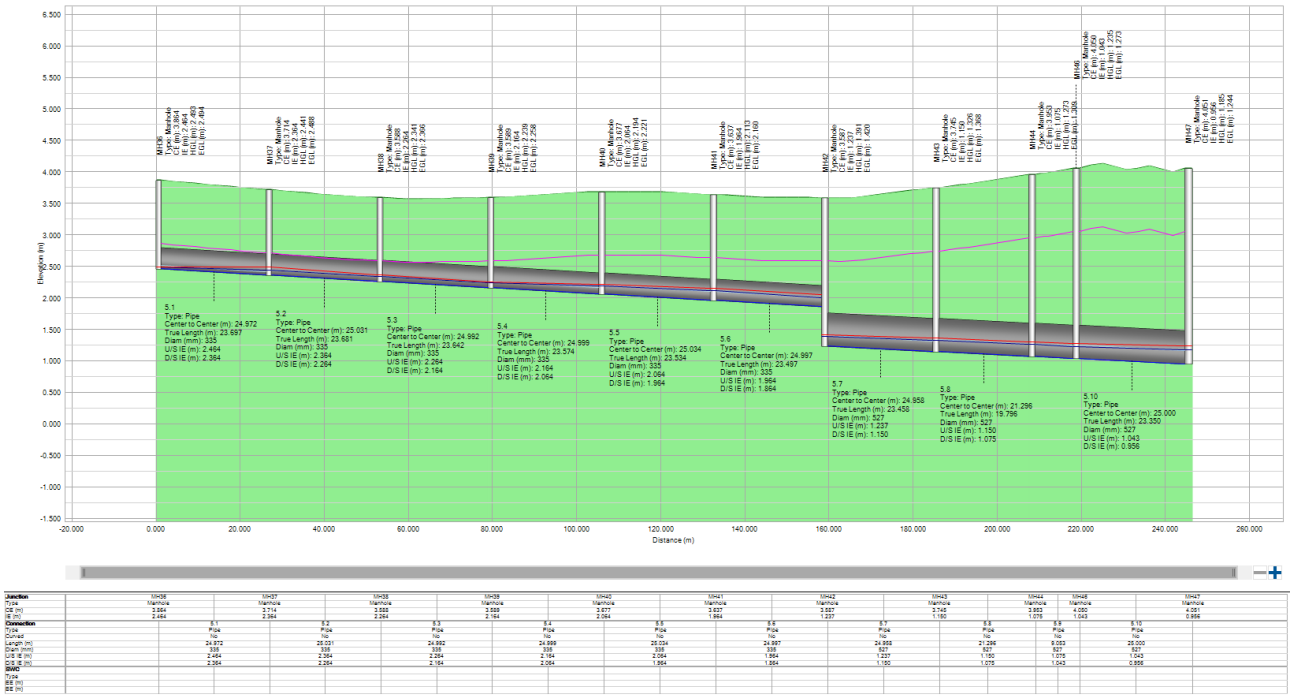


Figura 24. Perfil longitudinal de colector propuesto en ramal 5.X en InfoDrainage.

5.1.3. Simulación de las lluvias de diseño

Completada la construcción del modelo se procederá a la simulación de los eventos pluviométricos deseados. De acuerdo con la Ordenanza, se realizará la simulación de las tormentas de acuerdo con la curva IDF de Valencia para T25 años, presentada en el apartado 3.2.1.

Para las simulaciones se verifican los siguientes criterios:

- Capacidad suficiente en almacenamiento y colectores para garantizar el correcto funcionamiento del sistema de drenaje.
- Vaciado de elementos de laminación en menos de 48 horas (gestión de eventos sucesivos).
- En el caso de los SUDS que vierten al cauce, caudal vertido inferior al valor estimado del caudal preurbanizado.
- Comportamiento de la red separativa de pluviales.

5.1.4. Análisis de resultados y caudales vertidos fuera del ámbito

Los resultados completos de la simulación pueden consultarse en el Apéndice 2: Resultados de la Modelización: SUDS. Los resultados de la simulación muestran que el diseño funciona de manera satisfactoria, sin inundación para todos los episodios de lluvia analizados.

T25 Valencia: Increase Rainfall (%): +0: Critical Storm Per Item

Stormwater Control	Storm Event	Max. US Elevation (m)	Max. DS Elevation (m)	Max. US Depth (m)	Max. DS Depth (m)	Max. Inflow (L/s)	Max. Resident Volume (m³)	Max. Flooded Volume (m³)	Total Lost Volume (m³)	Max. Outflow (L/s)	Total Discharge Volume (m³)	Percentage Available (%)	Status
JLL55	T25 Valencia: +0 %: T25 Valencia90	2.919	2.716	0.200	0.200	2.0	13.106	0.000	0.000	0.3	2.825	92	OK
JLL56	T25 Valencia: +0 %: T25 Valencia90	3.412	2.924	0.200	0.200	4.9	32.423	0.000	0.000	0.4	3.712	92	OK
JLL57	T25 Valencia: +0 %: T25 Valencia90	3.336	2.891	0.200	0.200	4.5	29.536	0.000	0.000	0.4	3.593	92	OK
JLL58	T25 Valencia: +0 %: T25 Valencia90	2.909	2.670	0.200	0.200	2.4	15.420	0.000	0.000	0.3	2.940	92	OK
JLL2	T25 Valencia: +0 %: T25 Valencia20	3.479	3.469	0.660	0.776	11.0	6.910	0.000	0.000	10.7	9.822	46	OK
JLL1	T25 Valencia: +0 %: T25 Valencia30	3.167	3.161	0.652	0.771	8.2	7.165	0.000	0.000	8.0	10.673	48	OK
JLL3	T25 Valencia: +0 %: T25 Valencia20	3.809	3.799	0.728	0.781	14.6	9.116	0.000	0.000	14.2	12.308	34	OK
JLL4	T25 Valencia: +0 %: T25 Valencia30	3.655	3.652	0.713	0.772	8.5	8.569	0.000	0.000	8.3	9.942	38	OK
JLL5	T25 Valencia: +0 %: T25 Valencia30	3.518	3.514	0.713	0.772	8.6	8.579	0.000	0.000	8.4	10.103	38	OK
JLL6	T25 Valencia: +0 %: T25 Valencia30	3.367	3.361	0.709	0.775	10.6	10.001	0.000	0.000	10.3	12.754	38	OK
JLL7	T25 Valencia: +0 %: T25 Valencia30	3.199	3.194	0.716	0.774	9.9	8.727	0.000	0.000	9.7	12.416	37	OK
JLL8	T25 Valencia: +0 %: T25 Valencia30	3.058	3.054	0.713	0.772	8.6	8.570	0.000	0.000	8.3	9.958	38	OK
JLL9	T25 Valencia: +0 %: T25 Valencia30	3.024	3.019	0.714	0.772	8.6	8.615	0.000	0.000	8.4	10.066	38	OK
JLL10	T25 Valencia: +0 %: T25 Valencia20	3.049	3.041	0.676	0.777	11.6	7.460	0.000	0.000	11.3	10.037	44	OK
JLL22	T25 Valencia: +0 %: T25 Valencia90	3.560	3.538	0.555	0.778	11.1	16.316	0.000	0.000	11.0	58.526	49	OK
JLL23	T25 Valencia: +0 %: T25 Valencia45	3.572	3.563	0.612	0.685	11.1	7.434	0.000	0.000	10.8	29.285	59	OK
JLL11	T25 Valencia: +0 %: T25 Valencia90	3.156	3.152	0.586	0.771	9.6	39.681	0.000	0.000	9.0	33.566	40	OK
JLL12	T25 Valencia: +0 %: T25 Valencia20	3.468	3.447	0.567	0.772	8.6	5.465	0.000	0.000	8.3	8.014	60	OK
JLL13	T25 Valencia: +0 %: T25 Valencia30	3.878	3.878	0.722	0.763	4.1	5.314	0.000	0.000	4.0	3.894	39	OK
JLL14	T25 Valencia: +0 %: T25 Valencia45	3.943	3.942	0.703	0.764	5.0	8.254	0.000	0.000	4.9	10.950	40	OK
JLL15	T25 Valencia: +0 %: T25 Valencia30	3.818	3.815	0.708	0.768	6.8	8.346	0.000	0.000	6.5	6.824	40	OK
JLL16	T25 Valencia: +0 %: T25 Valencia30	3.668	3.665	0.708	0.768	6.8	8.346	0.000	0.000	6.5	6.824	40	OK
JLL17	T25 Valencia: +0 %: T25 Valencia30	3.496	3.494	0.708	0.768	6.8	8.346	0.000	0.000	6.5	6.824	40	OK
JLL18	T25 Valencia: +0 %: T25 Valencia30	3.315	3.311	0.713	0.772	8.7	8.585	0.000	0.000	8.5	10.263	38	OK
JLL19	T25 Valencia: +0 %: T25 Valencia30	3.182	3.179	0.708	0.768	6.8	8.346	0.000	0.000	6.5	6.824	40	OK
JLL20	T25 Valencia: +0 %: T25 Valencia30	3.157	3.154	0.708	0.768	6.8	8.346	0.000	0.000	6.5	6.824	40	OK
JLL21	T25 Valencia: +0 %: T25 Valencia30	3.212	3.212	0.713	0.764	4.8	5.201	0.000	0.000	4.8	5.337	40	OK
JLL25	T25 Valencia: +0 %: T25 Valencia30	3.907	3.904	0.718	0.769	7.2	6.794	0.000	0.000	7.1	8.558	39	OK
JLL26	T25 Valencia: +0 %: T25 Valencia30	3.866	3.863	0.717	0.769	7.1	7.497	0.000	0.000	7.0	8.046	38	OK
JLL27	T25 Valencia: +0 %: T25 Valencia30	3.877	3.876	0.716	0.769	7.1	7.485	0.000	0.000	7.0	8.040	38	OK

Figura 25. Ejemplo de resultados para evento crítico del conjunto de SUDS incluidos en el modelo extraído del APÉNDICE 2. RESULTADOS DE LA MODELIZACIÓN: SUDS.

A modo de resumen, se indican algunos de los aspectos más relevantes:

- A nivel de ámbito, la colocación de SUDS genera las siguientes reducciones en caudales punta (Tabla 13). Es especialmente relevante la aportación para reducir los caudales pico de las tormentas más cortas e intensas con atenuaciones superiores al 80 %.

Tabla 14. Laminación de los caudales punta generada por los SUDS para diferentes eventos de diseño.

Evento	Caudal de entrada (l/s)	Caudal de salida (l/s)	Reducción (%)
T25: 10 minutos	1.622,6	288,1	82,2
T25: 15 minutos	1.498,4	534,9	64,3
T25: 20 minutos	1.388,8	677,6	51,2
T25: 30 minutos	1.202,6	731,2	39,2
T25: 45 minutos	996,9	697,9	30,0
T25: 60 minutos	853,3	644,4	24,5
T25: 75 minutos	745,0	592,4	20,5
T25: 90 minutos	645,0	535,6	17,0

- Analizando particularmente, la cuenca que drena hacia el antiguo cauce (aproximadamente con una superficie de 4,25 ha). Empleando el método racional, podemos realizar una comparativa entre el modelo de cálculo y las situaciones preurbanizadas (caudal natural) y posturbanizadas, empleando diferentes coeficientes de escorrentía:
    - Situación preurbanizada: coeficiente de escorrentía asociado a una zona permeable 0,3
    - Situación posturbanizada: coeficiente de escorrentía 0,7
    - Situación posturbanizada con el uso de SUDS: empleando los resultados de la salida del modelo hidráulico (coeficiente de escorrentia aproximado 0.5).

Tabla 15. Laminación de los caudales punta generada por los SUDS para diferentes eventos de diseño.

-	Caudal (l/s)	Evento crítico
Caudal pre-urbanizado (l/s)	472,7	T25: 10 minutos
Caudal post-urbanizado (l/s)	1102,9	T25: 10 minutos
Caudal post-urbanizado con SUDS (l/s)	442,5	T25: 30 minutos

Analizando los tres escenarios, observamos un cambio en el evento crítico, debido a la laminación que los SUDS proporcionan. Esta laminación sucede dado que la escorrentía tiene que atravesar el cuerpo de los SUDS (y en el caso de los jardines de lluvia, el medio granular), hasta alcanzar el tubo de desagüe, favoreciendo el almacenamiento en superficie. Como consecuencia, la curva de caudales resulta más gradual, y se favorece la reducción de los caudales picos.

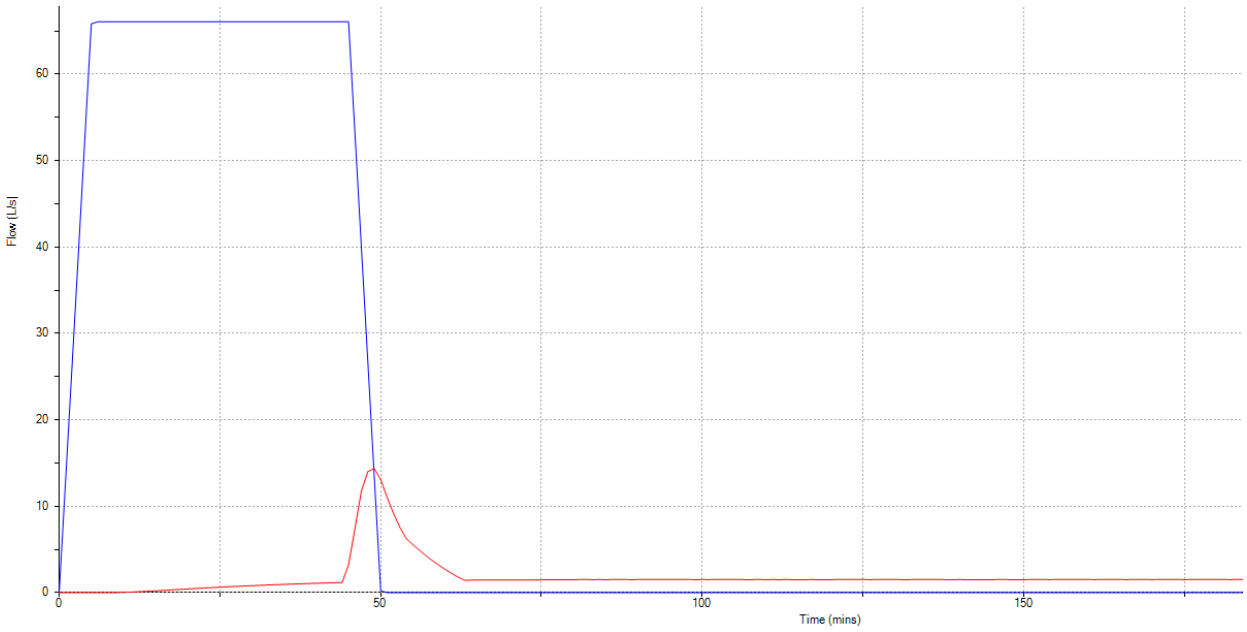


Figura 26. Ejemplo de atenuación en jardín de lluvia BJLL-4 para la tormenta de T25 45 minutos.
Entradas de escorrentía en azul, salidas de escorrentía en rojo.

En tercer lugar, se analiza el tiempo de vaciado de los SUDS. Este indicador es relevante, para garantizar el funcionamiento del sistema frente a eventos sucesivos, así como para evitar que exista volumen de agua almacenado en superficie después de 48 horas, que pueda favorecer la proliferación de insectos.

A modo de presentación, se muestran los resultados para los jardines de lluvia de mayores dimensiones situados en la Zona 1, de acuerdo con la Figura 16.

Tabla 16. Tiempos de vaciado para jardines de lluvia en zona 1.

SUDS	Evento crítico	Máx. calado (m)	Tiempo de vaciado (min)
BJLL-1	T25 30 minutos	0,034	27
BJLL-2	T25 30 minutos	0,073	36
BJLL-3	T25 75 minutos	0,157	162
BJLL-4	T25 75 minutos	0,375	875
BJLL-5	T25 30 minutos	0,320	658
BJLL-6	T25 30 minutos	0,080	57
BJLL-7	T25 30 minutos	0,033	25
BJLL-8	T25 30 minutos	0,055	39
BJLL-9	T25 45 minutos	0,094	74
BJLL-10	T25 45 minutos	0,092	72
BJLL-11	T25 45 minutos	0,111	111

Se puede observar que el calado en los jardines de lluvia es muy reducido, lo que se debe especialmente a que al mismo tiempo que se produce el llenado de los SUDS, la escorrentía comienza a percolar de forma subsuperficial a través del medio filtrante (100 mm/h), contribuyendo a una situación de entrada y salida de caudal simultánea.

A la vista de los resultados, aquellos jardines de lluvia con un mayor grado de llenado, tienen tiempos de vaciado que se sitúan por encima de las 10 horas (600 minutos), pero en ningún caso alcanzan las 24 o 48 horas. Esto garantiza el vaciado de los elementos, así como su gestión de eventos sucesivos.

Por último, se analiza el funcionamiento de los colectores de la red de pluviales, comprobando que su funcionamiento es adecuado para los eventos considerados. Analizando, por ejemplo, el ramal 5.x () se

observan que los resultados son adecuados para toda la red, y que no se producen reboses de la misma para el evento crítico de período de retorno 25 años.

T25 Valencia: Increase Rainfall (%): +0: Critical Storm Per Item

Connection	Storm Event	Connection Type	From	To	Upstream Cover Elevation (m)	Max. US Water Elevation (m)	Max. Flow Depth (m)	Discharge Volume (m³)	Max. Velocity (m/s)	Flow / Capacity	Max. Flow (L/s)	Status
5.1	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH36	MH37	3.864	2.534	0.091	12.013	0.5	0.1	9.4	OK
5.2	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH37	MH38	3.714	2.476	0.123	41.618	0.8	0.22	21.6	OK
5.3	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH38	MH39	3.588	2.398	0.144	52.016	0.8	0.3	29.0	OK
5.4	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH39	MH40	3.589	2.319	0.173	62.801	0.8	0.38	36.4	OK
5.5	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH40	MH41	3.677	2.256	0.198	111.800	1.2	0.53	62.8	OK
5.6	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH41	MH42	3.637	2.118	0.196	123.350	1.3	0.6	71.7	OK

Figura 27. Ejemplo de resultados para el ramal 5.X extraído desde InfoDrainage.

En resumen, la modelación hidrológico-hidráulica permite demostrar que los SUDS y redes de colectores propuestas son capaces de gestionar las escorrentías asociadas a los episodios de lluvia de periodos de retorno de diseño, sin exceder la limitación de vertido establecida, y sin causar inundación en ningún punto de la red.

El comportamiento de todos los SUDS introducidos en el modelo es correcto y de los resultados se desprende el cumplimiento de todos los criterios de diseño marcados.

El informe de resultados completo extraído del programa se incluye en el Apéndice 2, distinguiéndose los siguientes apartados:

- Datos y parámetros de entrada de los SUDS.
    - Jardines de lluvia y áreas de biorretención
    - Pavimentos permeables
- Datos y parámetros de las conducciones
- Datos y parámetros de los pozos
- Resultados para la lluvia crítica de volumen contenido para cada uno de los SUDS.
- Resultados para la lluvia crítica de caudal trasegado para cada uno de los pozos.

Cabe destacar que si bien una parte de los SUDS descargan al cauce existente, los SUDS situados en zona 2 y 3, descargan sobre la red de drenaje convencional. Para considerar la situación más desfavorable, la atenuación proporcionada por los SUDS; no se ha considerado dentro del análisis de la red de drenaje convencional.

5.2. Modelización de la red de colectores unitarios de saneamiento y drenaje

A continuación, se describe la red unitaria de colectores proyectada en lo que se refiere a la topología de esta, el área drenada y el cálculo hidráulico resultante.

5.2.1. Nomenclatura

Se ha mantenido la nomenclatura utilizada en el proyecto anterior de modo que la variación realizada a algunos ramales no ha supuesto una modificación en el nombre de los pozos afectados.

En el caso de la nueva tubería de residuales se extiende hasta el pozo del aliviadero ALIV01 y el resto de los pozos se han nombrado Rj (j = 01, 02, 03,...,46), enumerando todos los pozos situados cada 25 m correlativamente.

5.2.2. Topología de la red

La red de saneamiento proyectada adopta un esquema ramificado estructurado en ramales principales, que canalizan los caudales hacia los puntos de vertido definidos, y ramales secundarios, encargados de recoger las aportaciones distribuidas de la urbanización y conducirlas hasta los principales.

Ramales principales

Los ramales principales están formados por conducciones de mayor diámetro y capacidad hidráulica, diseñadas para transportar los caudales máximos generados bajo condiciones de tormenta de diseño con un período de retorno de 25 años, según la Normativa para obras de saneamiento y drenaje urbano del Ayuntamiento de Valencia (2015). Estas conducciones recorren los ejes viales estructurantes (Avenida de Francia, Alameda y calle Ejército Español) y desembocan en puntos de vertido estratégicos, como el aliviadero existente o la estación de bombeo de Cantarranas, considerando que, en caso de tormenta, previo a la estación de bombeo el exceso de volumen será retenido en un depósito de tormenta.

Cada ramal principal ha sido definido con sección uniforme (generalmente de tipo circular) y cotas adaptadas al relieve y al trazado urbano, asegurando pendientes mínimas compatibles con velocidades autolimpiantes y evitando, en la medida de lo posible, sobrecargas en la red. Los ramales A y B concentran la mayor parte del caudal del sector, habiéndose dispuesto pozos de registro con interdistancias aproximadas de 25 metros, facilitando su inspección y mantenimiento.

Ramales secundarios

Los ramales secundarios recogen las escorrentías de las distintas subcuencas generadas por superficies pavimentadas, cubiertas, viales y zonas dotacionales. Están conectados transversalmente a los principales y discurren, por lo general, por el interior de los viales secundarios. Estas conducciones presentan diámetros menores (normalmente 400–600 mm en PVC o PEAD corrugado) y han sido diseñadas para condiciones de caudal medio y caudal punta, considerando un coeficiente de escorrentía medio de 0,85.

Para la caracterización hidráulica de la red, se ha empleado el software InfoWorks ICM, modelando cada ramal mediante elementos tipo “link” entre nodos (pozos),

Los ramales unitarios integran el drenaje tanto de aguas residuales como de pluviales, con prioridad en la evacuación de éstas últimas mediante dispositivos de captación puntual (sumideros tipo Valencia, arquetas de clapeta) distribuidos en las zonas bajas de la topografía.

En zonas verdes y cubiertas vegetadas, se han previsto soluciones basadas en SUDS (zanjas drenantes, depósitos de infiltración) cuya aportación a la red se considera minoritaria o nula.

5.2.3. Construcción del modelo hidráulico

Datos de precipitación:

Para el diseño de la red de drenaje de aguas pluviales, es necesario caracterizar el régimen de precipitaciones de la zona mediante la curva Intensidad – Duración – Frecuencia correspondiente al período de retorno que se adopte para dimensionar la infraestructura, en nuestro caso 25 años, cumpliendo las condiciones exigidas en la normativa municipal de Valencia.

Un análisis detallado se puede encontrar en el apartado 3.2 selección de datos pluviométricos

Datos de la red de colectores

En INFOWORKS, los datos que definen la red se introducen en forma de tablas. Las redes se definen mediante dos tablas: una para los nudos o pozos y otra para los elementos de unión ("links") o conducciones.

La caracterización básica pasa por definir los siguientes datos:

Nodos (manholes, junctions, outfalls, storage nodes)

- POZOS: coordenadas (X, Y), cota de terreno (trapa), cota de solera de pozo.
- TRAMOS: pozo inicial, pozo final, sección, cota solera aguas arriba, cota solera aguas abajo, longitud, rugosidad.
- Cuencas tributarias, Se han delimitado las subcuencas drenantes a los puntos de entrada en la red. En el apéndice 1 se adjunta el plano de subcuencas, identificando los puntos (pozos) de entrada en la red.

A continuación, se adjunta una explicación de cada uno de los campos más importantes de las tres tablas fundamentales: pozos, tramos y subcuencas.

Nodos (manholes, junctions, outfalls, storage nodes)

ID	X	Y	GroundLevel	US_Invert	NodeType
Identificador único del nodo ✅ **NOD001**	Coordenadas (o usar la geometría del shapefile) ✅ 593210, 1912234		Nivel del terreno (en m) ✅ (si no hay DTM) 105.50	Cota de solera del nodo ✅ 104.00	Tipo (e.g. manhole, outfall, storage) ✅ manhole

Conducciones (conduits, pipes, culverts)

ID	FromNode	ToNode	US_Invert	DS_Invert	Diameter	Shape	Roughness
Identificador del conducto ✅ **PIPE001**	ID del nodo de inicio ✅ NOD001	ID del nodo final ✅ NOD002	Cota de solera al inicio ✅ 104.00	Cota de solera al final ✅ 103.80	Diámetro interno (en m o mm, según config.) ✅ 0.6	Forma de la sección (circular, rectangular, etc.) ✅ circular	Coeficiente de rugosidad (ej. n de Manning) ✅ 0.013

Subcuencas (subcatchments)

ID	Outlet	Area	Imperv	Slope	Width	InfilMethod
Identificador único ✅ **SC001**	ID del nodo receptor ✅ MH001	Área de la subcuenca (en m² o ha, según config.) ✅ 800.0	% de área impermeable ✅ 60.0	Pendiente media (%) ✅ 2.5	Ancho efectivo de escurrimiento (m) ✅ 20.0	Método de infiltración (horton, green_ampt) ✅ horton

Para la organización de los cálculos estos fueros agrupados en 4 tramos en los que cada uno contenía ramales principales y secundarios a continuación se muestran las figuras de estos cuatro tramos:

Figura 28. Tramo A

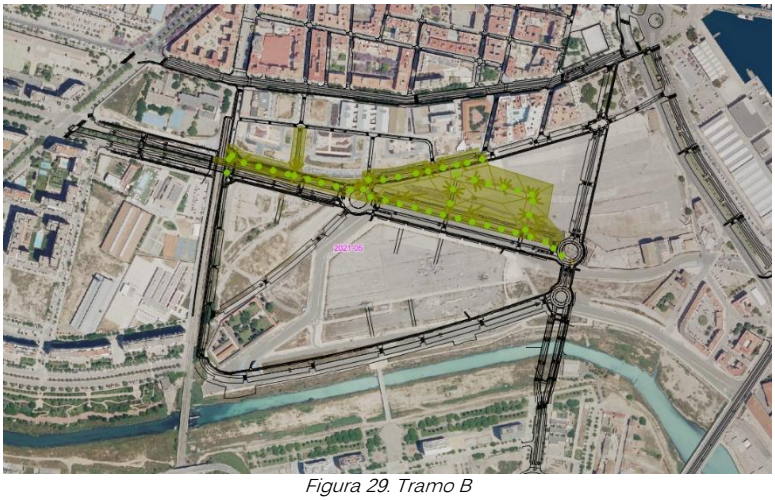


Figura 29. Tramo B

Figura 30. Tramo C

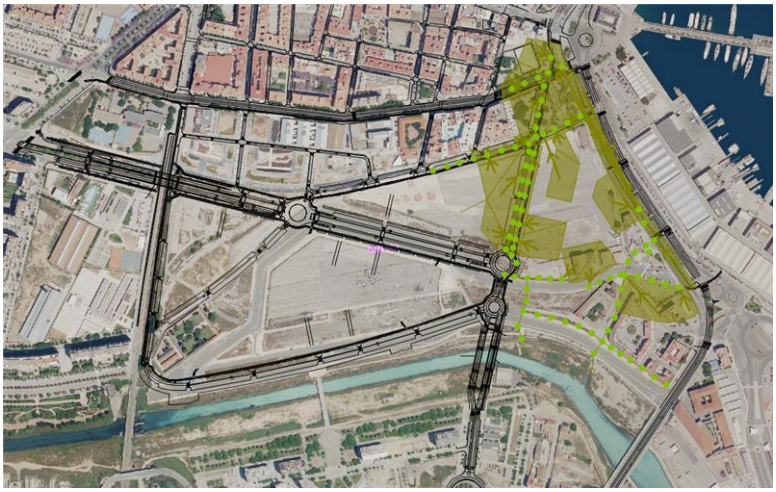


Figura 31. Tramo D

5.2.4. Análisis de resultados y caudales vertidos fuera del ámbito

Los resultados completos de la simulación pueden consultarse en el Apéndice 1: Resultados de la Modelización: en Infoworks. Los resultados de la simulación muestran que el diseño funciona de manera satisfactoria, sin inundación para todos los episodios de lluvia analizados.

5.2.5. Calculo sumideros en pasos superiores

Para el drenaje de los pasos superiores se han calculado las superficies drenantes y la distancia entre sumideros en cada una de las estructuras en función del caudal y las pendientes tanto transversal como longitudinal. A continuación, se incluye el cálculo del caudal de cada una de las estructuras y el caudal interceptado por sumidero.

Estructura	TRAMO (m)	Pendiente longitudinal del tramo (m/m)	Tiempo de concentración (min)	Ancho calzada (m)	Coeficiente de escorrentia	Intensidad media de precipitación (T=25 años) (mm/h)	a	b	Kp	Qtramo (l/s)
Puente Turia-Tablero Oeste	48	0.03	10.00	9	0.95	133.30	15.855	-0.145	1.10	16.73
Puente Turia-Tablero Oeste	48	0.01	10.00	9	0.95	133.30	15.855	-0.145	1.10	16.73
Puente Turia-Tablero Este	48	0.03	10.00	11.8	0.95	133.30	15.855	-0.145	1.10	21.93
Puente Turia-Tablero Este	48	0.01	10.00	11.8	0.95	133.30	15.855	-0.145	1.10	21.93

Estructura	TRAMO (m)	Pendiente longitudinal del tramo (m/m)	Tiempo de concentración (min)	Ancho calzada (m)	Coeficiente de escorrentia	Intensidad media de precipitación (T=25 años) (mm/h)	a	b	Kp	Qtramo (l/s)
Puente FFCC-Lado izquierdo	41	0.005	10.00	11	0.95	133.30	15.855	-0.145	1.10	17.46
Puente FFCC-Lado derecho	41	0.005	10.00	11	0.95	133.30	15.855	-0.145	1.10	17.46

Figura 32. Cálculo del caudal en cada una de las estructuras

A continuación, se incluye el cálculo del caudal interceptado en cada uno de los sumideros empleando la metodología de "Urban Drainage Design Manuel" implementado en el software Hydraulic tools v4.4 (FHWA) para su diseño, en función de la pendiente longitudinal, pendiente trasversal, dimensiones de la reja y caudal generado en la superficie drenante; se disponen sumideros de 30 cm x 30 cm de fundición dúctil:

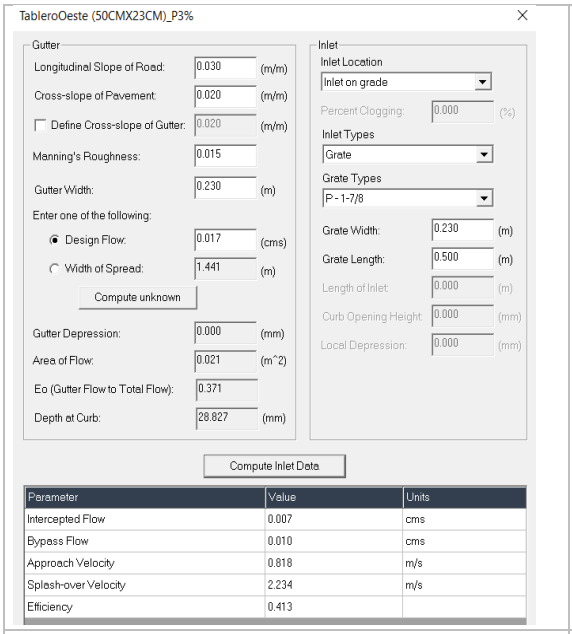


Figura 33. Caudal captado por sumidero en tablero Oeste (p 3%)

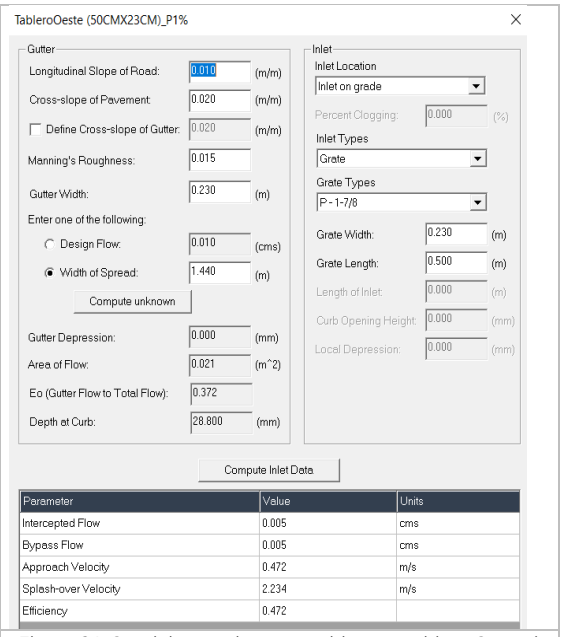


Figura 34. Caudal captado por sumidero en tablero Oeste (p 1%)

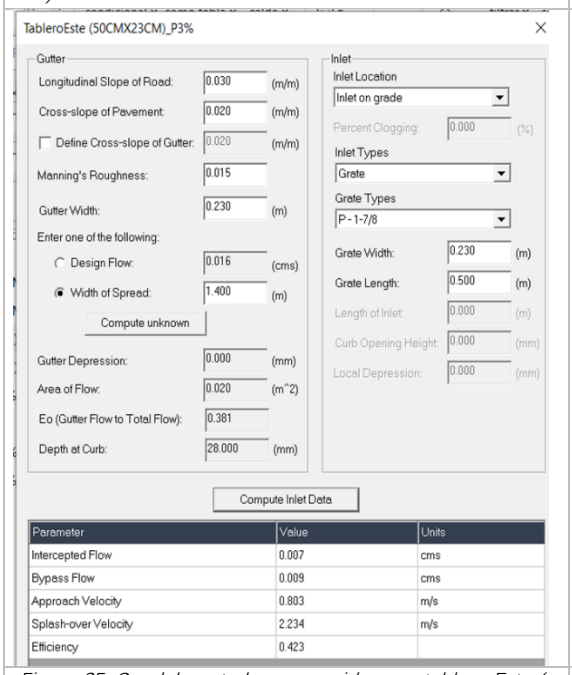


Figura 35. Caudal captado por sumidero en tablero Este (p 3%)

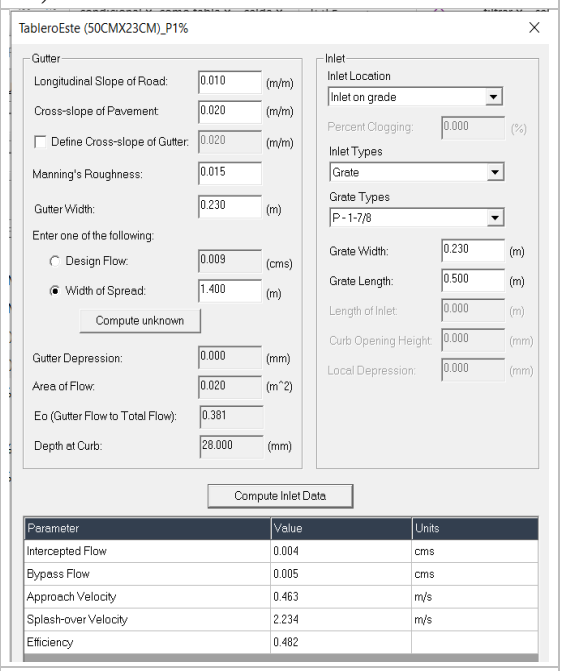


Figura 36. Caudal captado por sumidero en tablero Este (p 1%)

Estructura	Pendiente longitudinal del tramo (m/m)	Q sumidero (l/s)	Nº sumideros	Separación entre sumideros (m)
Puente Turia-Tablero Oeste	0.03	7	2	24
Puente Turia-Tablero Oeste	0.01	5	3	16
Puente Turia-Tablero Este	0.03	7	3	16
Puente Turia-Tablero Este	0.01	4	5	10

Figura 37. Resumen de caudales captados por los sumideros y separación entre ellos en la estructura sobre el río Turia

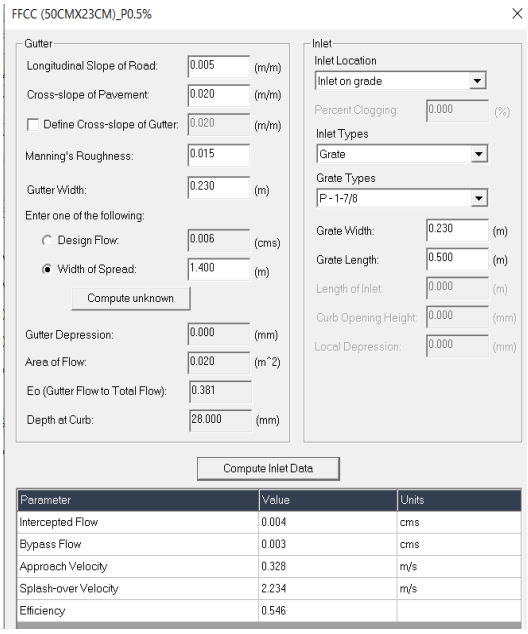


Figura 38. Caudal captado por sumidero en tablero sobre vías de FFCC (p 0.5%)

Estructura	Pendiente longitudinal del tramo (m/m)	Q sumidero (l/s)	Nº sumideros	Separación entre sumideros (m)
Puente FFCC-Lado izquierdo	0.005	4	4	10
Puente FFCC-Lado derecho	0.005	4	4	10

Figura 39. Resumen de caudales captados por los sumideros y separación entre ellos en la estructura sobre las vías de FFCC

6. Conclusiones

En el presente documento se describen las soluciones de saneamiento y drenaje propuestas de las obras de urbanización del Sector Grao con el empleo de Sistemas Urbanos de Drenaje Sostenible (SUDS).

El sistema de drenaje propuesto para la zona de estudio tiene como objetivo principal gestionar las aguas de escorrentía desde el origen, favoreciendo la retención, disminuyendo y laminando el caudal de escorrentía que accede a la red de saneamiento existente, mejorando así, la resiliencia del sistema. Por otro lado, la escorrentía generada en zonas cercanas al antiguo cauce, con cota suficiente para su descarga por gravedad, será conducida hacia este punto, disminuyendo los caudales que alcanzar la red de colectores.

Por todo ello, se propone que la escorrentía de la zona se gestione en origen de manera sostenible con el empleo de técnicas SUDS; en este caso mediante una combinación de jardines de lluvia y pavimentos permeables. La captación en los SUDS garantiza un tratamiento adecuado para la escorrentía, además de reducir los caudales pico.

Como criterio de diseño general se busca laminar lo máximo posible los caudales de escorrentía vertidos a la red de saneamiento existente, fuertemente congestionada en la zona; y asegurar un adecuado tratamiento de los caudales que se vierten al cauce.

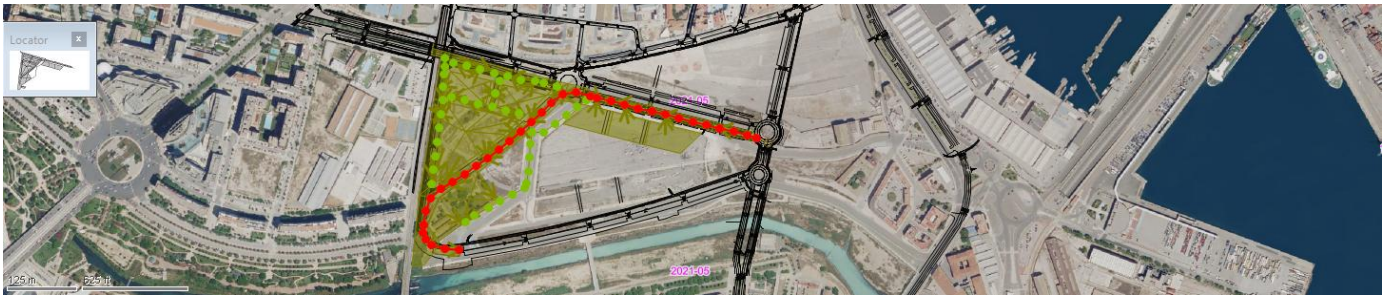
La elaboración de un modelo hidrológico-hidráulico de detalle ha permitido comprobar que la estrategia de drenaje propuesta plantea una reducción muy importante de los caudales pico vertidos, sin provocar inundaciones en ningún punto de la red.

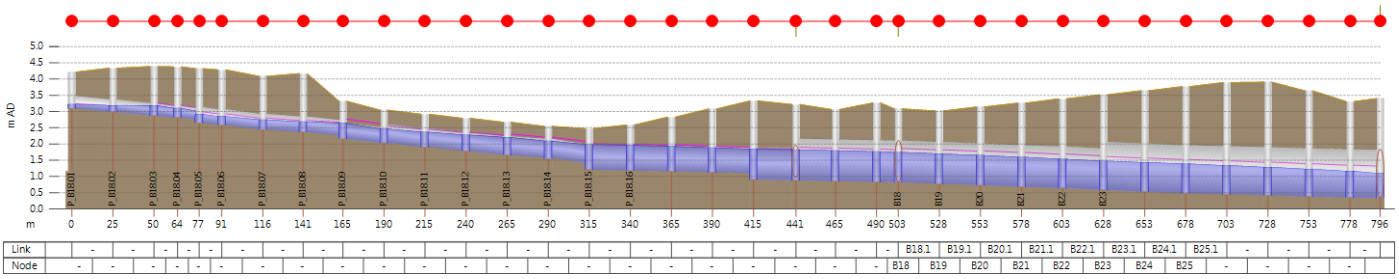
El resto se recoge en la red unitaria de saneamiento y drenaje convencional propuesta, ramificada en ramales secundarios y principales por todo el ámbito de la urbanización e integrando en lo posible la red existente en el ámbito en la actualidad.

APÉNDICE 1: RESULTADOS MODELIZACIÓN

APÉNDICE 2: RESULTADOS MODELIZACIÓN SUDS

TRAMO A





	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
0:05:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
0:10:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
0:15:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
0:20:00	0.076	0.00051	0.023	0.416	0.016	0.00058	0.05	0.077	0.00071	0.032	0.427	0.022	0	0	0.6
0:25:00	0.091	0.00847	0.26	0.433	0.195	0.0009	0.06	0.097	0.00975	0.256	0.449	0.201	0	0	0.8
0:30:00	0.123	0.02971	0.476	0.473	0.431	0.00126	0.09	0.136	0.03214	0.422	0.495	0.402	0	0	1.4
0:35:00	0.167	0.07028	0.617	0.529	0.652	0.00156	0.12	0.186	0.07257	0.517	0.553	0.577	0	0	2.2
0:40:00	0.191	0.09906	0.666	0.56	0.755	0.00168	0.14	0.212	0.10002	0.548	0.584	0.656	0	0	2.6
0:45:00	0.199	0.10876	0.674	0.57	0.781	0.0017	0.15	0.22	0.10901	0.554	0.594	0.676	0	0	2.8
0:50:00	0.201	0.11126	0.676	0.573	0.787	0.0017	0.15	0.222	0.11126	0.555	0.596	0.681	0	0	2.8
0:55:00	0.202	0.11175	0.677	0.573	0.788	0.0017	0.15	0.223	0.11176	0.555	0.597	0.682	0	0	2.8
1:00:00	0.202	0.11186	0.677	0.573	0.789	0.0017	0.15	0.223	0.11186	0.555	0.597	0.682	0	0	2.8
1:05:00	0.202	0.11281	0.678	0.574	0.792	0.00171	0.15	0.224	0.11291	0.557	0.598	0.685	0	0	2.8
1:10:00	0.205	0.11707	0.683	0.578	0.804	0.00173	0.15	0.227	0.11736	0.562	0.602	0.697	0	0	2.9
1:15:00	0.21	0.1245	0.69	0.585	0.822	0.00175	0.16	0.233	0.12435	0.568	0.608	0.713	0	0	3
1:20:00	0.215	0.12973	0.695	0.59	0.837	0.00177	0.16	0.237	0.12994	0.572	0.614	0.725	0	0	3.1
1:25:00	0.216	0.13245	0.697	0.593	0.843	0.00177	0.16	0.239	0.13253	0.574	0.616	0.731	0	0	3.1
1:30:00	0.217	0.13336	0.698	0.594	0.845	0.00178	0.16	0.24	0.13338	0.574	0.617	0.732	0	0	3.1
1:35:00	0.217	0.1336	0.698	0.594	0.845	0.00178	0.16	0.24	0.1336	0.574	0.617	0.733	0	0	3.1
1:40:00	0.217	0.13365	0.698	0.594	0.845	0.00178	0.16	0.24	0.13365	0.574	0.617	0.733	0	0	3.1
1:45:00	0.217	0.1336	0.698	0.594	0.845	0.00178	0.16	0.24	0.13366	0.574	0.617	0.733	0	0	3.1
1:50:00	0.217	0.13366	0.698	0.594	0.845	0.00178	0.16	0.24	0.13366	0.574	0.617	0.733	0	0	3.1
1:55:00	0.217	0.13366	0.698	0.594	0.845	0.00178	0.16	0.24	0.13366	0.574	0.617	0.733	0	0	3.1
2:00:00	0.217	0.13366	0.698	0.594	0.845	0.00178	0.16	0.24	0.13366	0.574	0.617	0.733	0	0	3.1
2:05:00	0.218	0.13506	0.7	0.595	0.849	0.00178	0.16	0.241	0.13522	0.576	0.619	0.737	0	0	3.2
2:10:00	0.222	0.14136	0.706	0.601	0.865	0.00181	0.16	0.245	0.14176	0.582	0.624	0.752	0	0	3.2
2:15:00	0.229	0.15115	0.713	0.609	0.888	0.00183	0.17	0.252	0.15158	0.59	0.633	0.772	0	0	3.4

2:20:00	0.234	0.15855	0.718	0.615	0.903	0.00185	0.17	0.258	0.15879	0.594	0.639	0.786	0	0	3.5
2:25:00	0.236	0.16179	0.72	0.618	0.91	0.00186	0.17	0.26	0.16188	0.595	0.642	0.791	0	0	3.5
2:30:00	0.236	0.1628	0.72	0.619	0.912	0.00186	0.17	0.261	0.16283	0.595	0.643	0.793	0	0	3.5
2:35:00	0.237	0.16306	0.72	0.619	0.912	0.00186	0.17	0.261	0.16306	0.595	0.643	0.793	0	0	3.5
2:40:00	0.237	0.16312	0.72	0.619	0.912	0.00186	0.17	0.261	0.16312	0.595	0.643	0.793	0	0	3.5
2:45:00	0.237	0.16313	0.72	0.619	0.912	0.00186	0.17	0.261	0.16313	0.595	0.643	0.793	0	0	3.5
2:50:00	0.237	0.16313	0.72	0.619	0.912	0.00186	0.17	0.261	0.16313	0.595	0.643	0.793	0	0	3.5
2:55:00	0.237	0.16313	0.72	0.619	0.912	0.00186	0.17	0.261	0.16313	0.595	0.643	0.793	0	0	3.5
3:00:00	0.237	0.16313	0.72	0.619	0.912	0.00186	0.17	0.261	0.16313	0.595	0.643	0.793	0	0	3.5
3:05:00	0.238	0.16539	0.722	0.621	0.918	0.00187	0.17	0.262	0.16562	0.598	0.645	0.799	0	0	3.6
3:10:00	0.244	0.17526	0.73	0.629	0.939	0.0019	0.18	0.269	0.17583	0.605	0.653	0.819	0	0	3.7
3:15:00	0.252	0.18968	0.738	0.64	0.967	0.00193	0.19	0.278	0.19025	0.613	0.664	0.845	0	0	3.9
3:20:00	0.258	0.19953	0.742	0.648	0.984	0.00195	0.19	0.284	0.19981	0.617	0.672	0.86	0	0	4
3:25:00	0.261	0.20346	0.744	0.651	0.99	0.00195	0.19	0.286	0.20355	0.618	0.674	0.865	0	0	4.1
3:30:00	0.261	0.20461	0.744	0.651	0.992	0.00195	0.19	0.287	0.20463	0.619	0.675	0.867	0	0	4.1
3:35:00	0.261	0.20489	0.744	0.652	0.993	0.00195	0.19	0.287	0.20489	0.619	0.675	0.867	0	0	4.1
3:40:00	0.261	0.20495	0.744	0.652	0.993	0.00195	0.19	0.287	0.20495	0.619	0.676	0.867	0	0	4.1
3:45:00	0.261	0.20496	0.744	0.652	0.993	0.00195	0.19	0.287	0.20496	0.619	0.676	0.867	0	0	4.1
3:50:00	0.261	0.20496	0.744	0.652	0.993	0.00195	0.19	0.287	0.20496	0.619	0.676	0.867	0	0	4.1
3:55:00	0.261	0.20497	0.744	0.652	0.993	0.00195	0.19	0.287	0.20497	0.619	0.676	0.867	0	0	4.1
4:00:00	0.261	0.20497	0.744	0.652	0.993	0.00195	0.19	0.287	0.20497	0.619	0.676	0.867	0	0	4.1
4:05:00	0.263	0.2089	0.747	0.654	1.001	0.00197	0.19	0.29	0.20927	0.622	0.679	0.875	0	0	4.1
4:10:00	0.272	0.22543	0.756	0.666	1.03	0.00201	0.2	0.299	0.22629	0.632	0.691	0.904	0	0	4.3
4:15:00	0.284	0.24761	0.765	0.682	1.065	0.00204	0.21	0.311	0.24837	0.64	0.706	0.936	0	0	4.6
4:20:00	0.291	0.26098	0.769	0.691	1.084	0.00206	0.21	0.319	0.26131	0.644	0.715	0.953	0	0	4.7
4:25:00	0.293	0.26582	0.77	0.694	1.091	0.00206	0.21	0.321	0.26592	0.645	0.718	0.958	0	0	4.8
4:30:00	0.294	0.26714	0.77	0.695	1.092	0.00206	0.21	0.322	0.26717	0.645	0.719	0.96	0	0	4.8
4:35:00	0.294	0.26745	0.77	0.695	1.093	0.00206	0.21	0.322	0.26746	0.645	0.719	0.96	0	0	4.8
4:40:00	0.294	0.26752	0.77	0.695	1.093	0.00207	0.21	0.322	0.26752	0.645	0.719	0.96	0	0	4.8
4:45:00	0.294	0.26753	0.77	0.695	1.093	0.00207	0.21	0.322	0.26753	0.645	0.719	0.96	0	0	4.8
4:50:00	0.294	0.26754	0.77	0.695	1.093	0.00207	0.21	0.322	0.26754	0.645	0.719	0.96	0	0	4.8
4:55:00	0.294	0.26754	0.77	0.695	1.093	0.00207	0.21	0.322	0.26754	0.645	0.719	0.96	0	0	4.8
5:00:00	0.294	0.26754	0.77	0.695	1.093	0.00207	0.21	0.322	0.26754	0.645	0.719	0.96	0	0	4.8
5:05:00	0.298	0.27511	0.774	0.7	1.105	0.00209	0.22	0.326	0.27574	0.649	0.724	0.973	0	0	4.9
5:10:00	0.312	0.30523	0.785	0.719	1.148	0.00214	0.23	0.341	0.30662	0.662	0.744	1.015	0	0	5.2
5:15:00	0.328	0.34116	0.793	0.741	1.193	0.00218	0.24	0.358	0.34219	0.671	0.765	1.057	0	0	5.6
5:20:00	0.337	0.35983	0.796	0.752	1.213	0.0022	0.24	0.367	0.36022	0.674	0.776	1.075	0	0	5.8
5:25:00	0.339	0.36588	0.797	0.755	1.22	0.0022	0.25	0.37	0.36599	0.674	0.779	1.081	0	0	5.9
5:30:00	0.34	0.36744	0.797	0.756	1.221	0.0022	0.25	0.37	0.36746	0.674	0.78	1.082	0	0	5.9
5:35:00	0.34	0.36779	0.797	0.756	1.222	0.0022	0.25	0.371	0.36785	0.674	0.78	1.082	0	0	5.9
5:40:00	0.34	0.36787	0.797	0.756	1.222	0.0022	0.25	0.371	0.36787	0.674	0.78	1.082	0	0	5.9
5:45:00	0.34	0.36789	0.797	0.756	1.222	0.0022	0.25	0.371	0.36789	0.674	0.78	1.082	0	0	5.9
5:50:00	0.34	0.36789	0.797	0.756	1.222	0.0022	0.25	0.371	0.36789	0.674	0.78	1.082	0	0	5.9
5:55:00	0.34	0.36789	0.797	0.756	1.222	0.0022	0.25	0.371	0.36789	0.674	0.78	1.082	0	0	5.9
6:00:00	0.34	0.36789	0.797	0.756	1.222	0.0022	0.25	0.371	0.36789	0.674	0.78	1.082	0	0	5.9

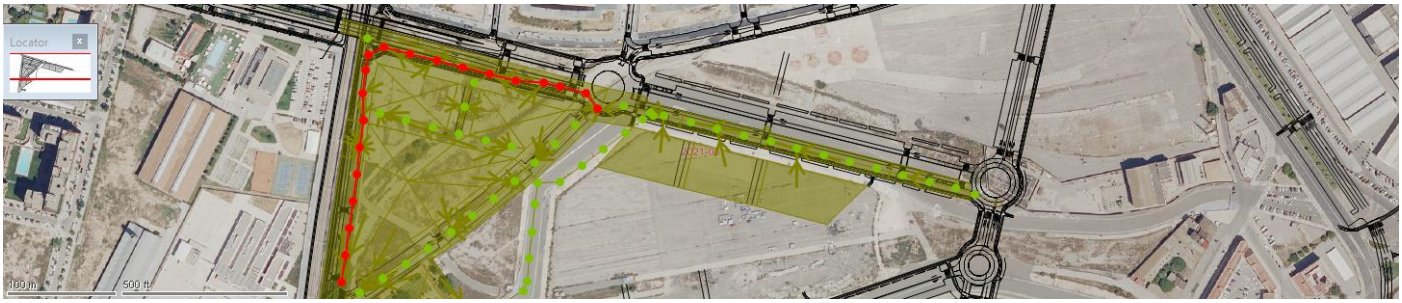
6:05:00	0.347	0.38469	0.803	0.766	1.244	0.00223	0.25	0.378	0.38593	0.682	0.79	1.106	0	0	6.1
6:10:00	0.371	0.44614	0.816	0.799	1.311	0.00231	0.27	0.403	0.44851	0.698	0.823	1.172	0	0	6.7
6:15:00	0.395	0.50814	0.823	0.83	1.367	0.00236	0.29	0.428	0.50956	0.706	0.855	1.225	0	0	7.2
6:20:00	0.405	0.53528	0.825	0.844	1.39	0.00237	0.29	0.439	0.53574	0.708	0.868	1.245	0	0	7.5
6:25:00	0.408	0.54309	0.826	0.847	1.396	0.00238	0.29	0.442	0.54321	0.708	0.871	1.25	0	0	7.6
6:30:00	0.409	0.54498	0.826	0.848	1.397	0.00238	0.29	0.442	0.545	0.708	0.872	1.251	0	0	7.6
6:35:00	0.409	0.5454	0.826	0.849	1.398	0.00238	0.3	0.443	0.5454	0.708	0.872	1.252	0	0	7.6
6:40:00	0.409	0.54549	0.826	0.849	1.398	0.00238	0.3	0.443	0.54549	0.708	0.872	1.252	0	0	7.6
6:45:00	0.409	0.54551	0.826	0.849	1.398	0.00238	0.3	0.443	0.54551	0.708	0.872	1.252	0	0	7.6
6:50:00	0.409	0.54551	0.826	0.849	1.398	0.00238	0.3	0.443	0.54551	0.708	0.873	1.252	0	0	7.6
6:55:00	0.409	0.54551	0.826	0.849	1.398	0.00238	0.3	0.443	0.54551	0.708	0.873	1.252	0	0	7.6
7:00:00	0.409	0.54551	0.826	0.849	1.398	0.00238	0.3	0.443	0.54551	0.708	0.873	1.252	0	0	7.6
7:05:00	0.424	0.59162	0.835	0.87	1.442	0.00243	0.31	0.459	0.59447	0.721	0.895	1.299	0	0	8
7:10:00	0.471	0.73708	0.849	0.934	1.553	0.00254	0.34	0.507	0.74133	0.739	0.959	1.409	0	0	9.2
7:15:00	0.505	0.84976	0.854	0.98	1.624	0.00261	0.36	0.543	0.85171	0.745	1.004	1.475	0	0	10.1
7:20:00	0.518	0.89272	0.855	0.997	1.649	0.00263	0.37	0.556	0.89334	0.746	1.021	1.498	0	0	10.5
7:25:00	0.522	0.90576	0.855	1.002	1.656	0.00263	0.37	0.56	0.90594	0.746	1.026	1.505	0	0	10.6
7:30:00	0.523	0.90948	0.855	1.003	1.658	0.00264	0.37	0.561	0.90953	0.746	1.027	1.507	0	0	10.6
7:35:00	0.523	0.91052	0.855	1.004	1.659	0.00264	0.37	0.562	0.91053	0.746	1.027	1.507	0	0	10.6
7:40:00	0.523	0.91081	0.855	1.004	1.659	0.00264	0.37	0.562	0.91081	0.746	1.028	1.507	0	0	10.6
7:45:00	0.524	0.91089	0.855	1.004	1.659	0.00264	0.37	0.562	0.91089	0.746	1.028	1.507	0	0	10.6
7:50:00	0.524	0.91091	0.855	1.004	1.659	0.00264	0.37	0.562	0.91091	0.746	1.028	1.507	0	0	10.6
7:55:00	0.524	0.91092	0.855	1.004	1.659	0.00264	0.37	0.562	0.91092	0.746	1.028	1.507	0	0	10.6
8:00:00	0.524	0.91092	0.855	1.004	1.659	0.00264	0.37	0.562	0.91092	0.746	1.028	1.507	0	0	10.6
8:05:00	0.568	1.08552	0.87	1.068	1.769	0.00276	0.41	0.609	1.09383	0.768	1.093	1.625	0	0	11.8
8:10:00	0.667	1.49321	0.879	1.204	1.965	0.00298	0.47	0.712	1.50087	0.781	1.23	1.816	0	0	14.6
8:15:00	0.722	1.73459	0.879	1.278	2.063	0.0031	0.51	0.768	1.73772	0.781	1.304	1.907	0	0	16.1
8:20:00	0.742	1.82972	0.879	1.307	2.099	0.00315	0.53	0.79	1.83086	0.781	1.332	1.941	0	0	16.7
8:25:00	0.75	1.86514	0.879	1.317	2.112	0.00316	0.53	0.798	1.86556	0.781	1.342	1.953	0	0	16.9
8:30:00	0.753	1.87833	0.879	1.321	2.117	0.00317	0.53	0.801	1.87849	0.781	1.346	1.958	0	0	17
8:35:00	0.754	1.88332	0.879	1.322	2.118	0.00317	0.53	0.802	1.88338	0.781	1.347	1.959	0	0	17
8:40:00	0.754	1.88521	0.879	1.323	2.119	0.00317	0.53	0.802	1.88523	0.781	1.348	1.96	0	0	17
8:45:00	0.754	1.88592	0.879	1.323	2.119	0.00317	0.53	0.802	1.88593	0.781	1.348	1.96	0	0	17
8:50:00	0.754	1.8862	0.879	1.323	2.119	0.00317	0.53	0.802	1.8862	0.781	1.348	1.96	0	0	17
8:55:00	0.754	1.8863	0.879	1.323	2.119	0.00317	0.53	0.802	1.8863	0.781	1.348	1.96	0	0	17
9:00:00	0.754	1.88634	0.879	1.323	2.119	0.00317	0.53	0.802	1.88634	0.781	1.348	1.96	0	0	17
9:05:00	0.729	1.75895	0.875	1.286	2.065	0.0031	0.52	0.776	1.75468	0.775	1.31	1.903	0	0	16.3
9:10:00	0.677	1.52336	0.871	1.214	1.966	0.00297	0.48	0.722	1.51888	0.769	1.238	1.805	0	0	14.8
9:15:00	0.641	1.36841	0.869	1.165	1.898	0.00289	0.46	0.684	1.36604	0.766	1.189	1.74	0	0	13.8
9:20:00	0.625	1.30137	0.869	1.143	1.868	0.00286	0.44	0.667	1.30044	0.766	1.167	1.712	0	0	13.4
9:25:00	0.619	1.27719	0.869	1.135	1.856	0.00284	0.44	0.661	1.27687	0.765	1.159	1.701	0	0	13.2
9:30:00	0.617	1.26909	0.869	1.132	1.853	0.00284	0.44	0.659	1.26898	0.765	1.156	1.698	0	0	13.2
9:35:00	0.616	1.26644	0.869	1.131	1.852	0.00284	0.44	0.658	1.26641	0.765	1.155	1.697	0	0	13.1
9:40:00	0.616	1.26559	0.869	1.131	1.851	0.00284	0.44	0.658	1.26557	0.765	1.155	1.696	0	0	13.1
9:45:00	0.616	1.26531	0.869	1.131	1.851	0.00284	0.44	0.658	1.2653	0.765	1.155	1.696	0	0	13.1

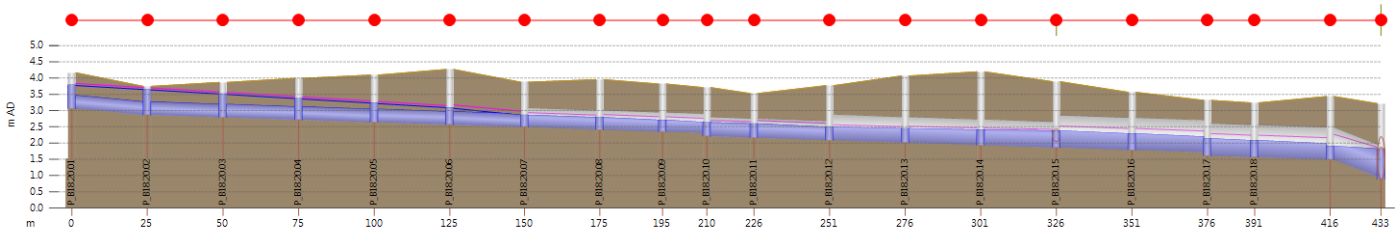
9:50:00	0.616	1.26522	0.869	1.131	1.851	0.00284	0.44	0.658	1.26522	0.765	1.155	1.696	0	0	13.1
9:55:00	0.616	1.26519	0.869	1.131	1.851	0.00284	0.44	0.658	1.26519	0.765	1.155	1.696	0	0	13.1
10:00:00	0.616	1.26518	0.869	1.131	1.851	0.00284	0.44	0.658	1.26518	0.765	1.155	1.696	0	0	13.1
10:05:00	0.592	1.165	0.862	1.097	1.796	0.00277	0.42	0.633	1.16084	0.756	1.12	1.637	0	0	12.5
10:10:00	0.536	0.9482	0.851	1.018	1.674	0.00264	0.38	0.574	0.943	0.741	1.041	1.516	0	0	10.9
10:15:00	0.49	0.79228	0.844	0.957	1.579	0.00255	0.35	0.527	0.78935	0.732	0.98	1.425	0	0	9.7
10:20:00	0.469	0.72428	0.842	0.929	1.535	0.00251	0.34	0.505	0.72316	0.728	0.952	1.384	0	0	9.1
10:25:00	0.461	0.70187	0.841	0.919	1.52	0.0025	0.33	0.497	0.70147	0.727	0.943	1.371	0	0	8.9
10:30:00	0.459	0.69544	0.841	0.916	1.516	0.00249	0.33	0.495	0.69535	0.727	0.94	1.367	0	0	8.9
10:35:00	0.459	0.69376	0.841	0.916	1.515	0.00249	0.33	0.494	0.69373	0.727	0.94	1.366	0	0	8.9
10:40:00	0.459	0.69332	0.841	0.916	1.515	0.00249	0.33	0.494	0.69331	0.727	0.939	1.366	0	0	8.9
10:45:00	0.459	0.69321	0.841	0.915	1.515	0.00249	0.33	0.494	0.6932	0.727	0.939	1.366	0	0	8.9
10:50:00	0.459	0.69318	0.841	0.915	1.515	0.00249	0.33	0.494	0.69318	0.727	0.939	1.366	0	0	8.9
10:55:00	0.459	0.69317	0.841	0.915	1.515	0.00249	0.33	0.494	0.69317	0.727	0.939	1.366	0	0	8.9
11:00:00	0.459	0.69317	0.841	0.915	1.515	0.00249	0.33	0.494	0.69317	0.727	0.939	1.366	0	0	8.9
11:00:00	0.449	0.66056	0.835	0.901	1.487	0.00246	0.32	0.484	0.65877	0.72	0.925	1.337	0	0	8.6
11:10:00	0.419	0.57156	0.824	0.861	1.414	0.00238	0.3	0.453	0.56875	0.706	0.884	1.264	0	0	7.9
11:15:00	0.391	0.49416	0.816	0.824	1.348	0.00232	0.28	0.424	0.49237	0.696	0.847	1.201	0	0	7.1
11:20:00	0.377	0.45863	0.813	0.806	1.316	0.00229	0.27	0.409	0.45796	0.692	0.829	1.172	0	0	6.8
11:25:00	0.373	0.44731	0.812	0.8	1.306	0.00229	0.27	0.405	0.44712	0.691	0.824	1.163	0	0	6.7
11:30:00	0.371	0.44445	0.811	0.798	1.304	0.00229	0.27	0.403	0.44435	0.691	0.822	1.161	0	0	6.7
11:35:00	0.371	0.44373	0.811	0.798	1.303	0.00229	0.27	0.403	0.44372	0.691	0.822	1.16	0	0	6.6
11:40:00	0.371	0.44359	0.811	0.798	1.303	0.00229	0.27	0.403	0.44359	0.691	0.822	1.16	0	0	6.6
11:45:00	0.371	0.44356	0.811	0.798	1.303	0.00229	0.27	0.403	0.44356	0.691	0.822	1.16	0	0	6.6
11:50:00	0.371	0.44356	0.811	0.798	1.303	0.00229	0.27	0.403	0.44356	0.691	0.822	1.16	0	0	6.6
11:55:00	0.371	0.44355	0.811	0.798	1.303	0.00229	0.27	0.403	0.44355	0.691	0.822	1.16	0	0	6.6
12:00:00	0.371	0.44355	0.811	0.798	1.303	0.00229	0.27	0.403	0.44355	0.691	0.822	1.16	0	0	6.6
12:05:00	0.366	0.43047	0.808	0.791	1.288	0.00226	0.27	0.398	0.42959	0.686	0.815	1.144	0	0	6.5
12:10:00	0.349	0.38802	0.798	0.768	1.241	0.00221	0.25	0.38	0.38637	0.675	0.791	1.098	0	0	6.1
12:15:00	0.331	0.34518	0.789	0.743	1.192	0.00216	0.24	0.361	0.34398	0.665	0.767	1.052	0	0	5.7
12:20:00	0.321	0.32256	0.785	0.73	1.166	0.00214	0.23	0.35	0.32205	0.661	0.754	1.028	0	0	5.4
12:25:00	0.317	0.31455	0.784	0.725	1.157	0.00213	0.23	0.346	0.31439	0.66	0.749	1.02	0	0	5.3
12:30:00	0.316	0.31236	0.783	0.724	1.154	0.00213	0.23	0.345	0.31232	0.659	0.748	1.018	0	0	5.3
12:35:00	0.315	0.31184	0.783	0.723	1.153	0.00213	0.23	0.345	0.31183	0.659	0.747	1.017	0	0	5.3
12:40:00	0.315	0.31173	0.783	0.723	1.153	0.00213	0.23	0.344	0.31173	0.659	0.747	1.017	0	0	5.3
12:45:00	0.315	0.31171	0.783	0.723	1.153	0.00213	0.23	0.344	0.31171	0.659	0.747	1.017	0	0	5.3
12:50:00	0.315	0.3117	0.783	0.723	1.153	0.00213	0.23	0.344	0.3117	0.659	0.747	1.017	0	0	5.3
12:55:00	0.315	0.3117	0.783	0.723	1.153	0.00213	0.23	0.344	0.3117	0.659	0.747	1.017	0	0	5.3
13:00:00	0.315	0.3117	0.783	0.723	1.153	0.00213	0.23	0.344	0.3117	0.659	0.747	1.017	0	0	5.3
13:05:00	0.313	0.30548	0.78	0.719	1.144	0.00212	0.23	0.342	0.30499	0.656	0.743	1.008	0	0	5.2
13:10:00	0.302	0.28297	0.772	0.705	1.112	0.00208	0.22	0.33	0.28195	0.647	0.729	0.976	0	0	5
13:15:00	0.29	0.25697	0.764	0.688	1.075	0.00204	0.21	0.317	0.25612	0.638	0.712	0.941	0	0	4.7
13:20:00	0.281	0.24144	0.759	0.678	1.052	0.00202	0.21	0.308	0.24104	0.633	0.702	0.921	0	0	4.5
13:25:00	0.278	0.23542	0.758	0.674	1.043	0.00201	0.2	0.305	0.23528	0.632	0.697	0.914	0	0	4.5
13:30:00	0.277	0.23366	0.757	0.672	1.041	0.00201	0.2	0.304	0.23363	0.632	0.696	0.912	0	0	4.4

13:35:00	0.277	0.23324	0.757	0.672	1.04	0.00201	0.2	0.304	0.23323	0.632	0.696	0.911	0	0	4.4
13:40:00	0.277	0.23314	0.757	0.672	1.04	0.00201	0.2	0.304	0.23314	0.632	0.696	0.911	0	0	4.4
13:45:00	0.277	0.23312	0.757	0.672	1.04	0.00201	0.2	0.304	0.23312	0.632	0.696	0.911	0	0	4.4
13:50:00	0.277	0.23312	0.757	0.672	1.04	0.00201	0.2	0.304	0.23312	0.632	0.696	0.911	0	0	4.4
13:55:00	0.277	0.23312	0.757	0.672	1.04	0.00201	0.2	0.304	0.23312	0.632	0.696	0.911	0	0	4.4
14:00:00	0.277	0.23312	0.757	0.672	1.04	0.00201	0.2	0.304	0.23312	0.632	0.696	0.911	0	0	4.4
14:05:00	0.275	0.22977	0.755	0.67	1.034	0.002	0.2	0.302	0.22947	0.629	0.693	0.905	0	0	4.4
14:10:00	0.268	0.21671	0.748	0.66	1.011	0.00197	0.2	0.294	0.21605	0.622	0.684	0.882	0	0	4.2
14:15:00	0.259	0.19998	0.74	0.648	0.982	0.00193	0.19	0.284	0.19935	0.614	0.672	0.855	0	0	4
14:20:00	0.252	0.18887	0.735	0.64	0.962	0.00191	0.18	0.277	0.18854	0.609	0.663	0.838	0	0	3.9
14:25:00	0.25	0.18418	0.733	0.636	0.954	0.00191	0.18	0.274	0.18406	0.607	0.66	0.831	0	0	3.8
14:30:00	0.249	0.18273	0.732	0.635	0.952	0.0019	0.18	0.274	0.1827	0.607	0.659	0.829	0	0	3.8
14:35:00	0.248	0.18236	0.732	0.634	0.951	0.0019	0.18	0.273	0.18235	0.607	0.658	0.828	0	0	3.8
14:40:00	0.248	0.18228	0.732	0.634	0.951	0.0019	0.18	0.273	0.18228	0.607	0.658	0.828	0	0	3.8
14:45:00	0.248	0.18226	0.732	0.634	0.951	0.0019	0.18	0.273	0.18226	0.607	0.658	0.828	0	0	3.8
14:50:00	0.248	0.18226	0.732	0.634	0.951	0.0019	0.18	0.273	0.18226	0.607	0.658	0.828	0	0	3.8
14:55:00	0.248	0.18226	0.732	0.634	0.951	0.0019	0.18	0.273	0.18226	0.607	0.658	0.828	0	0	3.8
15:00:00	0.248	0.18226	0.732	0.634	0.951	0.0019	0.18	0.273	0.18226	0.607	0.658	0.828	0	0	3.8
15:05:00	0.247	0.18029	0.73	0.633	0.946	0.0019	0.18	0.272	0.18009	0.605	0.657	0.824	0	0	3.8
15:10:00	0.243	0.17217	0.724	0.627	0.929	0.00187	0.18	0.267	0.17171	0.599	0.65	0.807	0	0	3.7
15:15:00	0.236	0.16092	0.717	0.617	0.906	0.00184	0.17	0.259	0.16042	0.592	0.641	0.786	0	0	3.5
15:20:00	0.23	0.15269	0.712	0.61	0.889	0.00182	0.17	0.254	0.15242	0.587	0.634	0.771	0	0	3.4
15:25:00	0.228	0.14895	0.71	0.607	0.881	0.00182	0.17	0.251	0.14885	0.585	0.631	0.764	0	0	3.4
15:30:00	0.227	0.14772	0.709	0.606	0.878	0.00182	0.17	0.25	0.14769	0.585	0.63	0.762	0	0	3.3
15:35:00	0.227	0.14739	0.709	0.606	0.878	0.00182	0.17	0.25	0.14739	0.585	0.629	0.762	0	0	3.3
15:40:00	0.227	0.14732	0.709	0.606	0.878	0.00182	0.17	0.25	0.14732	0.585	0.629	0.762	0	0	3.3
15:45:00	0.227	0.1473	0.709	0.606	0.878	0.00182	0.17	0.25	0.1473	0.585	0.629	0.762	0	0	3.3
15:50:00	0.227	0.1473	0.709	0.606	0.878	0.00182	0.17	0.25	0.1473	0.585	0.629	0.762	0	0	3.3
15:55:00	0.227	0.1473	0.709	0.606	0.878	0.00182	0.17	0.25	0.1473	0.585	0.629	0.762	0	0	3.3
16:00:00	0.227	0.1473	0.709	0.606	0.878	0.00182	0.17	0.25	0.1473	0.585	0.629	0.762	0	0	3.3
16:05:00	0.226	0.14606	0.707	0.605	0.874	0.00181	0.17	0.249	0.14593	0.583	0.628	0.758	0	0	3.3
16:10:00	0.222	0.14073	0.702	0.6	0.861	0.00179	0.16	0.245	0.1404	0.578	0.624	0.746	0	0	3.2
16:15:00	0.217	0.13285	0.695	0.593	0.842	0.00177	0.16	0.239	0.13248	0.572	0.616	0.728	0	0	3.1
16:20:00	0.213	0.12664	0.69	0.587	0.827	0.00175	0.16	0.235	0.12641	0.567	0.611	0.715	0	0	3
16:25:00	0.21	0.12359	0.688	0.585	0.82	0.00174	0.15	0.232	0.1235	0.565	0.608	0.709	0	0	3
16:30:00	0.21	0.12253	0.687	0.584	0.817	0.00174	0.15	0.231	0.12253	0.565	0.607	0.707	0	0	3
16:35:00	0.209	0.12224	0.687	0.583	0.817	0.00174	0.15	0.231	0.12223	0.565	0.607	0.707	0	0	3
16:40:00	0.209	0.12217	0.687	0.583	0.816	0.00174	0.15	0.231	0.12217	0.565	0.607	0.707	0	0	3
16:45:00	0.209	0.12215	0.687	0.583	0.816	0.00174	0.15	0.231	0.12215	0.565	0.607	0.707	0	0	3
16:50:00	0.209	0.12215	0.687	0.583	0.816	0.00174	0.15	0.231	0.12215	0.565	0.607	0.707	0	0	3
16:55:00	0.209	0.12215	0.687	0.583	0.816	0.00174	0.15	0.231	0.12215	0.565	0.607	0.707	0	0	3
17:00:00	0.209	0.12215	0.687	0.583	0.816	0.00174	0.15	0.231	0.12215	0.565	0.607	0.707	0	0	3
17:05:00	0.209	0.12133	0.686	0.583	0.814	0.00173	0.15	0.231	0.12123	0.563	0.606	0.704	0	0	3
17:10:00	0.206	0.11766	0.682	0.579	0.804	0.00172	0.15	0.228	0.11742	0.559	0.602	0.694	0	0	2.9
17:15:00	0.202	0.11197	0.675	0.574	0.788	0.0017	0.15	0.223	0.11168	0.554	0.597	0.68	0	0	2.8

17:20:00	0.198	0.10715	0.67	0.569	0.774	0.00168	0.15	0.219	0.10696	0.549	0.592	0.668	0	0	2.8
17:25:00	0.196	0.10464	0.668	0.566	0.768	0.00167	0.14	0.217	0.10456	0.547	0.589	0.663	0	0	2.7
17:30:00	0.196	0.10373	0.667	0.565	0.765	0.00167	0.14	0.216	0.1037	0.547	0.589	0.661	0	0	2.7
17:35:00	0.195	0.10347	0.667	0.565	0.764	0.00167	0.14	0.216	0.10346	0.547	0.588	0.66	0	0	2.7
17:40:00	0.195	0.10341	0.667	0.565	0.764	0.00167	0.14	0.216	0.10341	0.547	0.588	0.66	0	0	2.7
17:45:00	0.195	0.1034	0.667	0.565	0.764	0.00167	0.14	0.216	0.1034	0.547	0.588	0.66	0	0	2.7
17:50:00	0.195	0.10339	0.667	0.565	0.764	0.00167	0.14	0.216	0.10339	0.547	0.588	0.66	0	0	2.7
17:55:00	0.195	0.10339	0.667	0.565	0.764	0.00167	0.14	0.216	0.10339	0.547	0.588	0.66	0	0	2.7
18:00:00	0.195	0.10339	0.667	0.565	0.764	0.00167	0.14	0.216	0.10339	0.547	0.588	0.66	0	0	2.7
18:05:00	0.193	0.09953	0.66	0.561	0.751	0.00164	0.14	0.213	0.09904	0.539	0.584	0.646	0	0	2.6
18:10:00	0.179	0.08242	0.631	0.543	0.691	0.00155	0.13	0.198	0.08121	0.512	0.565	0.59	0	0	2.4
18:15:00	0.158	0.05792	0.567	0.515	0.583	0.00136	0.12	0.173	0.05648	0.462	0.536	0.498	0	0	2
18:20:00	0.136	0.03641	0.484	0.486	0.46	0.00116	0.1	0.147	0.03511	0.399	0.505	0.395	0	0	1.6
18:25:00	0.115	0.02142	0.392	0.461	0.343	0.00098	0.08	0.123	0.02042	0.327	0.478	0.296	0	0	1.2
18:30:00	0.099	0.01164	0.293	0.442	0.233	0.00081	0.07	0.104	0.0109	0.246	0.456	0.203	0	0	1
18:35:00	0.088	0.00571	0.188	0.429	0.138	0.00069	0.06	0.091	0.00526	0.162	0.442	0.121	0	0	0.8
18:40:00	0.082	0.00271	0.106	0.422	0.074	0.00062	0.06	0.083	0.00247	0.093	0.433	0.066	0	0	0.7
18:45:00	0.078	0.00128	0.055	0.418	0.037	0.00058	0.05	0.079	0.00116	0.049	0.429	0.034	0	0	0.6
18:50:00	0.077	0.00064	0.029	0.417	0.019	0.00057	0.05	0.077	0.00059	0.026	0.427	0.018	0	0	0.6
18:55:00	0.076	0.00038	0.018	0.416	0.012	0.00056	0.05	0.076	0.00036	0.017	0.426	0.011	0	0	0.6
19:00:00	0.076	0.00029	0.013	0.416	0.009	0.00056	0.05	0.076	0.00028	0.013	0.426	0.009	0	0	0.6
19:05:00	0.076	0.00025	0.011	0.416	0.008	0.00056	0.05	0.076	0.00024	0.011	0.426	0.007	0	0	0.6
19:10:00	0.076	0.00022	0.01	0.416	0.007	0.00055	0.05	0.076	0.00021	0.01	0.426	0.007	0	0	0.6
19:15:00	0.075	0.00019	0.009	0.415	0.006	0.00055	0.05	0.076	0.00018	0.009	0.426	0.006	0	0	0.6
19:20:00	0.075	0.00015	0.007	0.415	0.005	0.00055	0.05	0.075	0.00015	0.007	0.425	0.005	0	0	0.6
19:25:00	0.075	0.00012	0.006	0.415	0.004	0.00055	0.05	0.075	0.00011	0.005	0.425	0.004	0	0	0.6
19:30:00	0.075	0.00008	0.004	0.415	0.003	0.00055	0.05	0.075	0.00008	0.004	0.425	0.002	0	0	0.6
19:35:00	0.075	0.00005	0.003	0.415	0.002	0.00055	0.05	0.075	0.00005	0.002	0.425	0.002	0	0	0.6
19:40:00	0.075	0.00004	0.002	0.415	0.001	0.00055	0.05	0.075	0.00003	0.002	0.425	0.001	0	0	0.6
19:45:00	0.075	0.00002	0.001	0.415	0.001	0.00055	0.05	0.075	0.00002	0.001	0.425	0.001	0	0	0.6
19:50:00	0.075	0.00002	0.001	0.415	0.001	0.00055	0.05	0.075	0.00002	0.001	0.425	0.001	0	0	0.6
19:55:00	0.075	0.00002	0.001	0.415	0	0.00055	0.05	0.075	0.00001	0.001	0.425	0	0	0	0.6
20:00:00	0.075	0.00001	0.001	0.415	0	0.00055	0.05	0.075	0.00001	0.001	0.425	0	0	0	0.6
20:05:00	0.075	0.00001	0.001	0.415	0	0.00055	0.05	0.075	0.00001	0.001	0.425	0	0	0	0.6
20:10:00	0.075	0.00001	0	0.415	0	0.00055	0.05	0.075	0.00001	0	0.425	0	0	0	0.6
20:15:00	0.075	0.00001	0	0.415	0	0.00055	0.05	0.075	0.00001	0	0.425	0	0	0	0.6
20:20:00	0.075	0.00001	0	0.415	0	0.00055	0.05	0.075	0.00001	0	0.425	0	0	0	0.6
20:25:00	0.075	0.00001	0	0.415	0	0.00055	0.05	0.075	0.00001	0	0.425	0	0	0	0.6
20:30:00	0.075	0.00001	0	0.415	0	0.00055	0.05	0.075	0.00001	0	0.425	0	0	0	0.6
20:35:00	0.075	0.00001	0	0.415	0	0.00055	0.05	0.075	0.00001	0	0.425	0	0	0	0.6
20:40:00	0.075	0.00001	0	0.415	0	0.00055	0.05	0.075	0.00001	0	0.425	0	0	0	0.6
20:45:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
20:50:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
20:55:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:00:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6

21:05:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:10:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:15:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:20:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:25:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:30:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:35:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:40:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:45:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:50:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
21:55:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:00:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:05:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:10:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:15:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:20:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:25:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:30:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:35:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:40:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:45:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:50:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
22:55:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:00:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:05:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:10:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:15:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:20:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:25:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:30:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:35:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:40:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:45:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:50:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
23:55:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6
0:00:00	0.075	0	0	0.415	0	0.00055	0.05	0.075	0	0	0.425	0	0	0	0.6





Link		P_B18.20.01.1	P_B18.20.02.1	P_B18.20.03.1	P_B18.20.04.1	P_B18.20.05.1	P_B18.20.06.1	P_B18.20.07.1	-	-	-	P_B18.20.11.1	P_B18.20.12.1	P_B18.20.13.1	P_B18.20.14.1	P_B18.20.15.1	P_B18.20.16.1	-	P_B18.20.18.1	-	
Node	-	P_B18.20.02	P_B18.20.03	P_B18.20.04	P_B18.20.05	P_B18.20.06	P_B18.20.07	P_B18.20.08	-	-	-	P_B18.20.12	P_B18.20.13	P_B18.20.14	P_B18.20.15	P_B18.20.16	-	-	-	-	

	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
0:05:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
0:10:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
0:15:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
0:20:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
0:25:00	0.111	0.02134	0.523	1.084	0.45	0.0315	0.11	0.111	0.02169	0.53	1.613	0.457	0	0	0.8
0:30:00	0.118	0.03703	0.801	1.107	0.712	0.0315	0.12	0.118	0.0372	0.803	1.636	0.714	0	0	0.9
0:35:00	0.12	0.0422	0.878	1.115	0.789	0.03149	0.12	0.12	0.04223	0.879	1.644	0.789	0	0	0.9
0:40:00	0.124	0.04294	0.847	1.117	0.771	0.03131	0.12	0.121	0.04295	0.889	1.645	0.8	0	0	0.9
0:45:00	0.125	0.04305	0.835	1.117	0.764	0.03126	0.12	0.121	0.04306	0.891	1.645	0.801	0	0	0.9
0:50:00	0.125	0.04307	0.833	1.117	0.762	0.03125	0.12	0.121	0.04307	0.891	1.645	0.801	0	0	0.9
0:55:00	0.125	0.04307	0.833	1.117	0.762	0.03124	0.12	0.121	0.04307	0.891	1.645	0.801	0	0	0.9
1:00:00	0.125	0.04307	0.833	1.117	0.762	0.03124	0.12	0.121	0.04307	0.891	1.645	0.801	0	0	0.9
1:05:00	0.127	0.04465	0.831	1.12	0.768	0.03114	0.13	0.121	0.04474	0.915	1.648	0.825	0	0	0.9
1:10:00	0.134	0.04869	0.812	1.128	0.773	0.03082	0.13	0.123	0.04878	0.97	1.655	0.881	0	0	1
1:15:00	0.139	0.05079	0.788	1.132	0.764	0.03057	0.14	0.124	0.05083	0.996	1.658	0.909	0	0	1
1:20:00	0.141	0.05134	0.776	1.134	0.758	0.03047	0.14	0.124	0.05135	1.003	1.659	0.915	0	0	1
1:25:00	0.142	0.05144	0.772	1.134	0.755	0.03044	0.14	0.124	0.05144	1.004	1.659	0.917	0	0	1
1:30:00	0.142	0.05145	0.771	1.134	0.754	0.03044	0.14	0.124	0.05145	1.004	1.659	0.917	0	0	1
1:35:00	0.142	0.05146	0.771	1.134	0.754	0.03043	0.14	0.124	0.05146	1.004	1.659	0.917	0	0	1
1:40:00	0.142	0.05146	0.771	1.134	0.754	0.03043	0.14	0.124	0.05146	1.004	1.659	0.917	0	0	1
1:45:00	0.142	0.05146	0.771	1.134	0.754	0.03043	0.14	0.124	0.05146	1.004	1.659	0.917	0	0	1
1:50:00	0.142	0.05146	0.771	1.134	0.754	0.03043	0.14	0.124	0.05146	1.004	1.659	0.917	0	0	1
1:55:00	0.142	0.05146	0.771	1.134	0.754	0.03043	0.14	0.124	0.05146	1.004	1.659	0.917	0	0	1
2:00:00	0.142	0.05146	0.771	1.134	0.754	0.03043	0.14	0.124	0.05146	1.004	1.659	0.917	0	0	1
2:05:00	0.145	0.05377	0.77	1.138	0.763	0.0303	0.15	0.125	0.05389	1.035	1.663	0.949	0	0	1
2:10:00	0.154	0.05934	0.753	1.148	0.77	0.02989	0.15	0.128	0.05947	1.101	1.672	1.019	0	0	1
2:15:00	0.161	0.06203	0.729	1.153	0.761	0.02959	0.16	0.129	0.06207	1.13	1.677	1.051	0	0	1.1
2:20:00	0.163	0.06268	0.718	1.155	0.754	0.02948	0.16	0.129	0.06269	1.137	1.678	1.058	0	0	1.1
2:25:00	0.163	0.06278	0.715	1.155	0.752	0.02945	0.16	0.129	0.06278	1.138	1.678	1.059	0	0	1.1

2:30:00	0.163	0.0628	0.714	1.155	0.752	0.02945	0.16	0.129	0.0628	1.138	1.678	1.059	0	0	1.1
2:35:00	0.163	0.0628	0.714	1.155	0.751	0.02944	0.16	0.129	0.0628	1.138	1.678	1.06	0	0	1.1
2:40:00	0.163	0.0628	0.714	1.155	0.751	0.02944	0.16	0.129	0.0628	1.138	1.678	1.06	0	0	1.1
2:45:00	0.163	0.0628	0.714	1.155	0.751	0.02944	0.16	0.129	0.0628	1.138	1.678	1.06	0	0	1.1
2:50:00	0.163	0.0628	0.714	1.155	0.751	0.02944	0.16	0.129	0.0628	1.138	1.678	1.06	0	0	1.1
2:55:00	0.163	0.0628	0.714	1.155	0.751	0.02944	0.16	0.129	0.0628	1.138	1.678	1.06	0	0	1.1
3:00:00	0.163	0.0628	0.714	1.155	0.751	0.02944	0.16	0.129	0.0628	1.138	1.678	1.06	0	0	1.1
3:05:00	0.168	0.06638	0.714	1.161	0.763	0.02926	0.17	0.13	0.06656	1.179	1.685	1.104	0	0	1.1
3:10:00	0.18	0.07443	0.698	1.174	0.773	0.02872	0.18	0.134	0.0746	1.259	1.698	1.194	0	0	1.2
3:15:00	0.188	0.07799	0.675	1.18	0.764	0.02836	0.19	0.135	0.07805	1.291	1.704	1.231	0	0	1.2
3:20:00	0.19	0.07877	0.664	1.182	0.757	0.02823	0.19	0.135	0.07878	1.297	1.706	1.239	0	0	1.2
3:25:00	0.191	0.07889	0.661	1.183	0.755	0.0282	0.19	0.135	0.07889	1.298	1.706	1.24	0	0	1.2
3:30:00	0.191	0.0789	0.66	1.183	0.754	0.02819	0.19	0.135	0.0789	1.299	1.706	1.24	0	0	1.2
3:35:00	0.191	0.0789	0.66	1.183	0.754	0.02819	0.19	0.135	0.0789	1.299	1.706	1.24	0	0	1.2
3:40:00	0.191	0.0789	0.66	1.183	0.754	0.02819	0.19	0.135	0.0789	1.299	1.706	1.24	0	0	1.2
3:45:00	0.191	0.0789	0.66	1.183	0.754	0.02819	0.19	0.135	0.0789	1.299	1.706	1.24	0	0	1.2
3:50:00	0.191	0.0789	0.66	1.183	0.754	0.02819	0.19	0.135	0.0789	1.299	1.706	1.24	0	0	1.2
3:55:00	0.191	0.0789	0.66	1.183	0.754	0.02819	0.19	0.135	0.0789	1.299	1.706	1.24	0	0	1.2
4:00:00	0.191	0.0789	0.66	1.183	0.754	0.02819	0.19	0.135	0.0789	1.299	1.706	1.24	0	0	1.2
4:05:00	0.198	0.08486	0.662	1.191	0.771	0.02792	0.2	0.138	0.08516	1.353	1.716	1.304	0	0	1.2
4:10:00	0.215	0.0971	0.646	1.209	0.785	0.0272	0.21	0.142	0.09735	1.449	1.737	1.421	0	0	1.3
4:15:00	0.224	0.10191	0.623	1.218	0.775	0.02674	0.22	0.144	0.10199	1.482	1.745	1.463	0	0	1.4
4:20:00	0.227	0.10284	0.613	1.22	0.768	0.02658	0.23	0.144	0.10286	1.488	1.747	1.47	0	0	1.4
4:25:00	0.228	0.10297	0.61	1.221	0.765	0.02654	0.23	0.145	0.10298	1.489	1.747	1.471	0	0	1.4
4:30:00	0.228	0.10299	0.61	1.221	0.765	0.02653	0.23	0.145	0.10299	1.489	1.747	1.471	0	0	1.4
4:35:00	0.228	0.10299	0.609	1.221	0.765	0.02653	0.23	0.145	0.10299	1.489	1.747	1.471	0	0	1.4
4:40:00	0.228	0.10299	0.609	1.221	0.765	0.02653	0.23	0.145	0.10299	1.489	1.747	1.471	0	0	1.4
4:45:00	0.228	0.10299	0.609	1.221	0.765	0.02653	0.23	0.145	0.10299	1.489	1.747	1.471	0	0	1.4
4:50:00	0.228	0.10299	0.609	1.221	0.765	0.02653	0.23	0.145	0.10299	1.489	1.747	1.471	0	0	1.4
4:55:00	0.228	0.10299	0.609	1.221	0.765	0.02653	0.23	0.145	0.10299	1.489	1.747	1.471	0	0	1.4
5:00:00	0.228	0.10299	0.609	1.221	0.765	0.02653	0.23	0.145	0.10299	1.489	1.747	1.471	0	0	1.4
5:05:00	0.239	0.11382	0.614	1.234	0.79	0.02612	0.24	0.149	0.11434	1.564	1.766	1.568	0	0	1.5
5:10:00	0.263	0.13361	0.597	1.26	0.81	0.02509	0.26	0.156	0.13401	1.675	1.798	1.72	0	0	1.6
5:15:00	0.275	0.14032	0.574	1.271	0.798	0.02449	0.28	0.158	0.14044	1.706	1.809	1.765	0	0	1.7
5:20:00	0.279	0.14145	0.564	1.274	0.789	0.0243	0.28	0.158	0.14148	1.711	1.81	1.772	0	0	1.7
5:25:00	0.28	0.14161	0.561	1.275	0.787	0.02425	0.28	0.158	0.14161	1.711	1.811	1.773	0	0	1.7
5:30:00	0.28	0.14162	0.561	1.275	0.786	0.02424	0.28	0.158	0.14162	1.711	1.811	1.773	0	0	1.7
5:35:00	0.28	0.14162	0.56	1.275	0.786	0.02424	0.28	0.158	0.14162	1.711	1.811	1.773	0	0	1.7
5:40:00	0.28	0.14162	0.56	1.275	0.786	0.02424	0.28	0.158	0.14162	1.711	1.811	1.773	0	0	1.7
5:45:00	0.28	0.14162	0.56	1.275	0.786	0.02424	0.28	0.158	0.14162	1.711	1.811	1.773	0	0	1.7
5:50:00	0.28	0.14162	0.56	1.275	0.786	0.02424	0.28	0.158	0.14162	1.711	1.811	1.773	0	0	1.7
5:55:00	0.28	0.14162	0.56	1.275	0.786	0.02424	0.28	0.158	0.14162	1.711	1.811	1.773	0	0	1.7
6:00:00	0.28	0.14162	0.56	1.275	0.786	0.02424	0.28	0.158	0.14162	1.711	1.811	1.773	0	0	1.7
6:05:00	0.3	0.16397	0.569	1.298	0.828	0.02353	0.3	0.166	0.165	1.815	1.847	1.927	0	0	1.9
6:10:00	0.337	0.19859	0.55	1.337	0.854	0.02198	0.34	0.177	0.19928	1.929	1.898	2.12	0	0	2.2

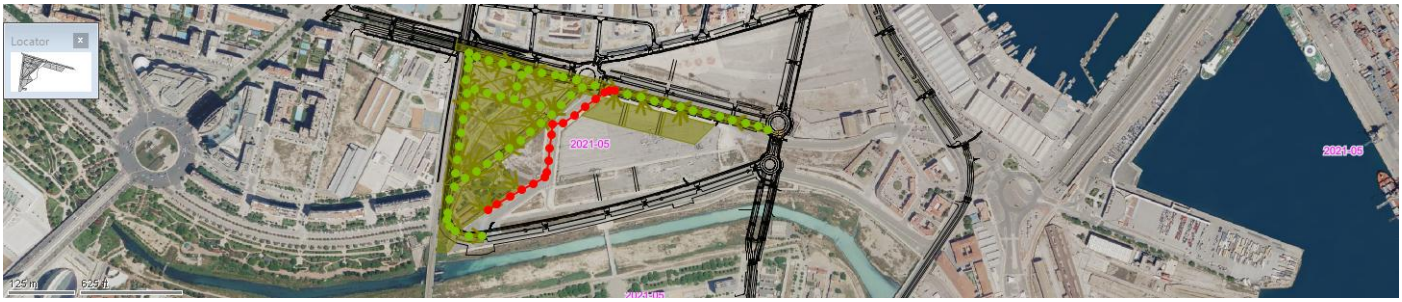
6:15:00	0.354	0.20838	0.524	1.353	0.837	0.02115	0.35	0.18	0.20858	1.952	1.911	2.164	0	0	2.3
6:20:00	0.359	0.20981	0.514	1.357	0.828	0.02089	0.36	0.181	0.20985	1.953	1.913	2.169	0	0	2.3
6:25:00	0.36	0.20998	0.512	1.358	0.825	0.02083	0.36	0.181	0.20999	1.953	1.913	2.169	0	0	2.3
6:30:00	0.36	0.21	0.511	1.358	0.824	0.02082	0.36	0.181	0.21	1.953	1.913	2.169	0	0	2.3
6:35:00	0.36	0.21	0.511	1.358	0.824	0.02081	0.36	0.181	0.21	1.953	1.913	2.169	0	0	2.3
6:40:00	0.36	0.21	0.511	1.358	0.824	0.02081	0.36	0.181	0.21	1.953	1.913	2.169	0	0	2.3
6:45:00	0.36	0.21	0.511	1.358	0.824	0.02081	0.36	0.181	0.21	1.953	1.913	2.169	0	0	2.3
6:50:00	0.36	0.21	0.511	1.358	0.824	0.02081	0.36	0.181	0.21	1.953	1.913	2.169	0	0	2.3
6:55:00	0.36	0.21	0.511	1.358	0.824	0.02081	0.36	0.181	0.21	1.953	1.913	2.169	0	0	2.3
7:00:00	0.36	0.21	0.511	1.358	0.824	0.02081	0.36	0.181	0.21	1.953	1.913	2.169	0	0	2.3
7:05:00	0.401	0.26506	0.525	1.405	0.9	0.01942	0.4	0.198	0.26751	2.08	1.99	2.423	0	0	2.7
7:10:00	0.463	0.33324	0.501	1.471	0.937	0.01696	0.46	0.219	0.33467	2.147	2.065	2.635	0	0	3.3
7:15:00	0.489	0.34844	0.472	1.495	0.913	0.01571	0.49	0.224	0.34889	2.135	2.075	2.655	0	0	3.6
7:20:00	0.497	0.35038	0.46	1.501	0.899	0.01529	0.5	0.225	0.35051	2.126	2.075	2.65	0	0	3.7
7:25:00	0.499	0.35062	0.456	1.503	0.894	0.01517	0.5	0.225	0.35065	2.123	2.074	2.647	0	0	3.7
7:30:00	0.5	0.35065	0.455	1.504	0.893	0.01513	0.5	0.225	0.35066	2.122	2.074	2.646	0	0	3.7
7:35:00	0.5	0.35066	0.454	1.504	0.892	0.01512	0.5	0.225	0.35067	2.122	2.074	2.646	0	0	3.7
7:40:00	0.5	0.35067	0.454	1.504	0.892	0.01512	0.5	0.225	0.35067	2.122	2.074	2.646	0	0	3.7
7:45:00	0.5	0.35067	0.454	1.504	0.892	0.01512	0.5	0.225	0.35067	2.122	2.074	2.646	0	0	3.7
7:50:00	0.5	0.35067	0.454	1.504	0.892	0.01512	0.5	0.225	0.35067	2.122	2.074	2.646	0	0	3.7
7:55:00	0.5	0.35067	0.454	1.504	0.892	0.01512	0.5	0.225	0.35067	2.122	2.074	2.646	0	0	3.7
8:00:00	0.5	0.35067	0.454	1.504	0.892	0.01512	0.5	0.225	0.35067	2.122	2.074	2.646	0	0	3.7
8:05:00	0.606	0.53016	0.476	1.627	1.065	0.01209	0.61	0.28	0.538	2.129	2.227	2.986	0	0	5.1
8:10:00	0.746	0.69211	0.414	1.771	1.102	0.00781	0.75	0.348	0.69668	1.812	2.259	2.867	0	0	7
8:15:00	0.814	0.7215	0.359	1.833	1.054	0.00583	0.81	0.383	0.72345	1.568	2.224	2.618	0	0	7.9
8:20:00	0.841	0.72511	0.335	1.858	1.029	0.0051	0.84	0.398	0.72587	1.46	2.207	2.494	0	0	8.2
8:25:00	0.851	0.72583	0.325	1.867	1.019	0.00484	0.85	0.404	0.72612	1.419	2.2	2.445	0	0	8.4
8:30:00	0.855	0.72605	0.321	1.871	1.015	0.00475	0.86	0.406	0.72616	1.403	2.198	2.426	0	0	8.4
8:35:00	0.857	0.72613	0.32	1.872	1.014	0.00471	0.86	0.407	0.72617	1.397	2.197	2.419	0	0	8.5
8:40:00	0.857	0.72615	0.32	1.873	1.013	0.0047	0.86	0.407	0.72617	1.395	2.197	2.416	0	0	8.5
8:45:00	0.858	0.72617	0.319	1.873	1.013	0.00469	0.86	0.407	0.72617	1.394	2.197	2.415	0	0	8.5
8:50:00	0.858	0.72617	0.319	1.873	1.013	0.00469	0.86	0.408	0.72617	1.394	2.197	2.414	0	0	8.5
8:55:00	0.858	0.72617	0.319	1.873	1.013	0.00469	0.86	0.408	0.72617	1.394	2.197	2.414	0	0	8.5
9:00:00	0.858	0.72617	0.319	1.873	1.013	0.00469	0.86	0.408	0.72617	1.394	2.197	2.414	0	0	8.5
9:05:00	0.787	0.60053	0.321	1.792	0.905	0.00545	0.79	0.35	0.59523	1.532	2.143	2.43	0	0	7.4
9:10:00	0.697	0.51264	0.352	1.699	0.878	0.00772	0.7	0.297	0.50944	1.797	2.135	2.604	0	0	6.1
9:15:00	0.651	0.49152	0.385	1.656	0.908	0.00943	0.65	0.28	0.49036	1.939	2.149	2.72	0	0	5.5
9:20:00	0.634	0.48774	0.402	1.641	0.929	0.01017	0.63	0.276	0.48736	1.99	2.158	2.767	0	0	5.3
9:25:00	0.628	0.48719	0.409	1.636	0.938	0.01043	0.63	0.274	0.48707	2.007	2.161	2.784	0	0	5.2
9:30:00	0.626	0.48708	0.411	1.634	0.941	0.01052	0.63	0.274	0.48704	2.013	2.162	2.789	0	0	5.2
9:35:00	0.626	0.48705	0.412	1.634	0.942	0.01055	0.63	0.274	0.48704	2.015	2.163	2.791	0	0	5.2
9:40:00	0.626	0.48704	0.412	1.634	0.942	0.01055	0.63	0.274	0.48704	2.015	2.163	2.791	0	0	5.2
9:45:00	0.625	0.48704	0.412	1.634	0.942	0.01056	0.63	0.274	0.48704	2.016	2.163	2.792	0	0	5.2
9:50:00	0.625	0.48704	0.412	1.634	0.942	0.01056	0.63	0.274	0.48704	2.016	2.163	2.792	0	0	5.2
9:55:00	0.625	0.48704	0.412	1.634	0.942	0.01056	0.63	0.274	0.48704	2.016	2.163	2.792	0	0	5.2

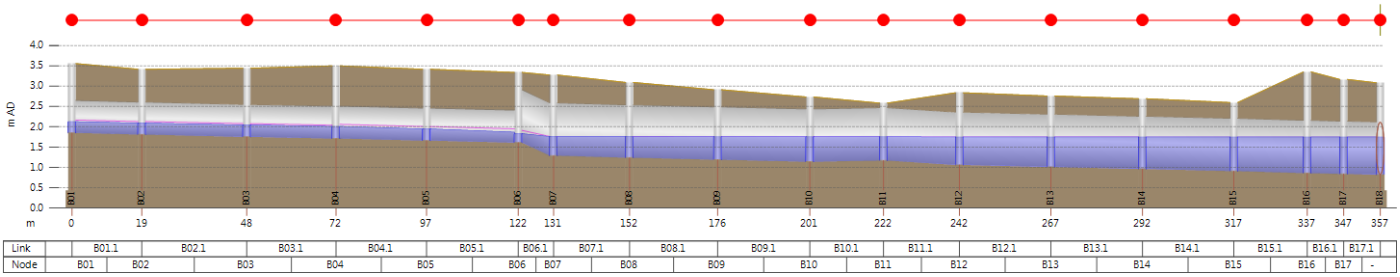
10:00	0.625	0.48704	0.412	1.634	0.942	0.01056	0.63	0.274	0.48704	2.016	2.163	2.792	0	0	5.2
10:05:00	0.567	0.39128	0.399	1.567	0.851	0.0121	0.57	0.241	0.38713	2.046	2.091	2.648	0	0	4.4
10:10:00	0.483	0.29436	0.409	1.477	0.784	0.0152	0.48	0.209	0.29206	2.047	2.008	2.453	0	0	3.4
10:15:00	0.439	0.27068	0.45	1.436	0.815	0.01727	0.44	0.201	0.26997	2.052	1.987	2.406	0	0	3
10:20:00	0.425	0.26733	0.473	1.424	0.841	0.01804	0.43	0.199	0.26714	2.059	1.986	2.405	0	0	2.9
10:25:00	0.421	0.26691	0.481	1.421	0.85	0.01826	0.42	0.199	0.26687	2.062	1.986	2.406	0	0	2.9
10:30:00	0.42	0.26685	0.483	1.42	0.852	0.01832	0.42	0.199	0.26684	2.062	1.986	2.407	0	0	2.9
10:35:00	0.42	0.26684	0.484	1.42	0.853	0.01834	0.42	0.199	0.26684	2.063	1.986	2.407	0	0	2.9
10:40:00	0.42	0.26684	0.484	1.42	0.853	0.01834	0.42	0.199	0.26684	2.063	1.986	2.407	0	0	2.9
10:45:00	0.42	0.26684	0.484	1.42	0.853	0.01834	0.42	0.199	0.26684	2.063	1.986	2.407	0	0	2.9
10:50:00	0.42	0.26684	0.484	1.42	0.853	0.01834	0.42	0.199	0.26684	2.063	1.986	2.407	0	0	2.9
10:55:00	0.42	0.26684	0.484	1.42	0.853	0.01834	0.42	0.199	0.26684	2.063	1.986	2.407	0	0	2.9
11:00:00	0.42	0.26684	0.484	1.42	0.853	0.01834	0.42	0.199	0.26684	2.063	1.986	2.407	0	0	2.9
11:00:00	0.394	0.23064	0.472	1.39	0.802	0.01918	0.39	0.187	0.22911	1.989	1.937	2.25	0	0	2.6
11:10:00	0.349	0.18622	0.482	1.342	0.763	0.02103	0.35	0.173	0.18526	1.876	1.877	2.037	0	0	2.2
11:15:00	0.325	0.17323	0.514	1.319	0.782	0.02219	0.33	0.169	0.17293	1.839	1.859	1.971	0	0	2
11:20:00	0.318	0.17106	0.53	1.313	0.796	0.02258	0.32	0.168	0.171	1.833	1.856	1.96	0	0	2
11:25:00	0.316	0.17079	0.534	1.312	0.801	0.02267	0.32	0.168	0.17077	1.833	1.856	1.959	0	0	2
11:30:00	0.316	0.17075	0.535	1.312	0.802	0.0227	0.32	0.168	0.17075	1.833	1.856	1.959	0	0	2
11:35:00	0.316	0.17075	0.536	1.312	0.802	0.0227	0.32	0.168	0.17075	1.833	1.856	1.959	0	0	2
11:40:00	0.316	0.17075	0.536	1.312	0.802	0.0227	0.32	0.168	0.17075	1.833	1.856	1.959	0	0	2
11:45:00	0.316	0.17075	0.536	1.312	0.802	0.0227	0.32	0.168	0.17075	1.833	1.856	1.959	0	0	2
11:50:00	0.316	0.17075	0.536	1.312	0.802	0.0227	0.32	0.168	0.17075	1.833	1.856	1.959	0	0	2
11:55:00	0.316	0.17075	0.536	1.312	0.802	0.0227	0.32	0.168	0.17075	1.833	1.856	1.959	0	0	2
12:00:00	0.316	0.17075	0.536	1.312	0.802	0.0227	0.32	0.168	0.17075	1.833	1.856	1.959	0	0	2
12:00:00	0.302	0.15448	0.529	1.295	0.773	0.0232	0.3	0.163	0.15375	1.764	1.829	1.853	0	0	1.9
12:10:00	0.274	0.13012	0.538	1.265	0.745	0.02437	0.27	0.154	0.12963	1.649	1.791	1.686	0	0	1.7
12:15:00	0.258	0.12181	0.564	1.251	0.757	0.02512	0.26	0.151	0.12166	1.606	1.778	1.626	0	0	1.6
12:20:00	0.253	0.12024	0.579	1.246	0.769	0.02539	0.25	0.151	0.12021	1.598	1.776	1.615	0	0	1.5
12:25:00	0.252	0.12002	0.583	1.246	0.772	0.02546	0.25	0.151	0.12002	1.597	1.775	1.613	0	0	1.5
12:30:00	0.252	0.12	0.584	1.245	0.773	0.02547	0.25	0.151	0.11999	1.597	1.775	1.613	0	0	1.5
12:35:00	0.252	0.11999	0.584	1.245	0.774	0.02548	0.25	0.151	0.11999	1.597	1.775	1.613	0	0	1.5
12:40:00	0.252	0.11999	0.585	1.245	0.774	0.02548	0.25	0.151	0.11999	1.597	1.775	1.613	0	0	1.5
12:45:00	0.252	0.11999	0.585	1.245	0.774	0.02548	0.25	0.151	0.11999	1.597	1.775	1.613	0	0	1.5
12:50:00	0.252	0.11999	0.585	1.245	0.774	0.02548	0.25	0.151	0.11999	1.597	1.775	1.613	0	0	1.5
12:55:00	0.252	0.11999	0.585	1.245	0.774	0.02548	0.25	0.151	0.11999	1.597	1.775	1.613	0	0	1.5
13:00:00	0.252	0.11999	0.585	1.245	0.774	0.02548	0.25	0.151	0.11999	1.597	1.775	1.613	0	0	1.5
13:00:00	0.243	0.11155	0.58	1.235	0.754	0.02579	0.24	0.148	0.11116	1.543	1.761	1.541	0	0	1.5
13:10:00	0.225	0.09688	0.59	1.215	0.735	0.02659	0.22	0.142	0.09657	1.442	1.736	1.413	0	0	1.4
13:15:00	0.213	0.09116	0.615	1.204	0.744	0.02714	0.21	0.14	0.09106	1.401	1.727	1.361	0	0	1.3
13:20:00	0.209	0.08995	0.629	1.201	0.754	0.02735	0.21	0.14	0.08993	1.392	1.725	1.351	0	0	1.3
13:25:00	0.208	0.08977	0.633	1.201	0.757	0.0274	0.21	0.14	0.08976	1.391	1.724	1.349	0	0	1.3
13:30:00	0.208	0.08974	0.634	1.2	0.758	0.02741	0.21	0.14	0.08974	1.391	1.724	1.349	0	0	1.3
13:35:00	0.208	0.08974	0.634	1.2	0.758	0.02741	0.21	0.14	0.08974	1.391	1.724	1.349	0	0	1.3
13:40:00	0.208	0.08974	0.634	1.2	0.758	0.02741	0.21	0.14	0.08974	1.391	1.724	1.349	0	0	1.3

13:45:00	0.208	0.08974	0.634	1.2	0.758	0.02741	0.21	0.14	0.08974	1.391	1.724	1.349	0	0	1.3
13:50:00	0.208	0.08974	0.634	1.2	0.758	0.02741	0.21	0.14	0.08974	1.391	1.724	1.349	0	0	1.3
13:55:00	0.208	0.08974	0.634	1.2	0.758	0.02741	0.21	0.14	0.08974	1.391	1.724	1.349	0	0	1.3
14:00:00	0.208	0.08974	0.634	1.2	0.758	0.02741	0.21	0.14	0.08974	1.391	1.724	1.349	0	0	1.3
14:00:00	0.203	0.08489	0.632	1.194	0.745	0.02762	0.2	0.138	0.08465	1.348	1.716	1.299	0	0	1.3
14:10:00	0.189	0.07541	0.643	1.179	0.731	0.02821	0.19	0.134	0.07521	1.264	1.699	1.2	0	0	1.2
14:15:00	0.18	0.07133	0.667	1.171	0.739	0.02863	0.18	0.132	0.07123	1.226	1.693	1.157	0	0	1.1
14:20:00	0.177	0.07034	0.68	1.169	0.748	0.02879	0.18	0.132	0.07032	1.217	1.691	1.147	0	0	1.1
14:25:00	0.177	0.07019	0.685	1.168	0.751	0.02884	0.18	0.132	0.07018	1.216	1.691	1.145	0	0	1.1
14:30:00	0.176	0.07016	0.686	1.168	0.752	0.02885	0.18	0.132	0.07016	1.215	1.691	1.145	0	0	1.1
14:35:00	0.176	0.07016	0.686	1.168	0.752	0.02885	0.18	0.132	0.07016	1.215	1.691	1.145	0	0	1.1
14:40:00	0.176	0.07016	0.686	1.168	0.752	0.02885	0.18	0.132	0.07016	1.215	1.691	1.145	0	0	1.1
14:45:00	0.176	0.07016	0.686	1.168	0.752	0.02885	0.18	0.132	0.07016	1.215	1.691	1.145	0	0	1.1
14:50:00	0.176	0.07016	0.686	1.168	0.752	0.02885	0.18	0.132	0.07016	1.215	1.691	1.145	0	0	1.1
14:55:00	0.176	0.07016	0.686	1.168	0.752	0.02885	0.18	0.132	0.07016	1.215	1.691	1.145	0	0	1.1
15:00:00	0.176	0.07016	0.686	1.168	0.752	0.02885	0.18	0.132	0.07016	1.215	1.691	1.145	0	0	1.1
15:00:00	0.173	0.06715	0.685	1.164	0.742	0.029	0.17	0.131	0.067	1.183	1.685	1.109	0	0	1.1
15:10:00	0.162	0.06069	0.697	1.153	0.732	0.02944	0.16	0.128	0.06054	1.113	1.674	1.032	0	0	1.1
15:15:00	0.156	0.05763	0.721	1.146	0.74	0.02978	0.16	0.127	0.05758	1.079	1.669	0.996	0	0	1
15:20:00	0.153	0.05686	0.735	1.145	0.748	0.02991	0.15	0.126	0.05685	1.07	1.668	0.986	0	0	1
15:25:00	0.152	0.05673	0.74	1.144	0.751	0.02995	0.15	0.126	0.05672	1.069	1.668	0.985	0	0	1
15:30:00	0.152	0.05671	0.741	1.144	0.752	0.02996	0.15	0.126	0.05671	1.069	1.668	0.985	0	0	1
15:35:00	0.152	0.0567	0.741	1.144	0.752	0.02996	0.15	0.126	0.0567	1.069	1.668	0.985	0	0	1
15:40:00	0.152	0.0567	0.741	1.144	0.752	0.02996	0.15	0.126	0.0567	1.069	1.668	0.985	0	0	1
15:45:00	0.152	0.0567	0.741	1.144	0.752	0.02996	0.15	0.126	0.0567	1.069	1.668	0.985	0	0	1
15:50:00	0.152	0.0567	0.741	1.144	0.752	0.02996	0.15	0.126	0.0567	1.069	1.668	0.985	0	0	1
15:55:00	0.152	0.0567	0.741	1.144	0.752	0.02996	0.15	0.126	0.0567	1.069	1.668	0.985	0	0	1
16:00:00	0.152	0.0567	0.741	1.144	0.752	0.02996	0.15	0.126	0.0567	1.069	1.668	0.985	0	0	1
16:00:00	0.149	0.05471	0.741	1.141	0.745	0.03007	0.15	0.126	0.05461	1.043	1.664	0.958	0	0	1
16:10:00	0.142	0.05012	0.755	1.132	0.738	0.03042	0.14	0.124	0.05002	0.986	1.657	0.898	0	0	1
16:15:00	0.136	0.04786	0.779	1.127	0.746	0.0307	0.14	0.123	0.04776	0.956	1.653	0.867	0	0	1
16:20:00	0.134	0.04716	0.794	1.126	0.753	0.03081	0.13	0.122	0.04715	0.948	1.652	0.859	0	0	0.9
16:25:00	0.133	0.04704	0.799	1.125	0.756	0.03084	0.13	0.122	0.04704	0.946	1.652	0.857	0	0	0.9
16:30:00	0.133	0.04703	0.8	1.125	0.757	0.03085	0.13	0.122	0.04702	0.946	1.652	0.857	0	0	0.9
16:35:00	0.133	0.04702	0.801	1.125	0.758	0.03085	0.13	0.122	0.04702	0.946	1.652	0.857	0	0	0.9
16:40:00	0.133	0.04702	0.801	1.125	0.758	0.03085	0.13	0.122	0.04702	0.946	1.652	0.857	0	0	0.9
16:45:00	0.133	0.04702	0.801	1.125	0.758	0.03085	0.13	0.122	0.04702	0.946	1.652	0.857	0	0	0.9
16:50:00	0.133	0.04702	0.801	1.125	0.758	0.03085	0.13	0.122	0.04702	0.946	1.652	0.857	0	0	0.9
16:55:00	0.133	0.04702	0.801	1.125	0.758	0.03085	0.13	0.122	0.04702	0.946	1.652	0.857	0	0	0.9
17:00:00	0.133	0.04702	0.801	1.125	0.758	0.03085	0.13	0.122	0.04702	0.946	1.652	0.857	0	0	0.9
17:00:00	0.131	0.04565	0.801	1.123	0.752	0.03094	0.13	0.122	0.04558	0.926	1.649	0.837	0	0	0.9
17:10:00	0.125	0.04228	0.816	1.116	0.747	0.03121	0.12	0.12	0.04228	0.878	1.644	0.789	0	0	0.9
17:15:00	0.12	0.04044	0.841	1.112	0.755	0.03144	0.12	0.119	0.04044	0.852	1.641	0.762	0	0	0.9
17:20:00	0.119	0.03991	0.845	1.111	0.755	0.03149	0.12	0.119	0.03991	0.845	1.64	0.755	0	0	0.9
17:25:00	0.119	0.03982	0.843	1.111	0.754	0.03149	0.12	0.119	0.03982	0.843	1.64	0.754	0	0	0.9

17:30:00	0.119	0.0398	0.843	1.111	0.754	0.03149	0.12	0.119	0.0398	0.843	1.64	0.754	0	0	0.9
17:35:00	0.119	0.0398	0.843	1.111	0.754	0.03149	0.12	0.119	0.0398	0.843	1.64	0.754	0	0	0.9
17:40:00	0.119	0.0398	0.843	1.111	0.754	0.03149	0.12	0.119	0.0398	0.843	1.64	0.754	0	0	0.9
17:45:00	0.119	0.0398	0.843	1.111	0.754	0.03149	0.12	0.119	0.0398	0.843	1.64	0.754	0	0	0.9
17:50:00	0.119	0.0398	0.843	1.111	0.754	0.03149	0.12	0.119	0.0398	0.843	1.64	0.754	0	0	0.9
17:55:00	0.119	0.0398	0.843	1.111	0.754	0.03149	0.12	0.119	0.0398	0.843	1.64	0.754	0	0	0.9
18:00:00	0.119	0.0398	0.843	1.111	0.754	0.03149	0.12	0.119	0.0398	0.843	1.64	0.754	0	0	0.9
18:05:00	0.116	0.03288	0.734	1.1	0.647	0.03149	0.12	0.116	0.03263	0.729	1.629	0.643	0	0	0.9
18:10:00	0.109	0.01691	0.43	1.078	0.367	0.03149	0.11	0.108	0.01668	0.425	1.607	0.362	0	0	0.8
18:15:00	0.104	0.00734	0.204	1.068	0.17	0.03149	0.1	0.104	0.00723	0.201	1.597	0.168	0	0	0.7
18:20:00	0.102	0.00288	0.084	1.065	0.069	0.03149	0.1	0.101	0.00283	0.082	1.594	0.068	0	0	0.7
18:25:00	0.101	0.00109	0.032	1.064	0.026	0.03149	0.1	0.101	0.00107	0.032	1.593	0.026	0	0	0.7
18:30:00	0.1	0.00049	0.012	1.063	0.01	0.03149	0.1	0.1	0.00039	0.012	1.592	0.009	0	0	0.7
18:35:00	0.1	0.00016	0.005	1.063	0.004	0.03149	0.1	0.1	0.00015	0.005	1.592	0.004	0	0	0.7
18:40:00	0.1	0.00009	0.003	1.063	0.002	0.03149	0.1	0.1	0.00009	0.003	1.592	0.002	0	0	0.7
18:45:00	0.1	0.00007	0.002	1.063	0.002	0.03149	0.1	0.1	0.00007	0.002	1.592	0.002	0	0	0.7
18:50:00	0.1	0.00007	0.002	1.063	0.002	0.03149	0.1	0.1	0.00007	0.002	1.592	0.002	0	0	0.7
18:55:00	0.1	0.00007	0.002	1.063	0.002	0.03149	0.1	0.1	0.00007	0.002	1.592	0.002	0	0	0.7
19:00:00	0.1	0.00007	0.002	1.063	0.002	0.03149	0.1	0.1	0.00007	0.002	1.592	0.002	0	0	0.7
19:00:00	0.1	0.00007	0.002	1.063	0.002	0.03149	0.1	0.1	0.00007	0.002	1.592	0.002	0	0	0.7
19:10:00	0.1	0.00005	0.001	1.063	0.001	0.03149	0.1	0.1	0.00005	0.001	1.592	0.001	0	0	0.7
19:15:00	0.1	0.00003	0.001	1.063	0.001	0.03149	0.1	0.1	0.00003	0.001	1.592	0.001	0	0	0.7
19:20:00	0.1	0.00001	0	1.063	0	0.03149	0.1	0.1	0.00001	0	1.592	0	0	0	0.7
19:25:00	0.1	0.00001	0	1.063	0	0.03149	0.1	0.1	0.00001	0	1.592	0	0	0	0.7
19:30:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
19:35:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
19:40:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
19:45:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
19:50:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
19:55:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:00:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:00:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:10:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:15:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:20:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:25:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:30:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:35:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:40:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:45:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:50:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
20:55:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:00:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:05:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:10:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7

21:15:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:20:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:25:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:30:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:35:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:40:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:45:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:50:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
21:55:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:00:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:05:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:10:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:15:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:20:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:25:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:30:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:35:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:40:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:45:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:50:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
22:55:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:00:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:05:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:10:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:15:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:20:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:25:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:30:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:35:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:40:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:45:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:50:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
23:55:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7
0:00:00	0.1	0	0	1.063	0	0.03149	0.1	0.1	0	0	1.592	0	0	0	0.7





	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
0:05:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
0:10:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
0:15:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
0:20:00	0.072	-0.0002	0.011	0.892	-0.007	0.00064	0.06	0.068	0.0001	0.006	0.901	0.004	0	0	0.4
0:25:00	0.11	0.02052	0.445	0.937	0.381	0.00143	0.09	0.116	0.02249	0.44	0.956	0.387	0	0	0.7
0:30:00	0.161	0.05644	0.577	0.999	0.599	0.00154	0.13	0.168	0.05794	0.542	1.018	0.576	0	0	1.3
0:35:00	0.19	0.07188	0.526	1.028	0.596	0.00122	0.15	0.194	0.07251	0.513	1.044	0.587	0	0	1.6
0:40:00	0.199	0.07602	0.51	1.037	0.592	0.00115	0.15	0.201	0.07617	0.501	1.051	0.584	0	0	1.7
0:45:00	0.201	0.0769	0.507	1.039	0.591	0.00113	0.16	0.203	0.07693	0.498	1.053	0.583	0	0	1.7
0:50:00	0.201	0.07707	0.506	1.039	0.59	0.00112	0.16	0.203	0.07707	0.497	1.053	0.583	0	0	1.7
0:55:00	0.201	0.0771	0.506	1.039	0.59	0.00112	0.16	0.203	0.0771	0.497	1.053	0.583	0	0	1.7
1:00:00	0.201	0.0771	0.506	1.039	0.59	0.00112	0.16	0.203	0.0771	0.497	1.053	0.583	0	0	1.7
1:05:00	0.203	0.07875	0.509	1.041	0.596	0.00113	0.16	0.205	0.07891	0.5	1.055	0.589	0	0	1.8
1:10:00	0.209	0.0850	0.519	1.048	0.618	0.00116	0.16	0.211	0.08537	0.51	1.063	0.61	0	0	1.8
1:15:00	0.214	0.0898	0.52	1.054	0.627	0.00115	0.17	0.217	0.08998	0.511	1.069	0.619	0	0	1.9
1:20:00	0.217	0.09155	0.518	1.057	0.628	0.00114	0.17	0.219	0.09161	0.509	1.072	0.62	0	0	1.9
1:25:00	0.218	0.092	0.516	1.058	0.628	0.00113	0.17	0.22	0.09201	0.507	1.072	0.62	0	0	1.9
1:30:00	0.218	0.09209	0.516	1.058	0.628	0.00113	0.17	0.22	0.09209	0.507	1.072	0.62	0	0	2
1:35:00	0.218	0.09211	0.516	1.058	0.628	0.00113	0.17	0.22	0.09211	0.507	1.073	0.62	0	0	2
1:40:00	0.218	0.09211	0.516	1.058	0.628	0.00113	0.17	0.22	0.09211	0.507	1.073	0.62	0	0	2
1:45:00	0.218	0.09211	0.516	1.058	0.628	0.00113	0.17	0.22	0.09211	0.507	1.073	0.62	0	0	2
1:50:00	0.218	0.09211	0.516	1.058	0.628	0.00113	0.17	0.22	0.09211	0.507	1.073	0.62	0	0	2
1:55:00	0.218	0.09211	0.516	1.058	0.628	0.00113	0.17	0.22	0.09211	0.507	1.073	0.62	0	0	2
2:00:00	0.218	0.09211	0.516	1.058	0.628	0.00113	0.17	0.22	0.09211	0.507	1.073	0.62	0	0	2
2:05:00	0.22	0.09463	0.52	1.061	0.636	0.00114	0.17	0.222	0.09486	0.511	1.075	0.629	0	0	2
2:10:00	0.228	0.10358	0.532	1.07	0.663	0.00118	0.18	0.23	0.10396	0.522	1.085	0.654	0	0	2.1
2:15:00	0.235	0.10969	0.531	1.078	0.672	0.00116	0.18	0.237	0.10991	0.522	1.093	0.664	0	0	2.2

2:20:00	0.238	0.11178	0.528	1.081	0.672	0.00115	0.18	0.24	0.11185	0.519	1.095	0.664	0	0	2.2
2:25:00	0.239	0.11229	0.526	1.082	0.672	0.00114	0.19	0.241	0.11231	0.518	1.096	0.664	0	0	2.2
2:30:00	0.239	0.1124	0.526	1.082	0.672	0.00114	0.19	0.241	0.1124	0.517	1.096	0.663	0	0	2.2
2:35:00	0.239	0.11242	0.526	1.082	0.671	0.00114	0.19	0.241	0.11242	0.517	1.096	0.663	0	0	2.2
2:40:00	0.239	0.11242	0.526	1.082	0.671	0.00114	0.19	0.241	0.11242	0.517	1.096	0.663	0	0	2.2
2:45:00	0.239	0.11242	0.526	1.082	0.671	0.00114	0.19	0.241	0.11242	0.517	1.096	0.663	0	0	2.2
2:50:00	0.239	0.11242	0.526	1.082	0.671	0.00114	0.19	0.241	0.11242	0.517	1.096	0.663	0	0	2.2
2:55:00	0.239	0.11242	0.526	1.082	0.671	0.00114	0.19	0.241	0.11242	0.517	1.096	0.663	0	0	2.2
3:00:00	0.239	0.11242	0.526	1.082	0.671	0.00114	0.19	0.241	0.11242	0.517	1.096	0.663	0	0	2.2
3:05:00	0.242	0.1165	0.532	1.086	0.683	0.00116	0.19	0.244	0.11684	0.523	1.101	0.676	0	0	2.3
3:10:00	0.252	0.12976	0.545	1.099	0.716	0.0012	0.2	0.255	0.13027	0.535	1.114	0.708	0	0	2.4
3:15:00	0.261	0.13797	0.542	1.108	0.725	0.00117	0.2	0.264	0.13823	0.533	1.123	0.717	0	0	2.5
3:20:00	0.265	0.14052	0.538	1.112	0.724	0.00115	0.21	0.267	0.1406	0.529	1.126	0.716	0	0	2.6
3:25:00	0.266	0.1411	0.536	1.112	0.724	0.00115	0.21	0.268	0.14112	0.528	1.127	0.716	0	0	2.6
3:30:00	0.266	0.14122	0.535	1.113	0.723	0.00114	0.21	0.268	0.14123	0.527	1.127	0.715	0	0	2.6
3:35:00	0.266	0.14125	0.535	1.113	0.723	0.00114	0.21	0.268	0.14125	0.527	1.127	0.715	0	0	2.6
3:40:00	0.266	0.14125	0.535	1.113	0.723	0.00114	0.21	0.268	0.14125	0.527	1.127	0.715	0	0	2.6
3:45:00	0.266	0.14125	0.535	1.113	0.723	0.00114	0.21	0.268	0.14125	0.527	1.127	0.715	0	0	2.6
3:50:00	0.266	0.14125	0.535	1.113	0.723	0.00114	0.21	0.268	0.14125	0.527	1.127	0.715	0	0	2.6
3:55:00	0.266	0.14125	0.535	1.113	0.723	0.00114	0.21	0.268	0.14125	0.527	1.127	0.715	0	0	2.6
4:00:00	0.266	0.14125	0.535	1.113	0.723	0.00114	0.21	0.268	0.14125	0.527	1.127	0.715	0	0	2.6
4:05:00	0.271	0.14838	0.544	1.119	0.741	0.00118	0.21	0.273	0.1489	0.536	1.134	0.734	0	0	2.7
4:10:00	0.285	0.16905	0.558	1.137	0.783	0.00122	0.22	0.289	0.16978	0.549	1.152	0.774	0	0	2.9
4:15:00	0.297	0.18034	0.552	1.149	0.79	0.00118	0.23	0.299	0.18068	0.543	1.164	0.782	0	0	3
4:20:00	0.301	0.18351	0.546	1.153	0.788	0.00116	0.23	0.303	0.18361	0.538	1.167	0.78	0	0	3.1
4:25:00	0.302	0.1842	0.544	1.154	0.787	0.00115	0.23	0.304	0.18422	0.537	1.168	0.779	0	0	3.1
4:30:00	0.302	0.18434	0.544	1.154	0.787	0.00115	0.23	0.305	0.18434	0.536	1.168	0.779	0	0	3.1
4:35:00	0.302	0.18437	0.544	1.154	0.786	0.00115	0.23	0.305	0.18437	0.536	1.169	0.779	0	0	3.1
4:40:00	0.302	0.18437	0.544	1.154	0.786	0.00115	0.23	0.305	0.18437	0.536	1.169	0.779	0	0	3.1
4:45:00	0.302	0.18437	0.544	1.154	0.786	0.00115	0.23	0.305	0.18437	0.536	1.169	0.779	0	0	3.1
4:50:00	0.302	0.18437	0.544	1.154	0.786	0.00115	0.23	0.305	0.18437	0.536	1.169	0.779	0	0	3.1
4:55:00	0.302	0.18437	0.544	1.154	0.786	0.00115	0.23	0.305	0.18437	0.536	1.169	0.778	0	0	3.1
5:00:00	0.302	0.18437	0.544	1.154	0.786	0.00115	0.23	0.305	0.18437	0.536	1.169	0.778	0	0	3.1
5:05:00	0.31	0.19806	0.557	1.164	0.816	0.00121	0.24	0.313	0.19892	0.549	1.179	0.809	0	0	3.2
5:10:00	0.332	0.23241	0.571	1.191	0.869	0.00125	0.26	0.336	0.23348	0.562	1.206	0.86	0	0	3.6
5:15:00	0.347	0.24846	0.56	1.206	0.872	0.00119	0.27	0.35	0.24891	0.552	1.221	0.864	0	0	3.8
5:20:00	0.352	0.25249	0.553	1.211	0.868	0.00117	0.27	0.355	0.25261	0.546	1.226	0.86	0	0	3.9
5:25:00	0.354	0.25332	0.55	1.212	0.866	0.00116	0.27	0.356	0.25335	0.544	1.227	0.859	0	0	3.9
5:30:00	0.354	0.25349	0.55	1.212	0.866	0.00116	0.27	0.356	0.2535	0.543	1.227	0.858	0	0	3.9
5:35:00	0.354	0.25352	0.55	1.212	0.866	0.00116	0.27	0.356	0.25352	0.543	1.227	0.858	0	0	3.9
5:40:00	0.354	0.25353	0.55	1.212	0.866	0.00115	0.27	0.356	0.25353	0.543	1.227	0.858	0	0	3.9
5:45:00	0.354	0.25353	0.55	1.212	0.866	0.00115	0.27	0.356	0.25353	0.543	1.227	0.858	0	0	3.9
5:50:00	0.354	0.25353	0.55	1.212	0.866	0.00115	0.27	0.356	0.25353	0.543	1.227	0.858	0	0	3.9
5:55:00	0.354	0.25353	0.55	1.212	0.866	0.00115	0.27	0.356	0.25353	0.543	1.227	0.858	0	0	3.9
6:00:00	0.354	0.25353	0.55	1.212	0.866	0.00115	0.27	0.356	0.25353	0.543	1.227	0.858	0	0	3.9

6:05:00	0.368	0.28356	0.571	1.231	0.918	0.00126	0.29	0.372	0.28516	0.563	1.247	0.911	0	0	4.1
6:10:00	0.404	0.34531	0.581	1.273	0.983	0.00128	0.31	0.408	0.34701	0.573	1.289	0.975	0	0	4.7
6:15:00	0.425	0.36928	0.562	1.294	0.979	0.0012	0.33	0.428	0.36992	0.556	1.309	0.972	0	0	5
6:20:00	0.432	0.37461	0.554	1.3	0.972	0.00117	0.33	0.434	0.37478	0.548	1.315	0.965	0	0	5.1
6:25:00	0.433	0.37567	0.551	1.301	0.97	0.00116	0.34	0.436	0.37571	0.546	1.316	0.963	0	0	5.1
6:30:00	0.434	0.37588	0.551	1.302	0.97	0.00116	0.34	0.436	0.37589	0.545	1.316	0.963	0	0	5.1
6:35:00	0.434	0.37593	0.55	1.302	0.969	0.00116	0.34	0.436	0.37593	0.545	1.316	0.963	0	0	5.1
6:40:00	0.434	0.37593	0.55	1.302	0.969	0.00116	0.34	0.436	0.37593	0.545	1.316	0.962	0	0	5.1
6:45:00	0.434	0.37594	0.55	1.302	0.969	0.00116	0.34	0.436	0.37594	0.545	1.316	0.962	0	0	5.1
6:50:00	0.434	0.37594	0.55	1.302	0.969	0.00116	0.34	0.436	0.37594	0.545	1.316	0.962	0	0	5.1
6:55:00	0.434	0.37594	0.55	1.302	0.969	0.00116	0.34	0.436	0.37594	0.545	1.316	0.962	0	0	5.1
7:00:00	0.434	0.37594	0.55	1.302	0.969	0.00116	0.34	0.436	0.37594	0.545	1.316	0.962	0	0	5.1
7:05:00	0.463	0.45517	0.586	1.342	1.072	0.00135	0.36	0.468	0.45861	0.579	1.359	1.065	0	0	5.6
7:10:00	0.526	0.57714	0.582	1.413	1.145	0.00132	0.41	0.531	0.57992	0.575	1.43	1.138	0	0	6.7
7:15:00	0.558	0.61603	0.555	1.444	1.13	0.00122	0.43	0.562	0.61705	0.55	1.459	1.124	0	0	7.2
7:20:00	0.569	0.62481	0.543	1.453	1.119	0.00118	0.44	0.571	0.62511	0.539	1.468	1.113	0	0	7.4
7:25:00	0.572	0.62696	0.539	1.455	1.115	0.00116	0.44	0.574	0.62705	0.535	1.47	1.109	0	0	7.4
7:30:00	0.573	0.62754	0.538	1.456	1.114	0.00116	0.44	0.575	0.62756	0.534	1.471	1.108	0	0	7.5
7:35:00	0.573	0.6277	0.538	1.456	1.113	0.00116	0.44	0.575	0.6277	0.534	1.471	1.107	0	0	7.5
7:40:00	0.573	0.62774	0.538	1.456	1.113	0.00116	0.44	0.575	0.62774	0.534	1.471	1.107	0	0	7.5
7:45:00	0.573	0.62775	0.538	1.456	1.113	0.00116	0.44	0.575	0.62775	0.534	1.471	1.107	0	0	7.5
7:50:00	0.573	0.62776	0.538	1.456	1.113	0.00116	0.44	0.575	0.62776	0.534	1.471	1.107	0	0	7.5
7:55:00	0.573	0.62776	0.538	1.456	1.113	0.00116	0.44	0.575	0.62776	0.534	1.471	1.107	0	0	7.5
8:00:00	0.573	0.62776	0.538	1.456	1.113	0.00116	0.44	0.575	0.62776	0.534	1.471	1.107	0	0	7.5
8:05:00	0.655	0.89986	0.598	1.567	1.343	0.00155	0.51	0.662	0.90856	0.59	1.586	1.337	0	0	8.9
8:10:00	0.798	1.18838	0.54	1.717	1.391	0.00136	0.62	0.803	1.19453	0.537	1.734	1.388	0	0	11.3
8:15:00	0.873	1.26535	0.484	1.784	1.335	0.0012	0.67	0.876	1.26786	0.482	1.799	1.333	0	0	12.5
8:20:00	0.903	1.28744	0.461	1.81	1.308	0.00114	0.7	0.905	1.28839	0.459	1.825	1.306	0	0	13
8:25:00	0.914	1.29528	0.452	1.82	1.298	0.00112	0.7	0.916	1.29564	0.451	1.835	1.296	0	0	13.2
8:30:00	0.919	1.29824	0.449	1.824	1.295	0.00112	0.71	0.92	1.29834	0.448	1.839	1.292	0	0	13.3
8:35:00	0.92	1.29936	0.448	1.826	1.293	0.00111	0.71	0.922	1.29936	0.446	1.84	1.291	0	0	13.3
8:40:00	0.921	1.29972	0.448	1.826	1.293	0.00111	0.71	0.923	1.29974	0.446	1.84	1.29	0	0	13.3
8:45:00	0.921	1.29988	0.447	1.826	1.293	0.00111	0.71	0.923	1.29989	0.446	1.841	1.29	0	0	13.3
8:50:00	0.921	1.29994	0.447	1.826	1.293	0.00111	0.71	0.923	1.29995	0.446	1.841	1.29	0	0	13.3
8:55:00	0.921	1.29997	0.447	1.826	1.293	0.00111	0.71	0.923	1.29997	0.446	1.841	1.29	0	0	13.3
9:00:00	0.921	1.29998	0.447	1.826	1.292	0.00111	0.71	0.923	1.29998	0.446	1.841	1.29	0	0	13.3
9:05:00	0.865	1.11672	0.435	1.757	1.191	0.00096	0.67	0.864	1.11161	0.433	1.769	1.186	0	0	12.4
9:10:00	0.775	0.95024	0.457	1.663	1.151	0.00099	0.6	0.775	0.94616	0.455	1.675	1.146	0	0	10.9
9:15:00	0.726	0.89542	0.488	1.616	1.175	0.00107	0.56	0.727	0.89365	0.486	1.63	1.17	0	0	10.1
9:20:00	0.706	0.87899	0.505	1.599	1.193	0.00112	0.54	0.708	0.87836	0.502	1.613	1.188	0	0	9.7
9:25:00	0.7	0.87414	0.511	1.593	1.2	0.00114	0.54	0.702	0.87393	0.508	1.608	1.196	0	0	9.6
9:30:00	0.698	0.87261	0.513	1.591	1.203	0.00115	0.54	0.7	0.87254	0.51	1.606	1.198	0	0	9.6
9:35:00	0.697	0.87212	0.514	1.591	1.204	0.00115	0.54	0.699	0.8721	0.511	1.605	1.199	0	0	9.6
9:40:00	0.697	0.87197	0.514	1.591	1.204	0.00115	0.54	0.699	0.87196	0.511	1.605	1.199	0	0	9.6
9:45:00	0.697	0.87192	0.515	1.59	1.204	0.00115	0.54	0.699	0.87191	0.511	1.605	1.199	0	0	9.6

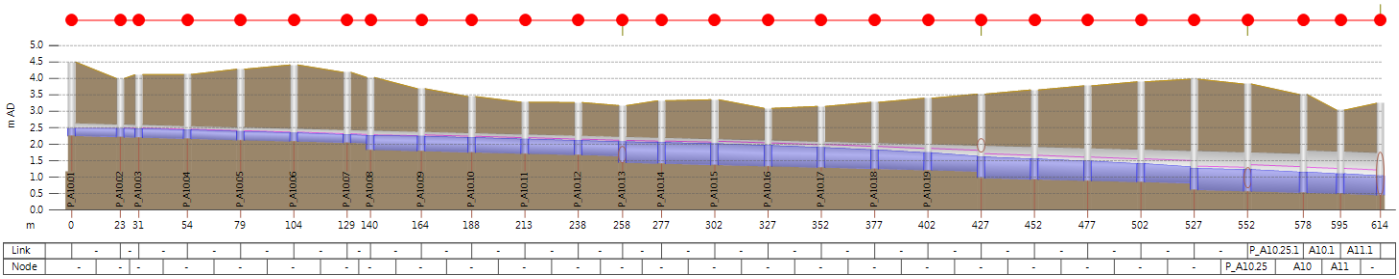
9:50:00	0.697	0.8719	0.515	1.59	1.204	0.00115	0.54	0.699	0.8719	0.511	1.605	1.199	0	0	9.6
9:55:00	0.697	0.87189	0.515	1.59	1.204	0.00115	0.54	0.699	0.87189	0.511	1.605	1.199	0	0	9.6
10:00:00	0.697	0.87189	0.515	1.59	1.204	0.00115	0.54	0.699	0.87189	0.511	1.605	1.199	0	0	9.6
10:05:00	0.651	0.7263	0.488	1.532	1.093	0.00098	0.5	0.651	0.72155	0.485	1.544	1.086	0	0	8.8
10:10:00	0.568	0.55654	0.485	1.439	0.999	0.00095	0.44	0.567	0.55249	0.482	1.451	0.993	0	0	7.4
10:15:00	0.518	0.49783	0.517	1.39	1.008	0.00106	0.4	0.519	0.49611	0.513	1.404	1.002	0	0	6.5
10:20:00	0.5	0.48259	0.537	1.374	1.026	0.00112	0.39	0.502	0.48206	0.533	1.388	1.019	0	0	6.2
10:25:00	0.495	0.47894	0.544	1.369	1.033	0.00115	0.38	0.497	0.4788	0.539	1.384	1.026	0	0	6.1
10:30:00	0.493	0.47801	0.546	1.368	1.035	0.00116	0.38	0.496	0.47797	0.541	1.382	1.028	0	0	6.1
10:35:00	0.493	0.47777	0.547	1.368	1.035	0.00116	0.38	0.495	0.47776	0.542	1.382	1.029	0	0	6.1
10:40:00	0.493	0.47771	0.547	1.368	1.035	0.00116	0.38	0.495	0.47771	0.542	1.382	1.029	0	0	6.1
10:45:00	0.493	0.4777	0.547	1.367	1.035	0.00116	0.38	0.495	0.4777	0.542	1.382	1.029	0	0	6.1
10:50:00	0.493	0.47769	0.547	1.367	1.035	0.00116	0.38	0.495	0.47769	0.542	1.382	1.029	0	0	6.1
10:55:00	0.493	0.47769	0.547	1.367	1.035	0.00116	0.38	0.495	0.47769	0.542	1.382	1.029	0	0	6.1
11:00:00	0.493	0.47769	0.547	1.367	1.035	0.00116	0.38	0.495	0.47769	0.542	1.382	1.029	0	0	6.1
11:05:00	0.474	0.4259	0.526	1.342	0.974	0.00105	0.37	0.475	0.42378	0.521	1.355	0.966	0	0	5.8
11:10:00	0.431	0.34711	0.516	1.292	0.904	0.00102	0.33	0.431	0.34489	0.511	1.305	0.897	0	0	5.1
11:15:00	0.402	0.31546	0.534	1.264	0.902	0.00109	0.31	0.404	0.31457	0.529	1.278	0.895	0	0	4.6
11:20:00	0.393	0.30769	0.546	1.255	0.91	0.00114	0.3	0.395	0.30745	0.54	1.269	0.903	0	0	4.5
11:25:00	0.39	0.30608	0.55	1.253	0.913	0.00115	0.3	0.392	0.30602	0.544	1.267	0.906	0	0	4.4
11:30:00	0.39	0.30575	0.551	1.252	0.914	0.00116	0.3	0.392	0.30574	0.545	1.267	0.907	0	0	4.4
11:35:00	0.39	0.30569	0.551	1.252	0.914	0.00116	0.3	0.392	0.30569	0.545	1.267	0.907	0	0	4.4
11:40:00	0.39	0.30568	0.551	1.252	0.914	0.00116	0.3	0.392	0.30568	0.545	1.267	0.907	0	0	4.4
11:45:00	0.39	0.30567	0.551	1.252	0.914	0.00116	0.3	0.392	0.30567	0.545	1.267	0.907	0	0	4.4
11:50:00	0.39	0.30567	0.551	1.252	0.914	0.00116	0.3	0.392	0.30567	0.545	1.267	0.907	0	0	4.4
11:55:00	0.39	0.30567	0.551	1.252	0.914	0.00116	0.3	0.392	0.30567	0.545	1.267	0.907	0	0	4.4
12:00:00	0.39	0.30567	0.551	1.252	0.914	0.00116	0.3	0.392	0.30567	0.545	1.267	0.907	0	0	4.4
12:05:00	0.38	0.28348	0.537	1.239	0.878	0.00109	0.29	0.381	0.28228	0.531	1.253	0.87	0	0	4.3
12:10:00	0.354	0.24111	0.524	1.208	0.825	0.00105	0.27	0.355	0.23982	0.519	1.222	0.817	0	0	3.9
12:15:00	0.335	0.22165	0.534	1.189	0.817	0.0011	0.26	0.337	0.22107	0.528	1.203	0.81	0	0	3.6
12:20:00	0.328	0.21628	0.543	1.183	0.821	0.00114	0.25	0.33	0.21611	0.536	1.197	0.813	0	0	3.5
12:25:00	0.327	0.21516	0.546	1.181	0.823	0.00115	0.25	0.329	0.21506	0.539	1.196	0.815	0	0	3.5
12:30:00	0.326	0.21486	0.547	1.181	0.824	0.00115	0.25	0.328	0.21486	0.54	1.195	0.816	0	0	3.5
12:35:00	0.326	0.21482	0.547	1.181	0.824	0.00115	0.25	0.328	0.21482	0.54	1.195	0.816	0	0	3.5
12:40:00	0.326	0.21481	0.547	1.181	0.824	0.00115	0.25	0.328	0.21481	0.54	1.195	0.816	0	0	3.5
12:45:00	0.326	0.21481	0.547	1.181	0.824	0.00115	0.25	0.328	0.21481	0.54	1.195	0.816	0	0	3.5
12:50:00	0.326	0.21481	0.547	1.181	0.824	0.00115	0.25	0.328	0.21481	0.54	1.195	0.816	0	0	3.5
12:55:00	0.326	0.21481	0.547	1.181	0.824	0.00115	0.25	0.328	0.21481	0.54	1.195	0.816	0	0	3.5
13:00:00	0.326	0.21481	0.547	1.181	0.824	0.00115	0.25	0.328	0.21481	0.54	1.195	0.816	0	0	3.5
13:05:00	0.32	0.20392	0.538	1.173	0.802	0.00111	0.25	0.322	0.20326	0.531	1.187	0.794	0	0	3.4
13:10:00	0.303	0.17895	0.524	1.153	0.76	0.00107	0.23	0.305	0.17811	0.518	1.166	0.752	0	0	3.1
13:15:00	0.29	0.16588	0.53	1.139	0.75	0.0011	0.22	0.292	0.16538	0.523	1.153	0.742	0	0	2.9
13:20:00	0.285	0.16181	0.536	1.134	0.751	0.00113	0.22	0.287	0.16168	0.529	1.148	0.744	0	0	2.9
13:25:00	0.283	0.16089	0.539	1.132	0.753	0.00114	0.22	0.285	0.16085	0.531	1.147	0.745	0	0	2.8
13:30:00	0.283	0.16079	0.54	1.132	0.753	0.00115	0.22	0.285	0.16069	0.532	1.146	0.745	0	0	2.8

13:35:00	0.283	0.16066	0.54	1.132	0.753	0.00115	0.22	0.285	0.16066	0.532	1.146	0.745	0	0	2.8
13:40:00	0.283	0.16065	0.54	1.132	0.753	0.00115	0.22	0.285	0.16065	0.532	1.146	0.745	0	0	2.8
13:45:00	0.283	0.16065	0.54	1.132	0.753	0.00115	0.22	0.285	0.16065	0.532	1.146	0.745	0	0	2.8
13:50:00	0.283	0.16065	0.54	1.132	0.753	0.00115	0.22	0.285	0.16065	0.532	1.146	0.745	0	0	2.8
13:55:00	0.283	0.16065	0.54	1.132	0.753	0.00115	0.22	0.285	0.16065	0.532	1.146	0.745	0	0	2.8
14:00:00	0.283	0.16065	0.54	1.132	0.753	0.00115	0.22	0.285	0.16065	0.532	1.146	0.745	0	0	2.8
14:05:00	0.279	0.15472	0.533	1.127	0.739	0.00112	0.22	0.281	0.15431	0.525	1.141	0.731	0	0	2.8
14:10:00	0.268	0.13893	0.521	1.113	0.706	0.00108	0.21	0.269	0.13835	0.514	1.127	0.698	0	0	2.6
14:15:00	0.258	0.12962	0.523	1.102	0.695	0.0011	0.2	0.259	0.1293	0.516	1.116	0.687	0	0	2.5
14:20:00	0.253	0.12654	0.528	1.098	0.695	0.00113	0.2	0.255	0.12644	0.52	1.112	0.687	0	0	2.4
14:25:00	0.252	0.1258	0.53	1.097	0.696	0.00114	0.2	0.254	0.12577	0.522	1.111	0.688	0	0	2.4
14:30:00	0.252	0.12564	0.531	1.096	0.696	0.00114	0.2	0.254	0.12563	0.522	1.111	0.688	0	0	2.4
14:35:00	0.252	0.12561	0.531	1.096	0.696	0.00114	0.2	0.254	0.12561	0.522	1.111	0.688	0	0	2.4
14:40:00	0.252	0.1256	0.531	1.096	0.696	0.00114	0.2	0.254	0.1256	0.522	1.111	0.688	0	0	2.4
14:45:00	0.252	0.1256	0.531	1.096	0.696	0.00114	0.2	0.254	0.1256	0.522	1.111	0.688	0	0	2.4
14:50:00	0.252	0.1256	0.531	1.096	0.696	0.00114	0.2	0.254	0.1256	0.522	1.111	0.688	0	0	2.4
14:55:00	0.252	0.1256	0.531	1.096	0.696	0.00114	0.2	0.254	0.1256	0.522	1.111	0.688	0	0	2.4
15:00:00	0.252	0.1256	0.531	1.096	0.696	0.00114	0.2	0.254	0.1256	0.522	1.111	0.688	0	0	2.4
15:05:00	0.249	0.12213	0.526	1.093	0.687	0.00112	0.19	0.251	0.12183	0.518	1.107	0.678	0	0	2.4
15:10:00	0.241	0.11158	0.515	1.083	0.66	0.00109	0.19	0.242	0.11115	0.507	1.097	0.652	0	0	2.2
15:15:00	0.233	0.10474	0.515	1.074	0.649	0.0011	0.18	0.235	0.10449	0.507	1.088	0.641	0	0	2.1
15:20:00	0.229	0.1023	0.519	1.071	0.648	0.00112	0.18	0.231	0.10222	0.51	1.085	0.64	0	0	2.1
15:25:00	0.228	0.10168	0.52	1.07	0.649	0.00113	0.18	0.23	0.10166	0.512	1.084	0.641	0	0	2.1
15:30:00	0.228	0.10154	0.521	1.069	0.649	0.00113	0.18	0.23	0.10154	0.512	1.084	0.641	0	0	2.1
15:35:00	0.228	0.10152	0.521	1.069	0.649	0.00113	0.18	0.23	0.10152	0.512	1.084	0.641	0	0	2.1
15:40:00	0.228	0.10151	0.521	1.069	0.649	0.00113	0.18	0.23	0.10151	0.512	1.084	0.641	0	0	2.1
15:45:00	0.228	0.10151	0.521	1.069	0.649	0.00113	0.18	0.23	0.10151	0.512	1.084	0.641	0	0	2.1
15:50:00	0.228	0.10151	0.521	1.069	0.649	0.00113	0.18	0.23	0.10151	0.512	1.084	0.641	0	0	2.1
15:55:00	0.228	0.10151	0.521	1.069	0.649	0.00113	0.18	0.23	0.10151	0.512	1.084	0.641	0	0	2.1
16:00:00	0.228	0.10151	0.521	1.069	0.649	0.00113	0.18	0.23	0.10151	0.512	1.084	0.641	0	0	2.1
16:05:00	0.226	0.09931	0.518	1.067	0.642	0.00112	0.18	0.228	0.09911	0.509	1.081	0.634	0	0	2.1
16:10:00	0.22	0.09198	0.507	1.059	0.62	0.00109	0.17	0.221	0.09167	0.499	1.073	0.612	0	0	2
16:15:00	0.214	0.08683	0.506	1.053	0.61	0.0011	0.17	0.215	0.08664	0.498	1.067	0.602	0	0	1.9
16:20:00	0.211	0.08486	0.509	1.049	0.608	0.00112	0.16	0.212	0.08479	0.5	1.064	0.6	0	0	1.9
16:25:00	0.21	0.08432	0.51	1.048	0.608	0.00112	0.16	0.211	0.08431	0.501	1.063	0.601	0	0	1.8
16:30:00	0.209	0.08421	0.511	1.048	0.609	0.00113	0.16	0.211	0.08421	0.502	1.063	0.601	0	0	1.8
16:35:00	0.209	0.08418	0.511	1.048	0.609	0.00113	0.16	0.211	0.08418	0.502	1.063	0.601	0	0	1.8
16:40:00	0.209	0.08418	0.511	1.048	0.609	0.00113	0.16	0.211	0.08418	0.502	1.063	0.601	0	0	1.8
16:45:00	0.209	0.08418	0.511	1.048	0.609	0.00113	0.16	0.211	0.08418	0.502	1.063	0.601	0	0	1.8
16:50:00	0.209	0.08418	0.511	1.048	0.609	0.00113	0.16	0.211	0.08418	0.502	1.063	0.601	0	0	1.8
16:55:00	0.209	0.08418	0.511	1.048	0.609	0.00113	0.16	0.211	0.08418	0.502	1.063	0.601	0	0	1.8
17:00:00	0.209	0.08418	0.511	1.048	0.609	0.00113	0.16	0.211	0.08418	0.502	1.063	0.601	0	0	1.8
17:05:00	0.208	0.08272	0.508	1.047	0.604	0.00112	0.16	0.21	0.08258	0.499	1.061	0.595	0	0	1.8
17:10:00	0.203	0.07746	0.499	1.04	0.585	0.00109	0.16	0.204	0.07721	0.491	1.054	0.578	0	0	1.8
17:15:00	0.198	0.07344	0.497	1.035	0.576	0.0011	0.15	0.199	0.07328	0.489	1.049	0.568	0	0	1.7

17:20:00	0.195	0.07183	0.499	1.032	0.574	0.00111	0.15	0.197	0.07177	0.49	1.046	0.566	0	0	1.7
17:25:00	0.195	0.07138	0.5	1.031	0.574	0.00112	0.15	0.196	0.07136	0.491	1.046	0.566	0	0	1.7
17:30:00	0.194	0.07128	0.501	1.031	0.574	0.00112	0.15	0.196	0.07127	0.492	1.045	0.566	0	0	1.7
17:35:00	0.194	0.07126	0.501	1.031	0.574	0.00112	0.15	0.196	0.07126	0.492	1.045	0.566	0	0	1.7
17:40:00	0.194	0.07125	0.501	1.031	0.574	0.00112	0.15	0.196	0.07125	0.492	1.045	0.566	0	0	1.7
17:45:00	0.194	0.07125	0.501	1.031	0.574	0.00112	0.15	0.196	0.07125	0.492	1.045	0.566	0	0	1.7
17:50:00	0.194	0.07125	0.501	1.031	0.574	0.00112	0.15	0.196	0.07125	0.492	1.045	0.566	0	0	1.7
17:55:00	0.194	0.07125	0.501	1.031	0.574	0.00112	0.15	0.196	0.07125	0.492	1.045	0.566	0	0	1.7
18:00:00	0.187	0.06439	0.488	1.022	0.548	0.00108	0.14	0.188	0.06365	0.476	1.036	0.536	0	0	1.6
18:10:00	0.159	0.04046	0.42	0.989	0.435	0.00092	0.12	0.159	0.03914	0.411	1.001	0.424	0	0	1.2
18:15:00	0.126	0.02138	0.355	0.951	0.325	0.00088	0.1	0.124	0.02031	0.345	0.962	0.314	0	0	0.9
18:20:00	0.099	0.01049	0.281	0.921	0.228	0.0009	0.08	0.098	0.0098	0.269	0.933	0.216	0	0	0.6
18:25:00	0.081	0.00465	0.191	0.902	0.136	0.00093	0.06	0.08	0.00427	0.179	0.914	0.127	0	0	0.4
18:30:00	0.072	0.00187	0.1	0.892	0.066	0.00094	0.06	0.072	0.0017	0.093	0.905	0.061	0	0	0.4
18:35:00	0.068	0.00073	0.045	0.888	0.028	0.00096	0.05	0.068	0.00066	0.041	0.901	0.026	0	0	0.3
18:40:00	0.067	0.00031	0.02	0.887	0.012	0.00096	0.05	0.066	0.00028	0.018	0.899	0.011	0	0	0.3
18:45:00	0.066	0.00017	0.012	0.886	0.007	0.00097	0.05	0.066	0.00017	0.011	0.899	0.007	0	0	0.3
18:50:00	0.066	0.00014	0.009	0.886	0.006	0.00097	0.05	0.066	0.00014	0.009	0.899	0.006	0	0	0.3
18:55:00	0.066	0.00013	0.009	0.886	0.005	0.00098	0.05	0.066	0.00013	0.009	0.899	0.005	0	0	0.3
19:00:00	0.066	0.00013	0.009	0.886	0.005	0.00098	0.05	0.066	0.00013	0.009	0.899	0.005	0	0	0.3
19:05:00	0.066	0.00013	0.008	0.886	0.005	0.00098	0.05	0.065	0.00012	0.008	0.898	0.005	0	0	0.3
19:10:00	0.065	0.00011	0.007	0.885	0.004	0.00098	0.05	0.065	0.00011	0.007	0.898	0.004	0	0	0.3
19:15:00	0.065	0.00008	0.005	0.885	0.003	0.00098	0.05	0.065	0.00007	0.005	0.898	0.003	0	0	0.3
19:20:00	0.065	0.00004	0.003	0.885	0.002	0.00098	0.05	0.065	0.00004	0.003	0.898	0.002	0	0	0.3
19:25:00	0.065	0.00002	0.002	0.885	0.001	0.00098	0.05	0.065	0.00002	0.001	0.898	0.001	0	0	0.3
19:30:00	0.065	0.00001	0.001	0.885	0	0.00098	0.05	0.065	0.00001	0.001	0.898	0	0	0	0.3
19:35:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
19:40:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
19:45:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
19:50:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
19:55:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:00:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:05:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:10:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:15:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:20:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:25:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:30:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:35:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:40:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:45:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:50:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
20:55:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:00:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3

21:05:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:10:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:15:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:20:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:25:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:30:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:35:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:40:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:45:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:50:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
21:55:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:00:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:05:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:10:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:15:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:20:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:25:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:30:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:35:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:40:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:45:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:50:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
22:55:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:00:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:05:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:10:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:15:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:20:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:25:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:30:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:35:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:40:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:45:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:50:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
23:55:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3
0:00:00	0.065	0	0	0.885	0	0.00098	0.05	0.065	0	0	0.898	0	0	0	0.3

TRAMO B



	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
0:05:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
0:10:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
0:15:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
0:20:00	0.069	0.00201	0.119	0.519	0.076	0.00224	0.05	0.071	0.00284	0.158	0.561	0.103	0	0	0.5
0:25:00	0.101	0.01929	0.493	0.559	0.404	0.0023	0.08	0.104	0.02089	0.503	0.603	0.419	0	0	0.9
0:30:00	0.13	0.0402	0.62	0.598	0.579	0.0023	0.1	0.134	0.04141	0.609	0.641	0.576	0	0	1.3
0:35:00	0.148	0.05642	0.676	0.621	0.674	0.00234	0.12	0.152	0.05704	0.65	0.664	0.656	0	0	1.6
0:40:00	0.155	0.06295	0.688	0.63	0.703	0.00233	0.12	0.159	0.06314	0.66	0.673	0.681	0	0	1.7
0:45:00	0.157	0.0647	0.691	0.633	0.71	0.00233	0.12	0.161	0.06474	0.662	0.675	0.687	0	0	1.7
0:50:00	0.158	0.06508	0.692	0.633	0.711	0.00232	0.12	0.161	0.06509	0.662	0.675	0.688	0	0	1.7
0:55:00	0.158	0.06515	0.692	0.633	0.711	0.00232	0.12	0.161	0.06515	0.662	0.675	0.689	0	0	1.7
1:00:00	0.158	0.06516	0.692	0.633	0.711	0.00232	0.12	0.161	0.06516	0.662	0.675	0.689	0	0	1.7
1:05:00	0.159	0.06676	0.696	0.635	0.719	0.00234	0.13	0.163	0.06696	0.667	0.678	0.697	0	0	1.8
1:10:00	0.164	0.07151	0.706	0.641	0.74	0.00235	0.13	0.168	0.07175	0.675	0.684	0.717	0	0	1.8
1:15:00	0.167	0.07508	0.712	0.646	0.754	0.00235	0.13	0.171	0.07522	0.68	0.688	0.729	0	0	1.9
1:20:00	0.169	0.07691	0.714	0.648	0.76	0.00235	0.13	0.173	0.07697	0.682	0.69	0.735	0	0	1.9
1:25:00	0.169	0.07759	0.715	0.649	0.763	0.00235	0.13	0.173	0.07761	0.683	0.691	0.738	0	0	1.9
1:30:00	0.17	0.07777	0.715	0.649	0.764	0.00235	0.13	0.174	0.07778	0.683	0.691	0.738	0	0	1.9
1:35:00	0.17	0.07782	0.715	0.649	0.764	0.00235	0.13	0.174	0.07782	0.683	0.691	0.738	0	0	1.9
1:40:00	0.17	0.07782	0.715	0.649	0.764	0.00235	0.13	0.174	0.07782	0.683	0.691	0.738	0	0	1.9
1:45:00	0.17	0.07782	0.715	0.649	0.764	0.00235	0.13	0.174	0.07782	0.683	0.691	0.738	0	0	1.9
1:50:00	0.17	0.07782	0.715	0.649	0.764	0.00235	0.13	0.174	0.07782	0.683	0.691	0.738	0	0	1.9
1:55:00	0.17	0.07782	0.715	0.649	0.764	0.00235	0.13	0.174	0.07782	0.683	0.691	0.738	0	0	1.9
2:00:00	0.17	0.07782	0.715	0.649	0.764	0.00235	0.13	0.174	0.07782	0.683	0.691	0.738	0	0	1.9
2:05:00	0.172	0.08021	0.721	0.652	0.774	0.00236	0.14	0.176	0.08049	0.689	0.694	0.749	0	0	2
2:10:00	0.177	0.08689	0.731	0.66	0.799	0.00238	0.14	0.182	0.0872	0.698	0.702	0.773	0	0	2.1
2:15:00	0.182	0.09167	0.736	0.665	0.815	0.00238	0.14	0.186	0.09185	0.702	0.708	0.787	0	0	2.2

2:20:00	0.184	0.09396	0.739	0.668	0.822	0.00238	0.14	0.188	0.09403	0.704	0.71	0.794	0	0	2.2
2:25:00	0.184	0.09473	0.739	0.669	0.824	0.00238	0.15	0.189	0.09475	0.705	0.711	0.796	0	0	2.2
2:30:00	0.184	0.09493	0.739	0.669	0.825	0.00238	0.15	0.189	0.09494	0.705	0.711	0.796	0	0	2.2
2:35:00	0.184	0.09497	0.739	0.669	0.825	0.00238	0.15	0.189	0.09497	0.705	0.711	0.796	0	0	2.2
2:40:00	0.184	0.09498	0.739	0.669	0.825	0.00238	0.15	0.189	0.09498	0.705	0.711	0.796	0	0	2.2
2:45:00	0.184	0.09498	0.739	0.669	0.825	0.00238	0.15	0.189	0.09498	0.705	0.711	0.796	0	0	2.2
2:50:00	0.184	0.09498	0.739	0.669	0.825	0.00238	0.15	0.189	0.09498	0.705	0.711	0.796	0	0	2.2
2:55:00	0.184	0.09498	0.739	0.669	0.825	0.00238	0.15	0.189	0.09498	0.705	0.711	0.796	0	0	2.2
3:00:00	0.184	0.09498	0.739	0.669	0.825	0.00238	0.15	0.189	0.09498	0.705	0.711	0.796	0	0	2.2
3:05:00	0.187	0.09877	0.746	0.673	0.839	0.0024	0.15	0.192	0.09917	0.712	0.716	0.811	0	0	2.3
3:10:00	0.195	0.10863	0.757	0.684	0.87	0.00241	0.15	0.2	0.10905	0.721	0.726	0.84	0	0	2.4
3:15:00	0.2	0.11528	0.762	0.691	0.888	0.00242	0.16	0.206	0.11558	0.726	0.733	0.857	0	0	2.5
3:20:00	0.203	0.11818	0.764	0.693	0.896	0.00242	0.16	0.208	0.11826	0.727	0.736	0.863	0	0	2.5
3:25:00	0.203	0.11908	0.765	0.694	0.898	0.00242	0.16	0.209	0.11918	0.727	0.737	0.865	0	0	2.5
3:30:00	0.203	0.11929	0.765	0.695	0.898	0.00242	0.16	0.209	0.11929	0.728	0.737	0.866	0	0	2.5
3:35:00	0.204	0.11933	0.765	0.695	0.898	0.00242	0.16	0.209	0.11933	0.728	0.737	0.866	0	0	2.5
3:40:00	0.204	0.11934	0.765	0.695	0.898	0.00242	0.16	0.209	0.11934	0.728	0.737	0.866	0	0	2.5
3:45:00	0.204	0.11934	0.765	0.695	0.898	0.00242	0.16	0.209	0.11934	0.728	0.737	0.866	0	0	2.5
3:50:00	0.204	0.11934	0.765	0.695	0.898	0.00242	0.16	0.209	0.11934	0.728	0.737	0.866	0	0	2.5
3:55:00	0.204	0.11934	0.765	0.695	0.898	0.00242	0.16	0.209	0.11934	0.728	0.737	0.866	0	0	2.5
4:00:00	0.204	0.11934	0.765	0.695	0.898	0.00242	0.16	0.209	0.11934	0.728	0.737	0.866	0	0	2.5
4:05:00	0.208	0.12578	0.773	0.701	0.918	0.00244	0.16	0.214	0.12648	0.736	0.744	0.887	0	0	2.6
4:10:00	0.219	0.14111	0.785	0.715	0.957	0.00246	0.17	0.225	0.14168	0.746	0.758	0.923	0	0	2.8
4:15:00	0.225	0.15066	0.79	0.724	0.978	0.00247	0.18	0.232	0.15093	0.75	0.767	0.943	0	0	2.9
4:20:00	0.228	0.15443	0.792	0.728	0.986	0.00247	0.18	0.234	0.15452	0.752	0.77	0.95	0	0	3
4:25:00	0.229	0.15549	0.792	0.729	0.989	0.00247	0.18	0.235	0.15551	0.752	0.771	0.951	0	0	3
4:30:00	0.229	0.15572	0.792	0.729	0.989	0.00247	0.18	0.235	0.15573	0.752	0.771	0.952	0	0	3
4:35:00	0.229	0.15577	0.792	0.729	0.989	0.00247	0.18	0.235	0.15577	0.752	0.771	0.952	0	0	3
4:40:00	0.229	0.15577	0.792	0.729	0.989	0.00247	0.18	0.235	0.15577	0.752	0.771	0.952	0	0	3
4:45:00	0.229	0.15577	0.792	0.729	0.989	0.00247	0.18	0.235	0.15577	0.752	0.771	0.952	0	0	3
4:50:00	0.229	0.15577	0.792	0.729	0.989	0.00247	0.18	0.235	0.15577	0.752	0.771	0.952	0	0	3
4:55:00	0.229	0.15577	0.792	0.729	0.989	0.00247	0.18	0.235	0.15577	0.752	0.771	0.952	0	0	3
5:00:00	0.229	0.15577	0.792	0.729	0.989	0.00247	0.18	0.235	0.15577	0.752	0.771	0.952	0	0	3
5:05:00	0.236	0.16777	0.803	0.739	1.019	0.0025	0.19	0.243	0.16879	0.763	0.782	0.983	0	0	3.2
5:10:00	0.252	0.19336	0.814	0.76	1.07	0.00253	0.2	0.259	0.19423	0.773	0.804	1.031	0	0	3.5
5:15:00	0.261	0.20773	0.819	0.772	1.095	0.00253	0.21	0.268	0.20808	0.776	0.815	1.053	0	0	3.6
5:20:00	0.264	0.21268	0.82	0.776	1.103	0.00253	0.21	0.271	0.21278	0.777	0.818	1.06	0	0	3.7
5:25:00	0.265	0.21391	0.82	0.777	1.104	0.00253	0.21	0.272	0.21393	0.777	0.819	1.062	0	0	3.7
5:30:00	0.265	0.21416	0.82	0.777	1.105	0.00253	0.21	0.272	0.21416	0.777	0.82	1.062	0	0	3.7
5:35:00	0.265	0.2142	0.82	0.777	1.105	0.00253	0.21	0.272	0.2142	0.777	0.82	1.062	0	0	3.7
5:40:00	0.265	0.21421	0.82	0.777	1.105	0.00253	0.21	0.272	0.21421	0.777	0.82	1.062	0	0	3.7
5:45:00	0.265	0.21421	0.82	0.777	1.105	0.00253	0.21	0.272	0.21421	0.777	0.82	1.062	0	0	3.7
5:50:00	0.265	0.21421	0.82	0.777	1.105	0.00253	0.21	0.272	0.21421	0.777	0.82	1.062	0	0	3.7
5:55:00	0.265	0.21421	0.82	0.777	1.105	0.00253	0.21	0.272	0.21421	0.777	0.82	1.062	0	0	3.7
6:00:00	0.265	0.21421	0.82	0.777	1.105	0.00253	0.21	0.272	0.21421	0.777	0.82	1.062	0	0	3.7

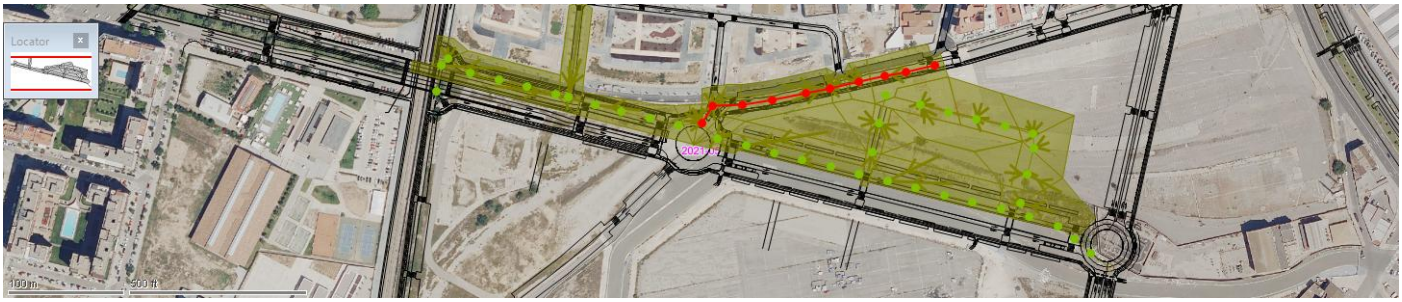
6:05:00	0.278	0.23975	0.834	0.796	1.154	0.00259	0.22	0.286	0.24157	0.793	0.84	1.114	0	0	4
6:10:00	0.303	0.28665	0.845	0.829	1.223	0.00262	0.24	0.311	0.28795	0.802	0.872	1.178	0	0	4.5
6:15:00	0.314	0.30935	0.848	0.844	1.252	0.00262	0.25	0.323	0.30979	0.803	0.887	1.204	0	0	4.7
6:20:00	0.317	0.31592	0.848	0.848	1.259	0.00262	0.25	0.326	0.31603	0.803	0.891	1.211	0	0	4.8
6:25:00	0.318	0.31734	0.849	0.849	1.261	0.00262	0.25	0.327	0.31736	0.803	0.892	1.212	0	0	4.8
6:30:00	0.318	0.31759	0.849	0.849	1.261	0.00262	0.25	0.327	0.31759	0.803	0.892	1.212	0	0	4.8
6:35:00	0.318	0.31763	0.849	0.849	1.261	0.00262	0.25	0.327	0.31763	0.803	0.892	1.212	0	0	4.8
6:40:00	0.318	0.31763	0.849	0.849	1.261	0.00262	0.25	0.327	0.31763	0.803	0.892	1.212	0	0	4.8
6:45:00	0.318	0.31763	0.849	0.849	1.261	0.00262	0.25	0.327	0.31763	0.803	0.892	1.212	0	0	4.8
6:50:00	0.318	0.31763	0.849	0.849	1.261	0.00262	0.25	0.327	0.31763	0.803	0.892	1.212	0	0	4.8
6:55:00	0.318	0.31763	0.849	0.849	1.261	0.00262	0.25	0.327	0.31763	0.803	0.892	1.212	0	0	4.8
7:00:00	0.318	0.31763	0.849	0.849	1.261	0.00262	0.25	0.327	0.31763	0.803	0.892	1.212	0	0	4.8
7:05:00	0.346	0.38302	0.868	0.889	1.35	0.00272	0.27	0.357	0.3868	0.825	0.934	1.306	0	0	5.4
7:10:00	0.388	0.48162	0.876	0.945	1.449	0.00276	0.31	0.399	0.48368	0.83	0.989	1.397	0	0	6.4
7:15:00	0.403	0.51921	0.876	0.965	1.482	0.00277	0.32	0.415	0.51976	0.83	1.008	1.425	0	0	6.7
7:20:00	0.407	0.52821	0.876	0.97	1.489	0.00277	0.32	0.418	0.52832	0.829	1.013	1.432	0	0	6.8
7:25:00	0.407	0.53001	0.876	0.97	1.49	0.00277	0.32	0.419	0.53003	0.829	1.014	1.433	0	0	6.8
7:30:00	0.407	0.53034	0.876	0.971	1.491	0.00277	0.32	0.419	0.53035	0.829	1.014	1.433	0	0	6.8
7:35:00	0.407	0.5304	0.876	0.971	1.491	0.00277	0.32	0.419	0.5304	0.829	1.014	1.433	0	0	6.8
7:40:00	0.407	0.53041	0.876	0.971	1.491	0.00277	0.32	0.419	0.53041	0.829	1.014	1.433	0	0	6.8
7:45:00	0.407	0.53041	0.876	0.971	1.491	0.00277	0.32	0.419	0.53041	0.829	1.014	1.433	0	0	6.8
7:50:00	0.407	0.53041	0.876	0.971	1.491	0.00277	0.32	0.419	0.53041	0.829	1.014	1.433	0	0	6.8
7:55:00	0.407	0.53041	0.876	0.971	1.491	0.00277	0.32	0.419	0.53041	0.829	1.014	1.433	0	0	6.8
8:00:00	0.407	0.53041	0.876	0.971	1.491	0.00277	0.32	0.419	0.53041	0.829	1.014	1.433	0	0	6.8
8:05:00	0.485	0.76247	0.901	1.08	1.69	0.00297	0.38	0.5	0.77206	0.858	1.127	1.639	0	0	8.6
8:10:00	0.56	1.00517	0.9	1.182	1.837	0.00307	0.44	0.578	1.00849	0.851	1.227	1.77	0	0	10.5
8:15:00	0.582	1.08181	0.899	1.212	1.878	0.00311	0.46	0.601	1.08255	0.848	1.257	1.806	0	0	11
8:20:00	0.586	1.09549	0.898	1.218	1.885	0.00311	0.47	0.605	1.09561	0.847	1.262	1.812	0	0	11.1
8:25:00	0.587	1.09789	0.898	1.218	1.887	0.00311	0.47	0.605	1.09791	0.847	1.263	1.813	0	0	11.1
8:30:00	0.587	1.09834	0.898	1.219	1.887	0.00312	0.47	0.606	1.09834	0.847	1.263	1.813	0	0	11.1
8:35:00	0.587	1.09843	0.898	1.219	1.887	0.00312	0.47	0.606	1.09843	0.847	1.263	1.813	0	0	11.1
8:40:00	0.587	1.09844	0.898	1.219	1.887	0.00312	0.47	0.606	1.09844	0.847	1.263	1.813	0	0	11.1
8:45:00	0.587	1.09845	0.898	1.219	1.887	0.00312	0.47	0.606	1.09845	0.847	1.263	1.813	0	0	11.1
8:50:00	0.587	1.09845	0.898	1.219	1.887	0.00312	0.47	0.606	1.09845	0.847	1.263	1.813	0	0	11.1
8:55:00	0.587	1.09845	0.898	1.219	1.887	0.00312	0.47	0.606	1.09845	0.847	1.263	1.813	0	0	11.1
9:00:00	0.587	1.09845	0.898	1.219	1.887	0.00312	0.47	0.606	1.09845	0.847	1.263	1.813	0	0	11.1
9:05:00	0.541	0.92936	0.89	1.152	1.779	0.00298	0.43	0.557	0.92415	0.837	1.194	1.703	0	0	10
9:10:00	0.498	0.79303	0.889	1.094	1.694	0.00292	0.39	0.513	0.79116	0.839	1.138	1.626	0	0	9
9:15:00	0.485	0.75361	0.889	1.077	1.668	0.0029	0.38	0.5	0.75302	0.84	1.12	1.603	0	0	8.6
9:20:00	0.481	0.74102	0.889	1.071	1.66	0.0029	0.38	0.495	0.74085	0.84	1.115	1.595	0	0	8.5
9:25:00	0.48	0.73762	0.889	1.07	1.658	0.00289	0.38	0.494	0.73758	0.84	1.113	1.594	0	0	8.5
9:30:00	0.48	0.73675	0.889	1.069	1.657	0.00289	0.38	0.494	0.73674	0.84	1.113	1.593	0	0	8.5
9:35:00	0.479	0.73653	0.889	1.069	1.657	0.00289	0.38	0.494	0.73653	0.84	1.113	1.593	0	0	8.5
9:40:00	0.479	0.73648	0.889	1.069	1.657	0.00289	0.38	0.494	0.73648	0.84	1.113	1.593	0	0	8.5
9:45:00	0.479	0.73647	0.889	1.069	1.657	0.00289	0.38	0.494	0.73647	0.84	1.113	1.593	0	0	8.5

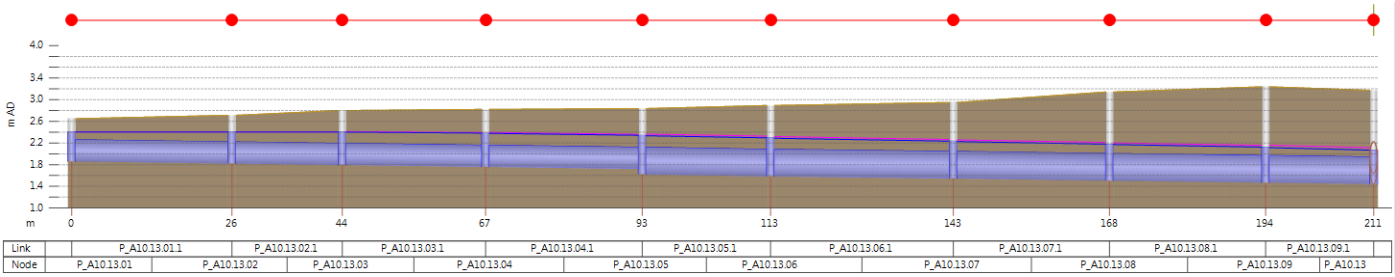
9:50:00	0.479	0.73646	0.889	1.069	1.657	0.00289	0.38	0.494	0.73646	0.84	1.113	1.593	0	0	8.5
9:55:00	0.479	0.73646	0.889	1.069	1.657	0.00289	0.38	0.494	0.73646	0.84	1.113	1.593	0	0	8.5
10:00:00	0.479	0.73646	0.889	1.069	1.657	0.00289	0.38	0.494	0.73646	0.84	1.113	1.593	0	0	8.5
10:05:00	0.438	0.61029	0.875	1.011	1.551	0.00278	0.35	0.45	0.60539	0.824	1.052	1.483	0	0	7.5
10:10:00	0.387	0.47502	0.866	0.942	1.433	0.0027	0.31	0.398	0.47228	0.817	0.984	1.372	0	0	6.3
10:15:00	0.365	0.4223	0.864	0.912	1.383	0.00269	0.29	0.375	0.4214	0.816	0.955	1.327	0	0	5.8
10:20:00	0.359	0.40747	0.863	0.904	1.368	0.00268	0.28	0.369	0.40725	0.816	0.947	1.314	0	0	5.7
10:25:00	0.357	0.40418	0.863	0.902	1.365	0.00268	0.28	0.367	0.40414	0.817	0.945	1.312	0	0	5.7
10:30:00	0.357	0.40357	0.863	0.902	1.364	0.00268	0.28	0.367	0.40356	0.817	0.945	1.311	0	0	5.7
10:35:00	0.357	0.40347	0.863	0.902	1.364	0.00268	0.28	0.367	0.40347	0.817	0.945	1.311	0	0	5.7
10:40:00	0.357	0.40345	0.863	0.902	1.364	0.00268	0.28	0.367	0.40345	0.817	0.945	1.311	0	0	5.7
10:45:00	0.357	0.40345	0.863	0.902	1.364	0.00268	0.28	0.367	0.40345	0.817	0.945	1.311	0	0	5.7
10:50:00	0.357	0.40345	0.863	0.902	1.364	0.00268	0.28	0.367	0.40345	0.817	0.945	1.311	0	0	5.7
10:55:00	0.357	0.40345	0.863	0.902	1.364	0.00268	0.28	0.367	0.40345	0.817	0.945	1.311	0	0	5.7
11:00:00	0.357	0.40345	0.863	0.902	1.364	0.00268	0.28	0.367	0.40345	0.817	0.945	1.311	0	0	5.7
11:05:00	0.339	0.3599	0.851	0.876	1.309	0.00262	0.27	0.348	0.35757	0.803	0.918	1.253	0	0	5.3
11:10:00	0.31	0.29807	0.84	0.837	1.231	0.00258	0.24	0.318	0.29648	0.794	0.879	1.179	0	0	4.6
11:15:00	0.295	0.2698	0.836	0.817	1.193	0.00257	0.23	0.303	0.26921	0.791	0.86	1.145	0	0	4.3
11:20:00	0.29	0.26084	0.835	0.811	1.181	0.00257	0.23	0.298	0.26068	0.79	0.854	1.134	0	0	4.2
11:25:00	0.289	0.25869	0.834	0.81	1.178	0.00257	0.23	0.297	0.25865	0.79	0.852	1.132	0	0	4.2
11:30:00	0.289	0.25827	0.834	0.809	1.177	0.00257	0.23	0.297	0.25826	0.79	0.852	1.132	0	0	4.2
11:35:00	0.289	0.2582	0.834	0.809	1.177	0.00257	0.23	0.297	0.2582	0.79	0.852	1.132	0	0	4.2
11:40:00	0.289	0.25819	0.834	0.809	1.177	0.00257	0.23	0.297	0.25819	0.79	0.852	1.131	0	0	4.2
11:45:00	0.289	0.25819	0.834	0.809	1.177	0.00257	0.23	0.297	0.25819	0.79	0.852	1.131	0	0	4.2
11:50:00	0.289	0.25819	0.834	0.809	1.177	0.00257	0.23	0.297	0.25819	0.79	0.852	1.131	0	0	4.2
11:55:00	0.289	0.25819	0.834	0.809	1.177	0.00257	0.23	0.297	0.25819	0.79	0.852	1.131	0	0	4.2
12:00:00	0.289	0.25819	0.834	0.809	1.177	0.00257	0.23	0.297	0.25819	0.79	0.852	1.131	0	0	4.2
12:05:00	0.279	0.23942	0.825	0.796	1.144	0.00253	0.22	0.287	0.23816	0.78	0.838	1.096	0	0	4
12:10:00	0.261	0.2069	0.814	0.771	1.088	0.0025	0.21	0.268	0.2059	0.77	0.813	1.044	0	0	3.6
12:15:00	0.251	0.18987	0.808	0.758	1.058	0.00249	0.2	0.257	0.18937	0.766	0.8	1.017	0	0	3.4
12:20:00	0.247	0.18359	0.807	0.753	1.047	0.00249	0.19	0.253	0.18346	0.765	0.795	1.007	0	0	3.4
12:25:00	0.246	0.18189	0.806	0.751	1.044	0.00249	0.19	0.252	0.18186	0.764	0.794	1.004	0	0	3.3
12:30:00	0.245	0.18152	0.806	0.751	1.044	0.00249	0.19	0.252	0.18152	0.764	0.793	1.004	0	0	3.3
12:35:00	0.245	0.18146	0.806	0.751	1.043	0.00249	0.19	0.252	0.18146	0.764	0.793	1.004	0	0	3.3
12:40:00	0.245	0.18145	0.806	0.751	1.043	0.00249	0.19	0.252	0.18145	0.764	0.793	1.004	0	0	3.3
12:45:00	0.245	0.18145	0.806	0.751	1.043	0.00249	0.19	0.252	0.18145	0.764	0.793	1.004	0	0	3.3
12:50:00	0.245	0.18145	0.806	0.751	1.043	0.00249	0.19	0.252	0.18145	0.764	0.793	1.004	0	0	3.3
12:55:00	0.245	0.18145	0.806	0.751	1.043	0.00249	0.19	0.252	0.18145	0.764	0.793	1.004	0	0	3.3
13:00:00	0.245	0.18145	0.806	0.751	1.043	0.00249	0.19	0.252	0.18145	0.764	0.793	1.004	0	0	3.3
13:05:00	0.24	0.172	0.799	0.743	1.022	0.00247	0.19	0.246	0.17125	0.756	0.785	0.981	0	0	3.2
13:10:00	0.228	0.15306	0.788	0.727	0.98	0.00244	0.18	0.233	0.15239	0.746	0.769	0.941	0	0	3
13:15:00	0.22	0.14196	0.782	0.716	0.956	0.00244	0.17	0.226	0.14164	0.742	0.759	0.919	0	0	2.8
13:20:00	0.217	0.13747	0.779	0.712	0.945	0.00244	0.17	0.222	0.13736	0.74	0.755	0.91	0	0	2.8
13:25:00	0.216	0.13617	0.779	0.711	0.942	0.00244	0.17	0.221	0.13607	0.74	0.753	0.907	0	0	2.8
13:30:00	0.215	0.13578	0.779	0.711	0.942	0.00244	0.17	0.221	0.13577	0.74	0.753	0.907	0	0	2.8

13:35:00	0.215	0.13572	0.778	0.711	0.942	0.00244	0.17	0.221	0.13572	0.74	0.753	0.907	0	0	2.8
13:40:00	0.215	0.13571	0.778	0.711	0.941	0.00244	0.17	0.221	0.13571	0.74	0.753	0.907	0	0	2.8
13:45:00	0.215	0.13571	0.778	0.711	0.941	0.00244	0.17	0.221	0.13571	0.74	0.753	0.907	0	0	2.8
13:50:00	0.215	0.13571	0.778	0.711	0.941	0.00244	0.17	0.221	0.13571	0.74	0.753	0.907	0	0	2.8
13:55:00	0.215	0.13571	0.778	0.711	0.941	0.00244	0.17	0.221	0.13571	0.74	0.753	0.907	0	0	2.8
14:00:00	0.215	0.13571	0.778	0.711	0.941	0.00244	0.17	0.221	0.13571	0.74	0.753	0.907	0	0	2.8
14:05:00	0.212	0.13041	0.772	0.706	0.926	0.00242	0.17	0.217	0.12992	0.733	0.748	0.89	0	0	2.7
14:10:00	0.203	0.11851	0.762	0.694	0.894	0.0024	0.16	0.208	0.11804	0.724	0.736	0.86	0	0	2.5
14:15:00	0.197	0.11089	0.756	0.686	0.873	0.0024	0.16	0.202	0.11065	0.719	0.728	0.841	0	0	2.4
14:20:00	0.195	0.10756	0.753	0.683	0.864	0.0024	0.15	0.199	0.10746	0.717	0.725	0.833	0	0	2.4
14:25:00	0.194	0.10645	0.752	0.681	0.861	0.0024	0.15	0.199	0.10642	0.716	0.724	0.83	0	0	2.4
14:30:00	0.193	0.10617	0.752	0.681	0.86	0.0024	0.15	0.198	0.10616	0.716	0.723	0.83	0	0	2.4
14:35:00	0.193	0.10611	0.752	0.681	0.86	0.0024	0.15	0.198	0.10611	0.716	0.723	0.83	0	0	2.4
14:40:00	0.193	0.1061	0.752	0.681	0.86	0.0024	0.15	0.198	0.1061	0.716	0.723	0.83	0	0	2.4
14:45:00	0.193	0.1061	0.752	0.681	0.86	0.0024	0.15	0.198	0.1061	0.716	0.723	0.83	0	0	2.4
14:50:00	0.193	0.1061	0.752	0.681	0.86	0.0024	0.15	0.198	0.1061	0.716	0.723	0.83	0	0	2.4
14:55:00	0.193	0.1061	0.752	0.681	0.86	0.0024	0.15	0.198	0.1061	0.716	0.723	0.83	0	0	2.4
15:00:00	0.193	0.1061	0.752	0.681	0.86	0.0024	0.15	0.198	0.1061	0.716	0.723	0.83	0	0	2.4
15:05:00	0.191	0.10289	0.747	0.678	0.849	0.00238	0.15	0.196	0.10256	0.711	0.72	0.818	0	0	2.3
15:10:00	0.185	0.09494	0.737	0.669	0.823	0.00237	0.15	0.189	0.09459	0.702	0.711	0.793	0	0	2.2
15:15:00	0.18	0.08955	0.731	0.663	0.806	0.00236	0.14	0.184	0.08936	0.697	0.705	0.777	0	0	2.1
15:20:00	0.178	0.08699	0.729	0.66	0.797	0.00236	0.14	0.182	0.08691	0.695	0.702	0.77	0	0	2.1
15:25:00	0.177	0.08607	0.728	0.659	0.794	0.00236	0.14	0.181	0.08604	0.694	0.701	0.767	0	0	2.1
15:30:00	0.177	0.08582	0.727	0.659	0.793	0.00236	0.14	0.181	0.08581	0.694	0.701	0.766	0	0	2.1
15:35:00	0.177	0.08576	0.727	0.659	0.793	0.00236	0.14	0.181	0.08576	0.694	0.701	0.766	0	0	2.1
15:40:00	0.177	0.08575	0.727	0.659	0.793	0.00236	0.14	0.181	0.08575	0.694	0.701	0.766	0	0	2.1
15:45:00	0.177	0.08575	0.727	0.659	0.793	0.00236	0.14	0.181	0.08575	0.694	0.701	0.766	0	0	2.1
15:50:00	0.177	0.08575	0.727	0.659	0.793	0.00236	0.14	0.181	0.08575	0.694	0.701	0.766	0	0	2.1
15:55:00	0.177	0.08575	0.727	0.659	0.793	0.00236	0.14	0.181	0.08575	0.694	0.701	0.766	0	0	2.1
16:00:00	0.177	0.08575	0.727	0.659	0.793	0.00236	0.14	0.181	0.08575	0.694	0.701	0.766	0	0	2.1
16:05:00	0.175	0.08368	0.723	0.656	0.785	0.00235	0.14	0.179	0.08345	0.689	0.698	0.757	0	0	2
16:10:00	0.17	0.07814	0.714	0.65	0.764	0.00234	0.13	0.174	0.07788	0.681	0.692	0.737	0	0	2
16:15:00	0.166	0.07419	0.708	0.645	0.749	0.00233	0.13	0.17	0.07403	0.676	0.687	0.723	0	0	1.9
16:20:00	0.164	0.07217	0.705	0.642	0.741	0.00233	0.13	0.168	0.07211	0.674	0.684	0.716	0	0	1.9
16:25:00	0.164	0.07148	0.704	0.641	0.738	0.00234	0.13	0.167	0.07138	0.673	0.683	0.714	0	0	1.8
16:30:00	0.163	0.07118	0.704	0.641	0.737	0.00234	0.13	0.167	0.07117	0.673	0.683	0.713	0	0	1.8
16:35:00	0.163	0.07112	0.704	0.641	0.737	0.00234	0.13	0.167	0.07112	0.673	0.683	0.713	0	0	1.8
16:40:00	0.163	0.07111	0.704	0.641	0.737	0.00234	0.13	0.167	0.07111	0.673	0.683	0.713	0	0	1.8
16:45:00	0.163	0.07111	0.704	0.641	0.737	0.00234	0.13	0.167	0.07111	0.673	0.683	0.713	0	0	1.8
16:50:00	0.163	0.07111	0.704	0.641	0.737	0.00234	0.13	0.167	0.07111	0.673	0.683	0.713	0	0	1.8
16:55:00	0.163	0.07111	0.704	0.641	0.737	0.00234	0.13	0.167	0.07111	0.673	0.683	0.713	0	0	1.8
17:00:00	0.162	0.06971	0.7	0.639	0.73	0.00233	0.13	0.166	0.06954	0.669	0.681	0.706	0	0	1.8
17:05:00	0.158	0.0657	0.691	0.634	0.713	0.00232	0.12	0.162	0.0655	0.661	0.676	0.689	0	0	1.8
17:10:00	0.155	0.06272	0.686	0.63	0.7	0.00231	0.12	0.159	0.0626	0.656	0.672	0.677	0	0	1.7

17:20:00	0.154	0.06112	0.682	0.628	0.693	0.00231	0.12	0.157	0.06106	0.653	0.67	0.671	0	0	1.7
17:25:00	0.153	0.06046	0.681	0.627	0.69	0.00231	0.12	0.156	0.06044	0.652	0.669	0.668	0	0	1.7
17:30:00	0.153	0.06025	0.681	0.627	0.689	0.00231	0.12	0.156	0.06025	0.652	0.669	0.667	0	0	1.7
17:35:00	0.153	0.0602	0.681	0.627	0.689	0.00231	0.12	0.156	0.0602	0.652	0.669	0.667	0	0	1.7
17:40:00	0.153	0.06019	0.681	0.627	0.689	0.00231	0.12	0.156	0.06019	0.652	0.669	0.667	0	0	1.7
17:45:00	0.153	0.06019	0.681	0.627	0.689	0.00231	0.12	0.156	0.06019	0.652	0.669	0.667	0	0	1.7
17:50:00	0.153	0.06019	0.681	0.627	0.689	0.00231	0.12	0.156	0.06019	0.652	0.669	0.667	0	0	1.7
17:55:00	0.153	0.06019	0.681	0.627	0.689	0.00231	0.12	0.156	0.06019	0.652	0.669	0.667	0	0	1.7
18:00:00	0.153	0.06019	0.681	0.627	0.689	0.00231	0.12	0.156	0.06019	0.652	0.669	0.667	0	0	1.7
18:05:00	0.147	0.05368	0.658	0.618	0.652	0.00226	0.11	0.149	0.05281	0.628	0.659	0.627	0	0	1.6
18:10:00	0.126	0.03473	0.576	0.59	0.528	0.00214	0.1	0.126	0.03358	0.556	0.629	0.51	0	0	1.2
18:15:00	0.105	0.02006	0.475	0.563	0.397	0.00208	0.08	0.104	0.01922	0.463	0.602	0.386	0	0	0.9
18:20:00	0.09	0.01144	0.373	0.544	0.286	0.00207	0.07	0.089	0.01091	0.367	0.583	0.278	0	0	0.7
18:25:00	0.08	0.00647	0.272	0.532	0.191	0.00208	0.06	0.079	0.00607	0.265	0.571	0.185	0	0	0.6
18:30:00	0.074	0.00344	0.177	0.524	0.118	0.0021	0.06	0.073	0.00324	0.17	0.563	0.112	0	0	0.5
18:35:00	0.069	0.00173	0.101	0.52	0.065	0.00211	0.05	0.069	0.00161	0.095	0.559	0.061	0	0	0.5
18:40:00	0.067	0.00082	0.052	0.517	0.032	0.00212	0.05	0.067	0.00076	0.048	0.557	0.03	0	0	0.5
18:45:00	0.066	0.00038	0.025	0.516	0.015	0.00213	0.05	0.066	0.00035	0.023	0.556	0.014	0	0	0.5
18:50:00	0.066	0.00019	0.013	0.516	0.008	0.00213	0.05	0.065	0.00018	0.012	0.555	0.007	0	0	0.5
18:55:00	0.065	0.00012	0.008	0.515	0.005	0.00213	0.05	0.065	0.00011	0.008	0.555	0.005	0	0	0.5
19:00:00	0.065	0.00009	0.006	0.515	0.004	0.00213	0.05	0.065	0.00009	0.006	0.555	0.004	0	0	0.4
19:05:00	0.065	0.00008	0.006	0.515	0.004	0.00214	0.05	0.065	0.00008	0.006	0.555	0.003	0	0	0.4
19:10:00	0.065	0.00007	0.005	0.515	0.003	0.00213	0.05	0.065	0.00007	0.004	0.555	0.003	0	0	0.4
19:15:00	0.065	0.00005	0.003	0.515	0.002	0.00214	0.05	0.065	0.00005	0.003	0.555	0.002	0	0	0.4
19:20:00	0.065	0.00004	0.002	0.515	0.001	0.00214	0.05	0.065	0.00003	0.002	0.555	0.001	0	0	0.4
19:25:00	0.065	0.00002	0.002	0.515	0.001	0.00214	0.05	0.065	0.00002	0.002	0.555	0.001	0	0	0.4
19:30:00	0.065	0.00001	0.001	0.515	0.001	0.00214	0.05	0.065	0.00001	0.001	0.555	0.001	0	0	0.4
19:35:00	0.065	0.00001	0.001	0.515	0	0.00214	0.05	0.065	0.00001	0	0.555	0	0	0	0.4
19:40:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
19:45:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
19:50:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
19:55:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:00:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:05:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:10:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:15:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:20:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:25:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:30:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:35:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:40:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:45:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:50:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
20:55:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:00:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4

21:05:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:10:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:15:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:20:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:25:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:30:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:35:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:40:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:45:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:50:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
21:55:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:00:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:05:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:10:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:15:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:20:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:25:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:30:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:35:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:40:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:45:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:50:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
22:55:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:00:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:05:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:10:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:15:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:20:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:25:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:30:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:35:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:40:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:45:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:50:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
23:55:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4
0:00:00	0.065	0	0	0.515	0	0.00214	0.05	0.065	0	0	0.555	0	0	0	0.4





	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.025	0	0	1.468	0	0.00148	0.05	0.025	0	0	1.494	0	0	0	0.1
0:05:00	0.025	0	0	1.468	0	0.00148	0.05	0.025	0	0	1.494	0	0	0	0.1
0:10:00	0.025	0	0	1.468	0	0.00148	0.05	0.025	0	0	1.494	0	0	0	0.1
0:15:00	0.025	0	0	1.468	0	0.00148	0.05	0.025	0	0	1.494	0	0	0	0.1
0:20:00	0.042	0.00091	0.222	1.485	0.117	0.00131	0.08	0.038	0.00121	0.343	1.509	0.174	0	0	0.1
0:25:00	0.084	0.00601	0.367	1.531	0.277	0.00111	0.17	0.077	0.00688	0.493	1.553	0.357	0	0	0.4
0:30:00	0.109	0.01008	0.365	1.558	0.317	0.00088	0.22	0.099	0.01038	0.46	1.575	0.378	0	0	0.5
0:35:00	0.117	0.01112	0.355	1.565	0.319	0.0008	0.23	0.105	0.0112	0.441	1.581	0.374	0	0	0.6
0:40:00	0.118	0.01136	0.353	1.567	0.319	0.00079	0.24	0.106	0.01138	0.437	1.582	0.373	0	0	0.6
0:45:00	0.119	0.01141	0.352	1.567	0.32	0.00078	0.24	0.106	0.01141	0.436	1.583	0.373	0	0	0.6
0:50:00	0.119	0.01142	0.352	1.567	0.32	0.00078	0.24	0.107	0.01142	0.436	1.583	0.373	0	0	0.6
0:55:00	0.119	0.01142	0.352	1.567	0.32	0.00078	0.24	0.107	0.01142	0.436	1.583	0.373	0	0	0.6
1:00:00	0.119	0.01142	0.352	1.567	0.32	0.00078	0.24	0.107	0.01142	0.436	1.583	0.373	0	0	0.6
1:05:00	0.121	0.01188	0.354	1.569	0.324	0.00079	0.24	0.109	0.01199	0.44	1.585	0.381	0	0	0.6
1:10:00	0.126	0.01293	0.356	1.575	0.333	0.00078	0.25	0.114	0.01303	0.439	1.59	0.389	0	0	0.6
1:15:00	0.129	0.01345	0.355	1.577	0.336	0.00076	0.26	0.116	0.01349	0.436	1.593	0.39	0	0	0.6
1:20:00	0.129	0.0136	0.355	1.578	0.337	0.00076	0.26	0.117	0.01361	0.434	1.594	0.39	0	0	0.7
1:25:00	0.13	0.01363	0.355	1.578	0.337	0.00076	0.26	0.117	0.01363	0.434	1.594	0.39	0	0	0.7
1:30:00	0.13	0.01364	0.355	1.579	0.337	0.00076	0.26	0.117	0.01364	0.434	1.594	0.39	0	0	0.7
1:35:00	0.13	0.01364	0.354	1.579	0.337	0.00076	0.26	0.117	0.01364	0.434	1.594	0.39	0	0	0.7
1:40:00	0.13	0.01364	0.354	1.579	0.337	0.00076	0.26	0.117	0.01364	0.434	1.594	0.39	0	0	0.7
1:45:00	0.13	0.01364	0.354	1.579	0.337	0.00076	0.26	0.117	0.01364	0.434	1.594	0.39	0	0	0.7
1:50:00	0.13	0.01364	0.354	1.579	0.337	0.00076	0.26	0.117	0.01364	0.434	1.594	0.39	0	0	0.7
1:55:00	0.13	0.01364	0.354	1.579	0.337	0.00076	0.26	0.117	0.01364	0.434	1.594	0.39	0	0	0.7
2:00:00	0.13	0.01364	0.354	1.579	0.337	0.00076	0.26	0.117	0.01364	0.434	1.594	0.39	0	0	0.7
2:05:00	0.133	0.0143	0.356	1.582	0.343	0.00076	0.27	0.12	0.01446	0.438	1.597	0.4	0	0	0.7
2:10:00	0.139	0.01573	0.358	1.588	0.353	0.00074	0.28	0.126	0.01586	0.436	1.604	0.408	0	0	0.7
2:15:00	0.142	0.0164	0.357	1.592	0.357	0.00073	0.28	0.129	0.01645	0.432	1.607	0.41	0	0	0.8
2:20:00	0.143	0.01659	0.356	1.593	0.357	0.00073	0.29	0.13	0.0166	0.43	1.607	0.41	0	0	0.8
2:25:00	0.143	0.01663	0.356	1.593	0.357	0.00073	0.29	0.13	0.01664	0.43	1.608	0.409	0	0	0.8

2:30:00	0.143	0.01664	0.356	1.593	0.357	0.00073	0.29	0.13	0.01664	0.43	1.608	0.409	0	0	0.8
2:35:00	0.143	0.01664	0.356	1.593	0.357	0.00073	0.29	0.13	0.01664	0.43	1.608	0.409	0	0	0.8
2:40:00	0.143	0.01664	0.356	1.593	0.357	0.00073	0.29	0.13	0.01664	0.43	1.608	0.409	0	0	0.8
2:45:00	0.143	0.01664	0.356	1.593	0.357	0.00073	0.29	0.13	0.01664	0.43	1.608	0.409	0	0	0.8
2:50:00	0.143	0.01664	0.356	1.593	0.357	0.00073	0.29	0.13	0.01664	0.43	1.608	0.409	0	0	0.8
2:55:00	0.143	0.01664	0.356	1.593	0.357	0.00073	0.29	0.13	0.01664	0.43	1.608	0.409	0	0	0.8
3:00:00	0.143	0.01664	0.356	1.593	0.357	0.00073	0.29	0.13	0.01664	0.43	1.608	0.409	0	0	0.8
3:05:00	0.148	0.01766	0.357	1.597	0.365	0.00073	0.3	0.134	0.01789	0.434	1.612	0.421	0	0	0.8
3:10:00	0.156	0.0197	0.358	1.606	0.377	0.00071	0.31	0.142	0.01987	0.431	1.621	0.431	0	0	0.9
3:15:00	0.16	0.0206	0.356	1.61	0.38	0.0007	0.32	0.146	0.02066	0.425	1.625	0.432	0	0	0.9
3:20:00	0.161	0.02085	0.356	1.612	0.381	0.00069	0.32	0.147	0.02086	0.424	1.626	0.432	0	0	0.9
3:25:00	0.161	0.0209	0.356	1.612	0.381	0.00069	0.32	0.148	0.0209	0.423	1.626	0.432	0	0	0.9
3:30:00	0.161	0.02091	0.356	1.612	0.381	0.00069	0.32	0.148	0.02091	0.423	1.626	0.432	0	0	0.9
3:35:00	0.161	0.02091	0.356	1.612	0.381	0.00069	0.32	0.148	0.02091	0.423	1.626	0.432	0	0	0.9
3:40:00	0.161	0.02091	0.356	1.612	0.381	0.00069	0.32	0.148	0.02091	0.423	1.626	0.432	0	0	0.9
3:45:00	0.161	0.02091	0.356	1.612	0.381	0.00069	0.32	0.148	0.02091	0.423	1.626	0.432	0	0	0.9
3:50:00	0.161	0.02091	0.356	1.612	0.381	0.00069	0.32	0.148	0.02091	0.423	1.626	0.432	0	0	0.9
3:55:00	0.161	0.02091	0.356	1.612	0.381	0.00069	0.32	0.148	0.02091	0.423	1.626	0.432	0	0	0.9
4:00:00	0.161	0.02091	0.356	1.612	0.381	0.00069	0.32	0.148	0.02091	0.423	1.626	0.432	0	0	0.9
4:05:00	0.168	0.02258	0.357	1.618	0.391	0.00069	0.34	0.154	0.02292	0.428	1.633	0.447	0	0	1
4:10:00	0.179	0.0256	0.356	1.63	0.405	0.00068	0.36	0.165	0.02583	0.422	1.645	0.457	0	0	1
4:15:00	0.184	0.02687	0.355	1.636	0.41	0.00067	0.37	0.17	0.02694	0.416	1.649	0.458	0	0	1.1
4:20:00	0.185	0.02721	0.354	1.637	0.411	0.00066	0.37	0.171	0.02723	0.414	1.651	0.458	0	0	1.1
4:25:00	0.186	0.02728	0.354	1.637	0.411	0.00066	0.37	0.171	0.02729	0.413	1.651	0.458	0	0	1.1
4:30:00	0.186	0.0273	0.354	1.637	0.411	0.00066	0.37	0.171	0.0273	0.413	1.651	0.458	0	0	1.1
4:35:00	0.186	0.0273	0.354	1.637	0.411	0.00066	0.37	0.171	0.0273	0.413	1.651	0.458	0	0	1.1
4:40:00	0.186	0.0273	0.354	1.637	0.411	0.00066	0.37	0.171	0.0273	0.413	1.651	0.458	0	0	1.1
4:45:00	0.186	0.0273	0.354	1.637	0.411	0.00066	0.37	0.171	0.0273	0.413	1.651	0.458	0	0	1.1
4:50:00	0.186	0.0273	0.354	1.637	0.411	0.00066	0.37	0.171	0.0273	0.413	1.651	0.458	0	0	1.1
4:55:00	0.186	0.0273	0.354	1.637	0.411	0.00066	0.37	0.171	0.0273	0.413	1.651	0.458	0	0	1.1
5:00:00	0.186	0.0273	0.354	1.637	0.411	0.00066	0.37	0.171	0.0273	0.413	1.651	0.458	0	0	1.1
5:05:00	0.196	0.03026	0.355	1.648	0.425	0.00066	0.39	0.181	0.0308	0.418	1.662	0.479	0	0	1.2
5:10:00	0.212	0.03505	0.352	1.665	0.442	0.00065	0.42	0.198	0.03538	0.408	1.679	0.49	0	0	1.3
5:15:00	0.219	0.03694	0.35	1.672	0.447	0.00064	0.44	0.204	0.03703	0.401	1.685	0.492	0	0	1.4
5:20:00	0.22	0.03742	0.349	1.674	0.449	0.00064	0.44	0.206	0.03744	0.4	1.687	0.492	0	0	1.4
5:25:00	0.221	0.03752	0.349	1.674	0.449	0.00064	0.44	0.206	0.03752	0.399	1.687	0.492	0	0	1.4
5:30:00	0.221	0.03753	0.349	1.674	0.449	0.00064	0.44	0.206	0.03753	0.399	1.687	0.492	0	0	1.4
5:35:00	0.221	0.03754	0.349	1.674	0.449	0.00064	0.44	0.206	0.03754	0.399	1.687	0.492	0	0	1.4
5:40:00	0.221	0.03754	0.349	1.674	0.449	0.00064	0.44	0.206	0.03754	0.399	1.687	0.492	0	0	1.4
5:45:00	0.221	0.03754	0.349	1.674	0.449	0.00064	0.44	0.206	0.03754	0.399	1.687	0.492	0	0	1.4
5:50:00	0.221	0.03754	0.349	1.674	0.449	0.00064	0.44	0.206	0.03754	0.399	1.687	0.492	0	0	1.4
5:55:00	0.221	0.03754	0.349	1.674	0.449	0.00064	0.44	0.206	0.03754	0.399	1.687	0.492	0	0	1.4
6:00:00	0.221	0.03754	0.349	1.674	0.449	0.00064	0.44	0.206	0.03754	0.399	1.687	0.492	0	0	1.4
6:05:00	0.239	0.04349	0.349	1.693	0.47	0.00064	0.48	0.224	0.04444	0.402	1.707	0.521	0	0	1.6
6:10:00	0.264	0.05178	0.343	1.719	0.493	0.00063	0.53	0.249	0.05226	0.387	1.733	0.535	0	0	1.8

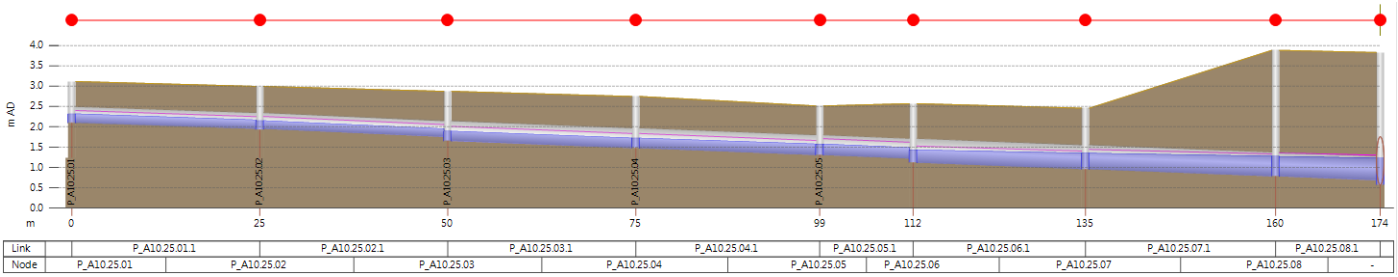
6:15:00	0.273	0.05478	0.34	1.729	0.5	0.00063	0.55	0.258	0.05498	0.38	1.742	0.537	0	0	1.9
6:20:00	0.275	0.05552	0.34	1.731	0.502	0.00064	0.55	0.26	0.05552	0.378	1.744	0.538	0	0	1.9
6:25:00	0.275	0.05564	0.34	1.731	0.502	0.00064	0.55	0.26	0.05564	0.378	1.744	0.538	0	0	1.9
6:30:00	0.275	0.05566	0.34	1.731	0.502	0.00064	0.55	0.26	0.05566	0.378	1.744	0.538	0	0	1.9
6:35:00	0.275	0.05566	0.34	1.731	0.502	0.00064	0.55	0.26	0.05566	0.378	1.744	0.538	0	0	1.9
6:40:00	0.275	0.05566	0.34	1.731	0.502	0.00064	0.55	0.26	0.05566	0.378	1.744	0.538	0	0	1.9
6:45:00	0.275	0.05566	0.34	1.731	0.502	0.00064	0.55	0.26	0.05566	0.378	1.744	0.538	0	0	1.9
6:50:00	0.275	0.05566	0.34	1.731	0.502	0.00064	0.55	0.26	0.05566	0.378	1.744	0.538	0	0	1.9
6:55:00	0.275	0.05566	0.34	1.731	0.502	0.00064	0.55	0.26	0.05566	0.378	1.744	0.538	0	0	1.9
7:00:00	0.275	0.05566	0.34	1.731	0.502	0.00064	0.55	0.26	0.05566	0.378	1.744	0.538	0	0	1.9
7:05:00	0.313	0.06948	0.332	1.77	0.538	0.00065	0.63	0.298	0.07118	0.373	1.784	0.583	0	0	2.2
7:10:00	0.355	0.08558	0.319	1.815	0.573	0.00069	0.71	0.342	0.08627	0.348	1.829	0.604	0	0	2.6
7:15:00	0.369	0.09116	0.316	1.829	0.587	0.00072	0.74	0.355	0.09131	0.341	1.843	0.612	0	0	2.7
7:20:00	0.372	0.09257	0.316	1.832	0.592	0.00073	0.74	0.358	0.0926	0.34	1.847	0.615	0	0	2.7
7:25:00	0.372	0.09288	0.316	1.833	0.593	0.00073	0.74	0.359	0.09288	0.34	1.847	0.616	0	0	2.7
7:30:00	0.372	0.09294	0.316	1.833	0.593	0.00073	0.74	0.359	0.09294	0.34	1.847	0.616	0	0	2.7
7:35:00	0.372	0.09295	0.316	1.833	0.593	0.00073	0.74	0.359	0.09295	0.34	1.847	0.616	0	0	2.7
7:40:00	0.372	0.09295	0.316	1.833	0.593	0.00073	0.74	0.359	0.09295	0.34	1.847	0.616	0	0	2.7
7:45:00	0.372	0.09295	0.316	1.833	0.593	0.00073	0.74	0.359	0.09295	0.34	1.847	0.616	0	0	2.7
7:50:00	0.372	0.09295	0.316	1.833	0.593	0.00073	0.74	0.359	0.09295	0.34	1.847	0.616	0	0	2.7
7:55:00	0.372	0.09295	0.316	1.833	0.593	0.00073	0.74	0.359	0.09295	0.34	1.847	0.616	0	0	2.7
8:00:00	0.372	0.09295	0.316	1.833	0.593	0.00073	0.74	0.359	0.09295	0.34	1.847	0.616	0	0	2.7
8:05:00	0.479	0.13478	0.24	1.946	0.696	0.00111	0.96	0.472	0.13693	0.255	1.967	0.713	0	0	3.4
8:10:00	0.586	0.18591	0.064	2.072	0.911	0.00249	2	0.604	0.18596	0.064	2.115	0.911	0	0	3.6
8:15:00	0.619	0.19171	0.066	2.107	0.938	0.0026	2	0.638	0.19172	0.066	2.152	0.937	0	0	3.6
8:20:00	0.625	0.19235	0.066	2.113	0.941	0.00261	2	0.644	0.19236	0.066	2.158	0.94	0	0	3.6
8:25:00	0.626	0.19246	0.066	2.114	0.941	0.00261	2	0.646	0.19246	0.066	2.16	0.94	0	0	3.6
8:30:00	0.626	0.19249	0.066	2.114	0.941	0.00262	2	0.646	0.19249	0.066	2.16	0.941	0	0	3.6
8:35:00	0.626	0.19249	0.066	2.114	0.941	0.00262	2	0.646	0.19249	0.066	2.16	0.941	0	0	3.6
8:40:00	0.626	0.19249	0.066	2.114	0.941	0.00262	2	0.646	0.19249	0.066	2.16	0.941	0	0	3.6
8:45:00	0.626	0.19249	0.066	2.114	0.941	0.00262	2	0.646	0.19249	0.066	2.16	0.941	0	0	3.6
8:50:00	0.626	0.19249	0.066	2.114	0.941	0.00262	2	0.646	0.19249	0.066	2.16	0.941	0	0	3.6
8:55:00	0.626	0.19249	0.066	2.114	0.941	0.00262	2	0.646	0.19249	0.066	2.16	0.941	0	0	3.6
9:00:00	0.626	0.19249	0.066	2.114	0.941	0.00262	2	0.646	0.19249	0.066	2.16	0.941	0	0	3.6
9:05:00	0.54	0.15202	0.14	2.012	0.75	0.00163	2	0.543	0.15169	0.133	2.04	0.748	0	0	3.6
9:10:00	0.489	0.14439	0.24	1.959	0.738	0.00126	0.98	0.485	0.14387	0.246	1.981	0.738	0	0	3.4
9:15:00	0.469	0.13332	0.253	1.937	0.697	0.00107	0.94	0.462	0.13316	0.265	1.956	0.703	0	0	3.3
9:20:00	0.464	0.13019	0.256	1.931	0.685	0.00103	0.93	0.456	0.13014	0.272	1.949	0.693	0	0	3.3
9:25:00	0.462	0.12935	0.257	1.929	0.682	0.00101	0.92	0.454	0.12933	0.274	1.947	0.691	0	0	3.3
9:30:00	0.462	0.12913	0.258	1.928	0.682	0.00101	0.92	0.453	0.12913	0.274	1.947	0.69	0	0	3.3
9:35:00	0.462	0.12907	0.258	1.928	0.681	0.00101	0.92	0.453	0.12907	0.274	1.947	0.69	0	0	3.3
9:40:00	0.462	0.12906	0.258	1.928	0.681	0.00101	0.92	0.453	0.12906	0.274	1.947	0.69	0	0	3.3
9:45:00	0.462	0.12906	0.258	1.928	0.681	0.00101	0.92	0.453	0.12906	0.274	1.947	0.69	0	0	3.3
9:50:00	0.462	0.12906	0.258	1.928	0.681	0.00101	0.92	0.453	0.12906	0.274	1.947	0.69	0	0	3.3
9:55:00	0.462	0.12906	0.258	1.928	0.681	0.00101	0.92	0.453	0.12906	0.274	1.947	0.69	0	0	3.3

10:00	0.462	0.12906	0.258	1.928	0.681	0.00101	0.92	0.453	0.12906	0.274	1.947	0.69	0	0	3.3
10:05	0.404	0.10744	0.308	1.867	0.633	0.00084	0.81	0.392	0.10545	0.321	1.882	0.638	0	0	2.9
10:10	0.343	0.08306	0.331	1.803	0.578	0.00072	0.69	0.33	0.08199	0.353	1.817	0.596	0	0	2.5
10:15	0.322	0.07354	0.332	1.781	0.55	0.00068	0.64	0.308	0.07324	0.361	1.794	0.577	0	0	2.3
10:20	0.317	0.07125	0.332	1.775	0.542	0.00066	0.63	0.303	0.07119	0.362	1.789	0.572	0	0	2.2
10:25	0.316	0.0708	0.331	1.774	0.541	0.00066	0.63	0.302	0.07079	0.362	1.788	0.571	0	0	2.2
10:30	0.316	0.07072	0.331	1.774	0.54	0.00066	0.63	0.302	0.07071	0.362	1.787	0.571	0	0	2.2
10:35	0.316	0.0707	0.331	1.774	0.54	0.00066	0.63	0.302	0.0707	0.362	1.787	0.571	0	0	2.2
10:40	0.316	0.0707	0.331	1.774	0.54	0.00066	0.63	0.302	0.0707	0.362	1.787	0.571	0	0	2.2
10:45	0.316	0.0707	0.331	1.774	0.54	0.00066	0.63	0.302	0.0707	0.362	1.787	0.571	0	0	2.2
10:50	0.316	0.0707	0.331	1.774	0.54	0.00066	0.63	0.302	0.0707	0.362	1.787	0.571	0	0	2.2
10:55	0.316	0.0707	0.331	1.774	0.54	0.00066	0.63	0.302	0.0707	0.362	1.787	0.571	0	0	2.2
11:00	0.316	0.0707	0.331	1.774	0.54	0.00066	0.63	0.302	0.0707	0.362	1.787	0.571	0	0	2.2
11:05	0.292	0.06175	0.337	1.749	0.519	0.00065	0.58	0.277	0.06064	0.365	1.761	0.542	0	0	2
11:10	0.261	0.05061	0.343	1.716	0.489	0.00064	0.52	0.246	0.04998	0.379	1.729	0.52	0	0	1.7
11:15	0.249	0.04648	0.345	1.703	0.477	0.00063	0.5	0.234	0.0463	0.387	1.716	0.514	0	0	1.6
11:20	0.246	0.04548	0.346	1.7	0.474	0.00063	0.49	0.231	0.04544	0.389	1.713	0.513	0	0	1.6
11:25	0.245	0.04528	0.346	1.699	0.473	0.00063	0.49	0.23	0.04528	0.39	1.712	0.513	0	0	1.6
11:30	0.245	0.04525	0.346	1.699	0.473	0.00063	0.49	0.23	0.04525	0.39	1.712	0.513	0	0	1.6
11:35	0.245	0.04525	0.346	1.699	0.473	0.00063	0.49	0.23	0.04525	0.39	1.712	0.513	0	0	1.6
11:40	0.245	0.04524	0.346	1.699	0.473	0.00063	0.49	0.23	0.04524	0.39	1.712	0.513	0	0	1.6
11:45	0.245	0.04524	0.346	1.699	0.473	0.00063	0.49	0.23	0.04524	0.39	1.712	0.513	0	0	1.6
11:50	0.245	0.04524	0.346	1.699	0.473	0.00063	0.49	0.23	0.04524	0.39	1.712	0.513	0	0	1.6
11:55	0.245	0.04524	0.346	1.699	0.473	0.00063	0.49	0.23	0.04524	0.39	1.712	0.513	0	0	1.6
12:00	0.245	0.04524	0.346	1.699	0.473	0.00063	0.49	0.23	0.04524	0.39	1.712	0.513	0	0	1.6
12:05	0.232	0.04094	0.346	1.686	0.459	0.00063	0.46	0.217	0.04034	0.387	1.699	0.493	0	0	1.5
12:10	0.213	0.03502	0.35	1.666	0.439	0.00064	0.43	0.198	0.03461	0.397	1.679	0.478	0	0	1.3
12:15	0.204	0.03259	0.352	1.657	0.431	0.00065	0.41	0.19	0.03247	0.404	1.67	0.475	0	0	1.3
12:20	0.202	0.03196	0.352	1.655	0.429	0.00065	0.4	0.188	0.03193	0.406	1.668	0.474	0	0	1.2
12:25	0.202	0.03182	0.352	1.654	0.429	0.00065	0.4	0.187	0.03182	0.407	1.668	0.474	0	0	1.2
12:30	0.202	0.0318	0.352	1.654	0.429	0.00065	0.4	0.187	0.0318	0.407	1.668	0.474	0	0	1.2
12:35	0.202	0.0318	0.352	1.654	0.429	0.00065	0.4	0.187	0.0318	0.407	1.668	0.474	0	0	1.2
12:40	0.202	0.0318	0.352	1.654	0.429	0.00065	0.4	0.187	0.0318	0.407	1.668	0.474	0	0	1.2
12:45	0.202	0.0318	0.352	1.654	0.429	0.00065	0.4	0.187	0.0318	0.407	1.668	0.474	0	0	1.2
12:50	0.202	0.0318	0.352	1.654	0.429	0.00065	0.4	0.187	0.0318	0.407	1.668	0.474	0	0	1.2
12:55	0.202	0.0318	0.352	1.654	0.429	0.00065	0.4	0.187	0.0318	0.407	1.668	0.474	0	0	1.2
13:00	0.202	0.0318	0.352	1.654	0.429	0.00065	0.4	0.187	0.0318	0.407	1.668	0.474	0	0	1.2
13:05	0.194	0.0295	0.352	1.646	0.419	0.00065	0.39	0.179	0.02911	0.403	1.659	0.459	0	0	1.2
13:10	0.181	0.02589	0.353	1.632	0.404	0.00066	0.36	0.167	0.02562	0.409	1.646	0.447	0	0	1.1
13:15	0.175	0.02432	0.354	1.626	0.397	0.00067	0.35	0.161	0.02423	0.416	1.64	0.445	0	0	1
13:20	0.173	0.02389	0.355	1.624	0.396	0.00068	0.35	0.159	0.02387	0.418	1.638	0.445	0	0	1
13:25	0.173	0.0238	0.355	1.624	0.396	0.00068	0.35	0.159	0.0238	0.419	1.638	0.445	0	0	1
13:30	0.173	0.02378	0.355	1.624	0.395	0.00068	0.35	0.159	0.02378	0.419	1.638	0.445	0	0	1
13:35	0.173	0.02378	0.355	1.624	0.395	0.00068	0.35	0.159	0.02378	0.419	1.638	0.445	0	0	1
13:40	0.173	0.02378	0.355	1.624	0.395	0.00068	0.35	0.159	0.02378	0.419	1.638	0.445	0	0	1

13:45:00	0.173	0.02378	0.355	1.624	0.395	0.00068	0.35	0.159	0.02378	0.419	1.638	0.445	0	0	1
13:50:00	0.173	0.02378	0.355	1.624	0.395	0.00068	0.35	0.159	0.02378	0.419	1.638	0.445	0	0	1
13:55:00	0.173	0.02378	0.355	1.624	0.395	0.00068	0.35	0.159	0.02378	0.419	1.638	0.445	0	0	1
14:00:00	0.173	0.02378	0.355	1.624	0.395	0.00068	0.35	0.159	0.02378	0.419	1.638	0.445	0	0	1
14:00:00	0.168	0.02243	0.354	1.618	0.388	0.00068	0.34	0.154	0.02217	0.415	1.632	0.433	0	0	1
14:10:00	0.158	0.02006	0.354	1.609	0.376	0.00069	0.32	0.145	0.01986	0.419	1.623	0.422	0	0	0.9
14:15:00	0.154	0.01898	0.355	1.604	0.37	0.0007	0.31	0.14	0.01891	0.424	1.618	0.42	0	0	0.8
14:20:00	0.152	0.01867	0.356	1.602	0.369	0.00071	0.3	0.139	0.01866	0.426	1.617	0.42	0	0	0.8
14:25:00	0.152	0.01861	0.356	1.602	0.369	0.00071	0.3	0.138	0.01867	0.427	1.616	0.42	0	0	0.8
14:30:00	0.152	0.01869	0.356	1.602	0.369	0.00071	0.3	0.138	0.01859	0.427	1.616	0.42	0	0	0.8
14:35:00	0.152	0.01859	0.356	1.602	0.369	0.00071	0.3	0.138	0.01859	0.427	1.616	0.42	0	0	0.8
14:40:00	0.152	0.01859	0.356	1.602	0.369	0.00071	0.3	0.138	0.01859	0.427	1.616	0.42	0	0	0.8
14:45:00	0.152	0.01859	0.356	1.602	0.369	0.00071	0.3	0.138	0.01859	0.427	1.616	0.42	0	0	0.8
14:50:00	0.152	0.01859	0.356	1.602	0.369	0.00071	0.3	0.138	0.01859	0.427	1.616	0.42	0	0	0.8
14:55:00	0.152	0.01859	0.356	1.602	0.369	0.00071	0.3	0.138	0.01859	0.427	1.616	0.42	0	0	0.8
15:00:00	0.149	0.01774	0.355	1.598	0.363	0.00071	0.3	0.135	0.01756	0.423	1.613	0.411	0	0	0.8
15:10:00	0.141	0.01615	0.354	1.591	0.352	0.00072	0.28	0.128	0.01595	0.425	1.605	0.401	0	0	0.7
15:15:00	0.138	0.01531	0.354	1.587	0.348	0.00073	0.28	0.125	0.01526	0.429	1.602	0.399	0	0	0.7
15:20:00	0.137	0.01509	0.355	1.586	0.347	0.00074	0.27	0.123	0.01508	0.431	1.601	0.399	0	0	0.7
15:25:00	0.136	0.01504	0.355	1.585	0.347	0.00074	0.27	0.123	0.01504	0.432	1.6	0.4	0	0	0.7
15:30:00	0.136	0.01503	0.355	1.585	0.347	0.00074	0.27	0.123	0.01503	0.432	1.6	0.4	0	0	0.7
15:35:00	0.136	0.01503	0.355	1.585	0.347	0.00074	0.27	0.123	0.01503	0.432	1.6	0.4	0	0	0.7
15:40:00	0.136	0.01503	0.355	1.585	0.347	0.00074	0.27	0.123	0.01503	0.432	1.6	0.4	0	0	0.7
15:45:00	0.136	0.01503	0.355	1.585	0.347	0.00074	0.27	0.123	0.01503	0.432	1.6	0.4	0	0	0.7
15:50:00	0.136	0.01503	0.355	1.585	0.347	0.00074	0.27	0.123	0.01503	0.432	1.6	0.4	0	0	0.7
15:55:00	0.136	0.01503	0.355	1.585	0.347	0.00074	0.27	0.123	0.01503	0.432	1.6	0.4	0	0	0.7
16:00:00	0.136	0.01503	0.355	1.585	0.347	0.00074	0.27	0.123	0.01503	0.432	1.6	0.4	0	0	0.7
16:00:00	0.134	0.01446	0.354	1.583	0.342	0.00074	0.27	0.121	0.01433	0.428	1.598	0.392	0	0	0.7
16:10:00	0.128	0.01327	0.352	1.577	0.333	0.00075	0.26	0.115	0.01316	0.429	1.592	0.383	0	0	0.6
16:15:00	0.125	0.01268	0.353	1.574	0.329	0.00076	0.25	0.113	0.01264	0.432	1.589	0.381	0	0	0.6
16:20:00	0.124	0.01251	0.353	1.573	0.328	0.00077	0.25	0.112	0.01251	0.434	1.588	0.381	0	0	0.6
16:25:00	0.124	0.01247	0.354	1.573	0.328	0.00077	0.25	0.112	0.01247	0.435	1.588	0.382	0	0	0.6
16:30:00	0.124	0.01246	0.354	1.573	0.328	0.00077	0.25	0.112	0.01246	0.435	1.588	0.382	0	0	0.6
16:35:00	0.124	0.01246	0.354	1.573	0.328	0.00077	0.25	0.112	0.01246	0.435	1.588	0.382	0	0	0.6
16:40:00	0.124	0.01246	0.354	1.573	0.328	0.00077	0.25	0.112	0.01246	0.435	1.588	0.382	0	0	0.6
16:45:00	0.124	0.01246	0.354	1.573	0.328	0.00077	0.25	0.112	0.01246	0.435	1.588	0.382	0	0	0.6
16:50:00	0.124	0.01246	0.354	1.573	0.328	0.00077	0.25	0.112	0.01246	0.435	1.588	0.382	0	0	0.6
16:55:00	0.124	0.01246	0.354	1.573	0.328	0.00077	0.25	0.112	0.01246	0.435	1.588	0.382	0	0	0.6
17:00:00	0.124	0.01246	0.354	1.573	0.328	0.00077	0.25	0.112	0.01246	0.435	1.588	0.382	0	0	0.6
17:00:00	0.122	0.01206	0.352	1.571	0.324	0.00077	0.24	0.11	0.01197	0.432	1.586	0.375	0	0	0.6
17:10:00	0.118	0.01118	0.35	1.566	0.316	0.00078	0.24	0.106	0.01109	0.432	1.581	0.368	0	0	0.6
17:15:00	0.115	0.01072	0.35	1.563	0.313	0.00079	0.23	0.103	0.01069	0.434	1.579	0.366	0	0	0.6
17:20:00	0.115	0.01059	0.351	1.562	0.312	0.00079	0.23	0.102	0.01058	0.436	1.578	0.366	0	0	0.5
17:25:00	0.114	0.01056	0.351	1.562	0.312	0.0008	0.23	0.102	0.01055	0.436	1.578	0.366	0	0	0.5

17:30:00	0.114	0.01055	0.351	1.562	0.312	0.0008	0.23	0.102	0.01055	0.437	1.578	0.366	0	0	0.5
17:35:00	0.114	0.01055	0.351	1.562	0.312	0.0008	0.23	0.102	0.01055	0.437	1.578	0.366	0	0	0.5
17:40:00	0.114	0.01055	0.351	1.562	0.312	0.0008	0.23	0.102	0.01055	0.437	1.578	0.366	0	0	0.5
17:45:00	0.114	0.01055	0.351	1.562	0.312	0.0008	0.23	0.102	0.01055	0.437	1.578	0.366	0	0	0.5
17:50:00	0.114	0.01055	0.351	1.562	0.312	0.0008	0.23	0.102	0.01055	0.437	1.578	0.366	0	0	0.5
17:55:00	0.114	0.01055	0.351	1.562	0.312	0.0008	0.23	0.102	0.01055	0.437	1.578	0.366	0	0	0.5
18:00:00	0.114	0.01055	0.351	1.562	0.312	0.0008	0.23	0.102	0.01055	0.437	1.578	0.366	0	0	0.5
18:05:00	0.105	0.00864	0.34	1.552	0.289	0.00077	0.21	0.092	0.00815	0.411	1.567	0.326	0	0	0.5
18:10:00	0.079	0.00443	0.306	1.524	0.223	0.0008	0.16	0.067	0.00389	0.371	1.539	0.249	0	0	0.3
18:15:00	0.057	0.00186	0.241	1.501	0.149	0.00086	0.11	0.046	0.00155	0.306	1.517	0.17	0	0	0.2
18:20:00	0.044	0.00072	0.152	1.487	0.082	0.0009	0.09	0.034	0.00054	0.203	1.503	0.095	0	0	0.1
18:25:00	0.037	0.00022	0.066	1.48	0.033	0.00095	0.07	0.028	0.00016	0.091	1.497	0.037	0	0	0.1
18:30:00	0.035	0.00007	0.024	1.478	0.012	0.001	0.07	0.026	0.00005	0.033	1.495	0.013	0	0	0.1
18:35:00	0.034	0.00003	0.01	1.477	0.005	0.00103	0.07	0.026	0.00002	0.015	1.495	0.006	0	0	0.1
18:40:00	0.033	0.00002	0.007	1.476	0.003	0.00104	0.07	0.026	0.00002	0.011	1.495	0.004	0	0	0.1
18:45:00	0.033	0.00002	0.006	1.476	0.003	0.00104	0.07	0.026	0.00002	0.011	1.495	0.004	0	0	0.1
18:50:00	0.033	0.00002	0.006	1.476	0.003	0.00104	0.07	0.026	0.00002	0.011	1.495	0.004	0	0	0.1
18:55:00	0.033	0.00002	0.006	1.476	0.003	0.00104	0.07	0.026	0.00002	0.011	1.495	0.004	0	0	0.1
19:00:00	0.033	0.00002	0.006	1.476	0.003	0.00104	0.07	0.026	0.00002	0.011	1.495	0.004	0	0	0.1
19:00:00	0.033	0.00001	0.005	1.476	0.002	0.00104	0.07	0.026	0.00001	0.01	1.495	0.004	0	0	0.1
19:10:00	0.033	0.00001	0.004	1.476	0.002	0.00104	0.07	0.025	0.00001	0.007	1.494	0.003	0	0	0.1
19:15:00	0.033	0.00001	0.002	1.476	0.001	0.00104	0.07	0.025	0	0.003	1.494	0.001	0	0	0.1
19:20:00	0.033	0	0.001	1.476	0	0.00104	0.07	0.025	0	0.001	1.494	0	0	0	0.1
19:25:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
19:30:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
19:35:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
19:40:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
19:45:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
19:50:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
19:55:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:00:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:05:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:10:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:15:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:20:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:25:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:30:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:35:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:40:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:45:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:50:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
20:55:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:00:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:05:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:10:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1

21:15:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:20:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:25:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:30:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:35:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:40:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:45:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:50:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
21:55:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:00:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:05:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:10:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:15:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:20:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:25:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:30:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:35:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:40:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:45:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:50:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
22:55:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:00:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:05:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:10:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:15:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:20:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:25:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:30:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:35:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:40:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:45:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:50:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
23:55:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1
0:00:00	0.033	0	0	1.476	0	0.00104	0.07	0.025	0	0	1.494	0	0	0	0.1



	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.06	0	0	0.627	0	0.0016	0.05	0.06	0	0	0.667	0	0	0	0.5
0:05:00	0.06	0	0	0.627	0	0.0016	0.05	0.06	0	0	0.667	0	0	0	0.5
0:10:00	0.06	0	0	0.627	0	0.0016	0.05	0.06	0	0	0.667	0	0	0	0.5
0:15:00	0.06	0	0	0.627	0	0.0016	0.05	0.06	0	0	0.667	0	0	0	0.5
0:20:00	0.074	-0.00011	0.006	0.641	-0.004	0.00115	0.06	0.063	0.00084	0.063	0.67	0.038	0	0	0.6
0:25:00	0.114	0.00858	0.18	0.682	0.157	0.00079	0.1	0.094	0.01066	0.329	0.704	0.26	0	0	1.2
0:30:00	0.143	0.02596	0.346	0.716	0.34	0.001	0.12	0.128	0.02777	0.461	0.745	0.427	0	0	1.7
0:35:00	0.162	0.03943	0.416	0.738	0.434	0.00109	0.13	0.149	0.04023	0.5	0.768	0.499	0	0	2.1
0:40:00	0.168	0.04424	0.433	0.746	0.461	0.0011	0.14	0.155	0.04446	0.506	0.776	0.518	0	0	2.3
0:45:00	0.169	0.04543	0.436	0.747	0.467	0.00111	0.14	0.157	0.04548	0.507	0.778	0.521	0	0	2.3
0:50:00	0.17	0.04568	0.437	0.748	0.468	0.00111	0.14	0.157	0.04569	0.508	0.778	0.522	0	0	2.3
0:55:00	0.17	0.04573	0.437	0.748	0.468	0.00111	0.14	0.157	0.04573	0.508	0.778	0.522	0	0	2.3
1:00:00	0.17	0.04573	0.437	0.748	0.468	0.00111	0.14	0.157	0.04573	0.508	0.778	0.522	0	0	2.3
1:05:00	0.172	0.04641	0.432	0.75	0.465	0.00108	0.14	0.159	0.04671	0.508	0.78	0.525	0	0	2.3
1:10:00	0.177	0.04955	0.435	0.756	0.476	0.00107	0.15	0.164	0.04987	0.511	0.786	0.537	0	0	2.4
1:15:00	0.181	0.05246	0.443	0.76	0.49	0.00108	0.15	0.168	0.05265	0.515	0.79	0.548	0	0	2.5
1:20:00	0.183	0.05395	0.447	0.762	0.497	0.00108	0.15	0.17	0.05402	0.517	0.792	0.553	0	0	2.6
1:25:00	0.183	0.05446	0.448	0.763	0.499	0.00109	0.15	0.17	0.05448	0.518	0.793	0.555	0	0	2.6
1:30:00	0.183	0.05459	0.449	0.763	0.5	0.00109	0.15	0.17	0.05459	0.518	0.793	0.555	0	0	2.6
1:35:00	0.183	0.05461	0.449	0.763	0.5	0.00109	0.15	0.171	0.05462	0.518	0.793	0.555	0	0	2.6
1:40:00	0.183	0.05462	0.449	0.763	0.5	0.00109	0.15	0.171	0.05462	0.518	0.793	0.555	0	0	2.6
1:45:00	0.183	0.05462	0.449	0.763	0.5	0.00109	0.15	0.171	0.05462	0.518	0.793	0.555	0	0	2.6
1:50:00	0.183	0.05462	0.449	0.763	0.5	0.00109	0.15	0.171	0.05462	0.518	0.793	0.555	0	0	2.6
1:55:00	0.183	0.05462	0.449	0.763	0.5	0.00109	0.15	0.171	0.05462	0.518	0.793	0.555	0	0	2.6
2:00:00	0.183	0.05462	0.449	0.763	0.5	0.00109	0.15	0.171	0.05462	0.518	0.793	0.555	0	0	2.6
2:05:00	0.187	0.05565	0.442	0.766	0.497	0.00105	0.16	0.173	0.05608	0.518	0.796	0.559	0	0	2.6
2:10:00	0.193	0.06016	0.446	0.773	0.511	0.00104	0.16	0.179	0.06059	0.521	0.803	0.573	0	0	2.8
2:15:00	0.197	0.06407	0.455	0.779	0.527	0.00106	0.16	0.184	0.0643	0.525	0.808	0.586	0	0	2.9
2:20:00	0.199	0.0659	0.459	0.781	0.534	0.00106	0.17	0.186	0.06599	0.527	0.811	0.592	0	0	2.9

2:25:00	0.2	0.06649	0.46	0.782	0.537	0.00107	0.17	0.187	0.06651	0.527	0.812	0.593	0	0	2.9
2:30:00	0.2	0.06663	0.461	0.782	0.537	0.00107	0.17	0.187	0.06663	0.528	0.812	0.593	0	0	2.9
2:35:00	0.2	0.06666	0.461	0.782	0.537	0.00107	0.17	0.187	0.06666	0.528	0.812	0.594	0	0	2.9
2:40:00	0.2	0.06666	0.461	0.782	0.537	0.00107	0.17	0.187	0.06666	0.528	0.812	0.594	0	0	2.9
2:45:00	0.2	0.06666	0.461	0.782	0.537	0.00107	0.17	0.187	0.06666	0.528	0.812	0.594	0	0	2.9
2:50:00	0.2	0.06666	0.461	0.782	0.537	0.00107	0.17	0.187	0.06666	0.528	0.812	0.594	0	0	2.9
2:55:00	0.2	0.06666	0.461	0.782	0.537	0.00107	0.17	0.187	0.06666	0.528	0.812	0.594	0	0	2.9
3:00:00	0.2	0.06666	0.461	0.782	0.537	0.00107	0.17	0.187	0.06666	0.528	0.812	0.594	0	0	2.9
3:05:00	0.205	0.06837	0.453	0.786	0.534	0.00103	0.17	0.19	0.06898	0.527	0.816	0.598	0	0	3
3:10:00	0.213	0.07515	0.458	0.796	0.552	0.00102	0.18	0.199	0.07573	0.53	0.825	0.616	0	0	3.2
3:15:00	0.219	0.08058	0.468	0.802	0.571	0.00104	0.18	0.205	0.08087	0.535	0.832	0.631	0	0	3.3
3:20:00	0.221	0.0829	0.472	0.805	0.579	0.00105	0.18	0.207	0.08299	0.536	0.835	0.637	0	0	3.4
3:25:00	0.222	0.08357	0.473	0.806	0.582	0.00105	0.18	0.208	0.0836	0.537	0.836	0.638	0	0	3.4
3:30:00	0.222	0.08372	0.473	0.806	0.582	0.00105	0.18	0.208	0.08373	0.537	0.836	0.639	0	0	3.4
3:35:00	0.222	0.08375	0.473	0.806	0.582	0.00105	0.18	0.208	0.08375	0.537	0.836	0.639	0	0	3.4
3:40:00	0.222	0.08376	0.473	0.806	0.582	0.00105	0.18	0.208	0.08376	0.537	0.836	0.639	0	0	3.4
3:45:00	0.222	0.08376	0.473	0.806	0.582	0.00105	0.18	0.208	0.08376	0.537	0.836	0.639	0	0	3.4
3:50:00	0.222	0.08376	0.473	0.806	0.582	0.00105	0.18	0.208	0.08376	0.537	0.836	0.639	0	0	3.4
3:55:00	0.222	0.08376	0.473	0.806	0.582	0.00105	0.18	0.208	0.08376	0.537	0.836	0.639	0	0	3.4
4:00:00	0.222	0.08376	0.473	0.806	0.582	0.00105	0.18	0.208	0.08376	0.537	0.836	0.639	0	0	3.4
4:05:00	0.228	0.08679	0.463	0.812	0.579	0.001	0.19	0.213	0.08773	0.535	0.842	0.645	0	0	3.6
4:10:00	0.24	0.09762	0.471	0.826	0.605	0.001	0.2	0.225	0.0984	0.539	0.855	0.669	0	0	3.8
4:15:00	0.247	0.10537	0.482	0.834	0.627	0.00102	0.21	0.233	0.10574	0.544	0.864	0.686	0	0	4
4:20:00	0.25	0.10834	0.485	0.837	0.636	0.00103	0.21	0.235	0.10846	0.545	0.867	0.692	0	0	4.1
4:25:00	0.25	0.10913	0.486	0.838	0.638	0.00103	0.21	0.236	0.10916	0.545	0.868	0.694	0	0	4.1
4:30:00	0.251	0.10929	0.486	0.838	0.638	0.00103	0.21	0.236	0.1093	0.545	0.868	0.694	0	0	4.1
4:35:00	0.251	0.10932	0.486	0.838	0.638	0.00103	0.21	0.236	0.10932	0.545	0.868	0.694	0	0	4.1
4:40:00	0.251	0.10933	0.486	0.838	0.638	0.00103	0.21	0.236	0.10933	0.545	0.868	0.694	0	0	4.1
4:45:00	0.251	0.10933	0.486	0.838	0.638	0.00103	0.21	0.236	0.10933	0.545	0.868	0.694	0	0	4.1
4:50:00	0.251	0.10933	0.486	0.838	0.638	0.00103	0.21	0.236	0.10933	0.545	0.868	0.694	0	0	4.1
4:55:00	0.251	0.10933	0.486	0.838	0.638	0.00103	0.21	0.236	0.10933	0.545	0.868	0.694	0	0	4.1
5:00:00	0.251	0.10933	0.486	0.838	0.638	0.00103	0.21	0.236	0.10933	0.545	0.868	0.694	0	0	4.1
5:05:00	0.261	0.11528	0.474	0.848	0.635	0.00097	0.22	0.245	0.11679	0.543	0.877	0.704	0	0	4.3
5:10:00	0.278	0.13373	0.485	0.868	0.673	0.00098	0.23	0.263	0.1349	0.547	0.897	0.736	0	0	4.8
5:15:00	0.287	0.14535	0.496	0.879	0.7	0.00101	0.24	0.272	0.14581	0.552	0.908	0.757	0	0	5
5:20:00	0.29	0.14922	0.5	0.882	0.708	0.00102	0.24	0.275	0.14934	0.553	0.912	0.763	0	0	5.1
5:25:00	0.291	0.15013	0.5	0.883	0.71	0.00102	0.24	0.276	0.15016	0.553	0.913	0.764	0	0	5.1
5:30:00	0.291	0.15031	0.5	0.883	0.711	0.00102	0.24	0.276	0.15031	0.553	0.913	0.764	0	0	5.1
5:35:00	0.291	0.15034	0.5	0.883	0.711	0.00102	0.24	0.276	0.15034	0.553	0.913	0.764	0	0	5.1
5:40:00	0.291	0.15034	0.5	0.883	0.711	0.00102	0.24	0.276	0.15034	0.553	0.913	0.764	0	0	5.1
5:45:00	0.291	0.15034	0.5	0.883	0.711	0.00102	0.24	0.276	0.15034	0.553	0.913	0.764	0	0	5.1
5:50:00	0.291	0.15034	0.5	0.883	0.711	0.00102	0.24	0.276	0.15034	0.553	0.913	0.764	0	0	5.1
5:55:00	0.291	0.15034	0.5	0.883	0.711	0.00102	0.24	0.276	0.15034	0.553	0.913	0.764	0	0	5.1
6:00:00	0.291	0.15034	0.5	0.883	0.711	0.00102	0.24	0.276	0.15034	0.553	0.913	0.764	0	0	5.1
6:05:00	0.309	0.16375	0.485	0.901	0.712	0.00094	0.26	0.292	0.16642	0.549	0.93	0.782	0	0	5.5

6:10:00	0.335	0.19838	0.501	0.932	0.768	0.00098	0.28	0.32	0.20015	0.554	0.962	0.828	0	0	6.2
6:15:00	0.347	0.21677	0.512	0.946	0.8	0.00101	0.29	0.332	0.21716	0.558	0.976	0.852	0	0	6.6
6:20:00	0.35	0.22166	0.515	0.95	0.808	0.00102	0.29	0.335	0.2218	0.559	0.98	0.858	0	0	6.6
6:25:00	0.351	0.22272	0.515	0.951	0.81	0.00102	0.29	0.336	0.22274	0.559	0.981	0.859	0	0	6.7
6:30:00	0.351	0.2229	0.515	0.951	0.81	0.00102	0.29	0.336	0.2229	0.559	0.981	0.859	0	0	6.7
6:35:00	0.351	0.22293	0.515	0.951	0.81	0.00102	0.29	0.336	0.22293	0.559	0.981	0.859	0	0	6.7
6:40:00	0.351	0.22293	0.515	0.951	0.81	0.00102	0.29	0.336	0.22293	0.559	0.981	0.859	0	0	6.7
6:45:00	0.351	0.22293	0.515	0.951	0.81	0.00102	0.29	0.336	0.22293	0.559	0.981	0.859	0	0	6.7
6:50:00	0.351	0.22293	0.515	0.951	0.81	0.00102	0.29	0.336	0.22293	0.559	0.981	0.859	0	0	6.7
6:55:00	0.351	0.22293	0.515	0.951	0.81	0.00102	0.29	0.336	0.22293	0.559	0.981	0.859	0	0	6.7
7:00:00	0.351	0.22293	0.515	0.951	0.81	0.00102	0.29	0.336	0.22293	0.559	0.981	0.859	0	0	6.7
7:05:00	0.387	0.25956	0.496	0.988	0.824	0.00093	0.32	0.37	0.265	0.553	1.018	0.895	0	0	7.6
7:10:00	0.431	0.33372	0.518	1.04	0.914	0.00101	0.36	0.416	0.33651	0.559	1.071	0.966	0	0	8.9
7:15:00	0.446	0.36358	0.527	1.059	0.949	0.00105	0.37	0.433	0.36431	0.561	1.09	0.992	0	0	9.4
7:20:00	0.45	0.37058	0.529	1.064	0.957	0.00106	0.37	0.436	0.37073	0.562	1.094	0.998	0	0	9.5
7:25:00	0.451	0.37196	0.53	1.064	0.958	0.00106	0.38	0.437	0.37199	0.562	1.095	0.999	0	0	9.5
7:30:00	0.451	0.37221	0.53	1.065	0.959	0.00106	0.38	0.437	0.37222	0.562	1.095	0.999	0	0	9.5
7:35:00	0.451	0.37226	0.53	1.065	0.959	0.00106	0.38	0.437	0.37226	0.562	1.095	0.999	0	0	9.5
7:40:00	0.451	0.37227	0.53	1.065	0.959	0.00106	0.38	0.437	0.37227	0.562	1.095	0.999	0	0	9.5
7:45:00	0.451	0.37227	0.53	1.065	0.959	0.00106	0.38	0.437	0.37227	0.562	1.095	0.999	0	0	9.5
7:50:00	0.451	0.37227	0.53	1.065	0.959	0.00106	0.38	0.437	0.37227	0.562	1.095	0.999	0	0	9.5
7:55:00	0.451	0.37227	0.53	1.065	0.959	0.00106	0.38	0.437	0.37227	0.562	1.095	0.999	0	0	9.5
8:00:00	0.451	0.37227	0.53	1.065	0.959	0.00106	0.38	0.437	0.37227	0.562	1.095	0.999	0	0	9.5
8:05:00	0.545	0.51126	0.506	1.165	1.024	0.00097	0.45	0.529	0.52463	0.549	1.197	1.091	0	0	12.2
8:10:00	0.627	0.69508	0.526	1.263	1.163	0.00114	0.52	0.615	0.69986	0.548	1.296	1.198	0	0	14.8
8:15:00	0.652	0.758	0.532	1.293	1.207	0.0012	0.54	0.642	0.75902	0.549	1.326	1.233	0	0	15.5
8:20:00	0.656	0.7686	0.533	1.299	1.214	0.0012	0.55	0.646	0.76878	0.548	1.332	1.238	0	0	15.7
8:25:00	0.657	0.7705	0.533	1.299	1.215	0.00121	0.55	0.647	0.77053	0.548	1.332	1.238	0	0	15.7
8:30:00	0.657	0.77086	0.533	1.3	1.216	0.00121	0.55	0.647	0.77086	0.548	1.333	1.239	0	0	15.7
8:35:00	0.657	0.77093	0.533	1.3	1.216	0.00121	0.55	0.647	0.77093	0.548	1.333	1.239	0	0	15.7
8:40:00	0.657	0.77094	0.533	1.3	1.216	0.00121	0.55	0.647	0.77094	0.548	1.333	1.239	0	0	15.7
8:45:00	0.657	0.77094	0.533	1.3	1.216	0.00121	0.55	0.647	0.77094	0.548	1.333	1.239	0	0	15.7
8:50:00	0.657	0.77094	0.533	1.3	1.216	0.00121	0.55	0.647	0.77094	0.548	1.333	1.239	0	0	15.7
8:55:00	0.657	0.77094	0.533	1.3	1.216	0.00121	0.55	0.647	0.77094	0.548	1.333	1.239	0	0	15.7
9:00:00	0.657	0.77094	0.533	1.3	1.216	0.00121	0.55	0.647	0.77094	0.548	1.333	1.239	0	0	15.7
9:05:00	0.599	0.66315	0.548	1.236	1.176	0.00123	0.5	0.59	0.65567	0.558	1.268	1.186	0	0	14
9:10:00	0.552	0.56346	0.543	1.182	1.109	0.00117	0.46	0.541	0.56093	0.562	1.214	1.133	0	0	12.5
9:15:00	0.538	0.53119	0.538	1.165	1.081	0.00113	0.45	0.526	0.53036	0.56	1.196	1.111	0	0	12.1
9:20:00	0.534	0.52063	0.536	1.159	1.071	0.00112	0.44	0.522	0.5204	0.56	1.191	1.104	0	0	12
9:25:00	0.532	0.51783	0.535	1.158	1.069	0.00111	0.44	0.52	0.51777	0.56	1.189	1.102	0	0	11.9
9:30:00	0.532	0.51712	0.535	1.157	1.068	0.00111	0.44	0.52	0.51711	0.559	1.189	1.101	0	0	11.9
9:35:00	0.532	0.51694	0.535	1.157	1.068	0.00111	0.44	0.52	0.51694	0.559	1.189	1.101	0	0	11.9
9:40:00	0.532	0.5169	0.535	1.157	1.068	0.00111	0.44	0.52	0.5169	0.559	1.189	1.101	0	0	11.9
9:45:00	0.532	0.51689	0.535	1.157	1.068	0.00111	0.44	0.52	0.51689	0.559	1.189	1.101	0	0	11.9
9:50:00	0.532	0.51688	0.535	1.157	1.068	0.00111	0.44	0.52	0.51688	0.559	1.189	1.101	0	0	11.9

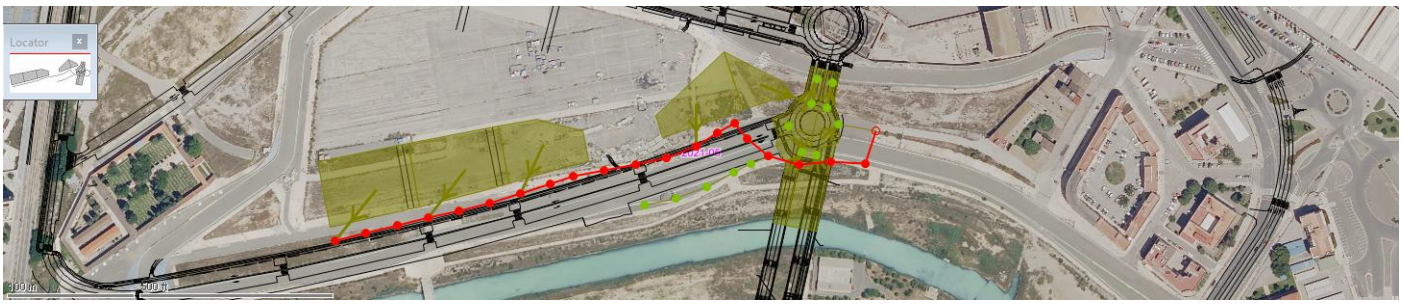
9:55:00	0.532	0.51688	0.535	1.157	1.068	0.00111	0.44	0.52	0.51688	0.559	1.189	1.101	0	0	11.9
10:00:00	0.532	0.51688	0.535	1.157	1.068	0.00111	0.44	0.52	0.51688	0.559	1.189	1.101	0	0	11.9
10:05:00	0.481	0.44135	0.553	1.104	1.041	0.00119	0.4	0.471	0.43436	0.568	1.135	1.054	0	0	10.4
10:00:00	0.425	0.34032	0.542	1.038	0.948	0.00111	0.35	0.413	0.33653	0.567	1.069	0.976	0	0	8.8
10:15:00	0.402	0.29794	0.528	1.01	0.896	0.00106	0.34	0.389	0.29672	0.562	1.04	0.935	0	0	8.1
10:20:00	0.396	0.28621	0.524	1.002	0.88	0.00104	0.33	0.382	0.28591	0.561	1.032	0.924	0	0	7.9
10:25:00	0.394	0.2837	0.523	1	0.877	0.00104	0.33	0.38	0.28365	0.561	1.03	0.922	0	0	7.9
10:30:00	0.394	0.28325	0.523	1	0.877	0.00104	0.33	0.38	0.28324	0.561	1.03	0.922	0	0	7.9
10:35:00	0.394	0.28317	0.523	1	0.876	0.00104	0.33	0.38	0.28317	0.561	1.03	0.922	0	0	7.9
10:40:00	0.394	0.28316	0.523	1	0.876	0.00104	0.33	0.38	0.28316	0.561	1.03	0.922	0	0	7.9
10:45:00	0.394	0.28316	0.523	1	0.876	0.00104	0.33	0.38	0.28316	0.561	1.03	0.922	0	0	7.9
10:50:00	0.394	0.28316	0.523	1	0.876	0.00104	0.33	0.38	0.28316	0.561	1.03	0.922	0	0	7.9
10:55:00	0.394	0.28316	0.523	1	0.876	0.00104	0.33	0.38	0.28316	0.561	1.03	0.922	0	0	7.9
11:00:00	0.394	0.28316	0.523	1	0.876	0.00104	0.33	0.38	0.28316	0.561	1.03	0.922	0	0	7.9
11:05:00	0.371	0.2583	0.536	0.976	0.869	0.0011	0.31	0.358	0.2549	0.565	1.007	0.899	0	0	7.3
11:10:00	0.339	0.21284	0.526	0.939	0.812	0.00107	0.28	0.326	0.21065	0.562	0.969	0.849	0	0	6.4
11:15:00	0.324	0.19022	0.513	0.921	0.773	0.00104	0.27	0.31	0.18942	0.558	0.951	0.819	0	0	6
11:20:00	0.319	0.18318	0.509	0.915	0.76	0.00102	0.27	0.305	0.18297	0.556	0.945	0.81	0	0	5.8
11:25:00	0.318	0.18157	0.508	0.914	0.757	0.00102	0.26	0.303	0.18152	0.556	0.944	0.808	0	0	5.8
11:30:00	0.318	0.18127	0.508	0.914	0.757	0.00102	0.26	0.303	0.18126	0.556	0.943	0.808	0	0	5.8
11:35:00	0.318	0.18122	0.508	0.914	0.756	0.00102	0.26	0.303	0.18122	0.556	0.943	0.808	0	0	5.8
11:40:00	0.318	0.18121	0.508	0.914	0.756	0.00102	0.26	0.303	0.18121	0.556	0.943	0.808	0	0	5.8
11:45:00	0.318	0.18121	0.508	0.914	0.756	0.00102	0.26	0.303	0.18121	0.556	0.943	0.808	0	0	5.8
11:50:00	0.318	0.18121	0.508	0.914	0.756	0.00102	0.26	0.303	0.18121	0.556	0.943	0.808	0	0	5.8
11:55:00	0.318	0.18121	0.508	0.914	0.756	0.00102	0.26	0.303	0.18121	0.556	0.943	0.808	0	0	5.8
12:00:00	0.318	0.18121	0.508	0.914	0.756	0.00102	0.26	0.303	0.18121	0.556	0.943	0.808	0	0	5.8
12:05:00	0.305	0.1711	0.519	0.901	0.756	0.00108	0.25	0.292	0.16924	0.559	0.931	0.795	0	0	5.5
12:10:00	0.285	0.14759	0.511	0.878	0.718	0.00107	0.24	0.272	0.14625	0.556	0.908	0.761	0	0	5
12:15:00	0.274	0.13385	0.5	0.865	0.688	0.00104	0.23	0.26	0.13327	0.551	0.895	0.738	0	0	4.7
12:20:00	0.27	0.12894	0.495	0.861	0.676	0.00103	0.23	0.256	0.12877	0.55	0.89	0.729	0	0	4.6
12:25:00	0.269	0.12766	0.494	0.859	0.673	0.00103	0.22	0.255	0.12762	0.549	0.889	0.727	0	0	4.5
12:30:00	0.269	0.12749	0.493	0.859	0.672	0.00103	0.22	0.255	0.12739	0.549	0.889	0.727	0	0	4.5
12:35:00	0.269	0.12736	0.493	0.859	0.672	0.00103	0.22	0.255	0.12735	0.549	0.889	0.727	0	0	4.5
12:40:00	0.269	0.12735	0.493	0.859	0.672	0.00103	0.22	0.255	0.12735	0.549	0.889	0.727	0	0	4.5
12:45:00	0.269	0.12735	0.493	0.859	0.672	0.00103	0.22	0.255	0.12735	0.549	0.889	0.727	0	0	4.5
12:50:00	0.269	0.12735	0.493	0.859	0.672	0.00103	0.22	0.255	0.12735	0.549	0.889	0.727	0	0	4.5
12:55:00	0.269	0.12735	0.493	0.859	0.672	0.00103	0.22	0.255	0.12735	0.549	0.889	0.727	0	0	4.5
13:00:00	0.269	0.12735	0.493	0.859	0.672	0.00103	0.22	0.255	0.12735	0.549	0.889	0.727	0	0	4.5
13:05:00	0.261	0.12254	0.502	0.851	0.674	0.00107	0.22	0.248	0.12142	0.551	0.881	0.719	0	0	4.4
13:10:00	0.248	0.10908	0.497	0.836	0.648	0.00107	0.21	0.234	0.10815	0.548	0.866	0.695	0	0	4
13:15:00	0.24	0.10013	0.486	0.826	0.623	0.00105	0.2	0.226	0.09972	0.544	0.856	0.675	0	0	3.8
13:20:00	0.236	0.09655	0.482	0.823	0.613	0.00104	0.2	0.222	0.09641	0.542	0.852	0.668	0	0	3.8
13:25:00	0.235	0.09552	0.48	0.821	0.61	0.00104	0.2	0.221	0.09549	0.541	0.851	0.665	0	0	3.7
13:30:00	0.235	0.0953	0.48	0.821	0.609	0.00104	0.2	0.221	0.09529	0.541	0.851	0.665	0	0	3.7
13:35:00	0.235	0.09525	0.48	0.821	0.609	0.00104	0.2	0.221	0.09525	0.541	0.851	0.665	0	0	3.7

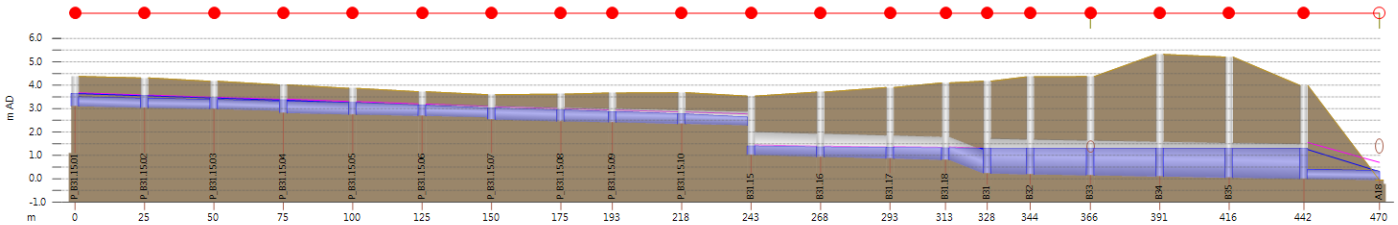
13:40:00	0.235	0.09525	0.48	0.821	0.609	0.00104	0.2	0.221	0.09525	0.541	0.851	0.665	0	0	3.7
13:45:00	0.235	0.09525	0.48	0.821	0.609	0.00104	0.2	0.221	0.09525	0.541	0.851	0.665	0	0	3.7
13:50:00	0.235	0.09525	0.48	0.821	0.609	0.00104	0.2	0.221	0.09525	0.541	0.851	0.665	0	0	3.7
13:55:00	0.235	0.09525	0.48	0.821	0.609	0.00104	0.2	0.221	0.09525	0.541	0.851	0.665	0	0	3.7
14:00:00	0.235	0.09525	0.48	0.821	0.609	0.00104	0.2	0.221	0.09525	0.541	0.851	0.665	0	0	3.7
14:05:00	0.23	0.09268	0.487	0.816	0.611	0.00108	0.19	0.217	0.09195	0.542	0.846	0.66	0	0	3.6
14:10:00	0.22	0.08438	0.483	0.805	0.593	0.00109	0.18	0.207	0.08372	0.54	0.835	0.641	0	0	3.4
14:15:00	0.214	0.07825	0.474	0.798	0.572	0.00107	0.18	0.201	0.07791	0.535	0.828	0.625	0	0	3.3
14:20:00	0.211	0.07556	0.469	0.795	0.563	0.00106	0.18	0.198	0.07543	0.533	0.824	0.618	0	0	3.2
14:25:00	0.211	0.07472	0.467	0.794	0.56	0.00106	0.18	0.197	0.07468	0.532	0.823	0.616	0	0	3.2
14:30:00	0.21	0.07451	0.467	0.793	0.559	0.00106	0.18	0.197	0.07451	0.532	0.823	0.615	0	0	3.2
14:35:00	0.21	0.07447	0.467	0.793	0.559	0.00106	0.18	0.197	0.07447	0.532	0.823	0.615	0	0	3.2
14:40:00	0.21	0.07447	0.467	0.793	0.559	0.00106	0.18	0.197	0.07447	0.532	0.823	0.615	0	0	3.2
14:45:00	0.21	0.07447	0.467	0.793	0.559	0.00106	0.18	0.197	0.07447	0.532	0.823	0.615	0	0	3.2
14:50:00	0.21	0.07447	0.467	0.793	0.559	0.00106	0.18	0.197	0.07447	0.532	0.823	0.615	0	0	3.2
14:55:00	0.21	0.07447	0.467	0.793	0.559	0.00106	0.18	0.197	0.07447	0.532	0.823	0.615	0	0	3.2
15:00:00	0.21	0.07447	0.467	0.793	0.559	0.00106	0.18	0.197	0.07447	0.532	0.823	0.615	0	0	3.2
15:05:00	0.207	0.07298	0.473	0.79	0.561	0.00109	0.17	0.194	0.07248	0.533	0.82	0.611	0	0	3.1
15:10:00	0.199	0.06755	0.47	0.782	0.548	0.0011	0.17	0.187	0.06707	0.53	0.812	0.597	0	0	2.9
15:15:00	0.195	0.06318	0.462	0.776	0.531	0.00109	0.16	0.182	0.06292	0.526	0.806	0.583	0	0	2.8
15:20:00	0.192	0.06111	0.457	0.773	0.522	0.00108	0.16	0.179	0.061	0.523	0.803	0.577	0	0	2.8
15:25:00	0.192	0.06041	0.455	0.772	0.519	0.00108	0.16	0.179	0.06038	0.523	0.802	0.574	0	0	2.8
15:30:00	0.191	0.06023	0.455	0.772	0.518	0.00108	0.16	0.178	0.06022	0.523	0.802	0.574	0	0	2.7
15:35:00	0.191	0.06019	0.455	0.772	0.518	0.00108	0.16	0.178	0.06019	0.523	0.802	0.574	0	0	2.7
15:40:00	0.191	0.06019	0.455	0.772	0.518	0.00108	0.16	0.178	0.06019	0.523	0.802	0.574	0	0	2.7
15:45:00	0.191	0.06018	0.455	0.772	0.518	0.00108	0.16	0.178	0.06018	0.523	0.802	0.574	0	0	2.7
15:50:00	0.191	0.06018	0.455	0.772	0.518	0.00108	0.16	0.178	0.06018	0.523	0.802	0.574	0	0	2.7
15:55:00	0.191	0.06018	0.455	0.772	0.518	0.00108	0.16	0.178	0.06018	0.523	0.802	0.574	0	0	2.7
16:00:00	0.191	0.06018	0.455	0.772	0.518	0.00108	0.16	0.178	0.06018	0.523	0.802	0.574	0	0	2.7
16:05:00	0.189	0.05927	0.46	0.769	0.52	0.0011	0.16	0.176	0.05891	0.523	0.8	0.571	0	0	2.7
16:10:00	0.183	0.05555	0.458	0.763	0.51	0.00112	0.15	0.171	0.05518	0.521	0.794	0.559	0	0	2.6
16:15:00	0.179	0.05234	0.45	0.759	0.495	0.00111	0.15	0.167	0.05213	0.516	0.789	0.547	0	0	2.5
16:20:00	0.177	0.05071	0.445	0.756	0.487	0.0011	0.15	0.165	0.05061	0.514	0.787	0.541	0	0	2.5
16:25:00	0.177	0.05011	0.444	0.756	0.485	0.0011	0.15	0.164	0.05008	0.513	0.786	0.539	0	0	2.4
16:30:00	0.176	0.04995	0.443	0.755	0.484	0.0011	0.15	0.164	0.04994	0.513	0.786	0.539	0	0	2.4
16:35:00	0.176	0.04992	0.443	0.755	0.484	0.0011	0.15	0.164	0.04992	0.513	0.785	0.539	0	0	2.4
16:40:00	0.176	0.04991	0.443	0.755	0.484	0.0011	0.15	0.164	0.04991	0.513	0.785	0.539	0	0	2.4
16:45:00	0.176	0.04991	0.443	0.755	0.484	0.0011	0.15	0.164	0.04991	0.513	0.785	0.539	0	0	2.4
16:50:00	0.176	0.04991	0.443	0.755	0.484	0.0011	0.15	0.164	0.04991	0.513	0.785	0.539	0	0	2.4
16:55:00	0.176	0.04991	0.443	0.755	0.484	0.0011	0.15	0.164	0.04991	0.513	0.785	0.539	0	0	2.4
17:00:00	0.176	0.04991	0.443	0.755	0.484	0.0011	0.15	0.164	0.04991	0.513	0.785	0.539	0	0	2.4
17:05:00	0.174	0.04931	0.448	0.753	0.486	0.00112	0.15	0.162	0.04905	0.513	0.784	0.536	0	0	2.4
17:10:00	0.17	0.04667	0.446	0.748	0.477	0.00113	0.14	0.158	0.04639	0.51	0.779	0.526	0	0	2.3
17:15:00	0.167	0.04425	0.439	0.745	0.465	0.00113	0.14	0.155	0.04408	0.506	0.775	0.516	0	0	2.2
17:20:00	0.165	0.04294	0.434	0.743	0.458	0.00112	0.14	0.153	0.04286	0.504	0.773	0.51	0	0	2.2

17:25:00	0.164	0.04243	0.433	0.742	0.455	0.00112	0.14	0.152	0.04241	0.503	0.772	0.508	0	0	2.2
17:30:00	0.164	0.04229	0.432	0.742	0.454	0.00112	0.14	0.152	0.04228	0.503	0.772	0.508	0	0	2.2
17:35:00	0.164	0.04225	0.432	0.742	0.454	0.00112	0.14	0.152	0.04225	0.503	0.772	0.508	0	0	2.2
17:40:00	0.164	0.04225	0.432	0.742	0.454	0.00112	0.14	0.152	0.04225	0.503	0.772	0.508	0	0	2.2
17:45:00	0.164	0.04225	0.432	0.742	0.454	0.00112	0.14	0.152	0.04225	0.503	0.772	0.508	0	0	2.2
17:50:00	0.164	0.04225	0.432	0.742	0.454	0.00112	0.14	0.152	0.04225	0.503	0.772	0.508	0	0	2.2
17:55:00	0.164	0.04225	0.432	0.742	0.454	0.00112	0.14	0.152	0.04225	0.503	0.772	0.508	0	0	2.2
18:00:00	0.164	0.04225	0.432	0.742	0.454	0.00112	0.14	0.152	0.04225	0.503	0.772	0.508	0	0	2.2
18:05:00	0.153	0.03956	0.462	0.732	0.469	0.00126	0.13	0.145	0.03825	0.5	0.764	0.493	0	0	2
18:10:00	0.126	0.02725	0.469	0.703	0.431	0.00144	0.11	0.122	0.02563	0.469	0.738	0.424	0	0	1.5
18:15:00	0.102	0.01613	0.421	0.675	0.347	0.00153	0.09	0.1	0.01502	0.406	0.713	0.332	0	0	1.1
18:20:00	0.086	0.00915	0.34	0.656	0.256	0.00155	0.07	0.084	0.00845	0.324	0.694	0.242	0	0	0.9
18:25:00	0.075	0.00503	0.252	0.643	0.172	0.00156	0.06	0.074	0.0046	0.237	0.682	0.161	0	0	0.7
18:30:00	0.068	0.00257	0.159	0.636	0.102	0.00157	0.06	0.067	0.00231	0.147	0.675	0.093	0	0	0.6
18:35:00	0.064	0.00122	0.086	0.631	0.053	0.00158	0.05	0.064	0.00107	0.078	0.671	0.048	0	0	0.6
18:40:00	0.062	0.00055	0.042	0.629	0.025	0.00158	0.05	0.062	0.00048	0.037	0.669	0.022	0	0	0.5
18:45:00	0.061	0.00024	0.019	0.628	0.011	0.00159	0.05	0.061	0.00021	0.017	0.668	0.01	0	0	0.5
18:50:00	0.061	0.00012	0.009	0.628	0.006	0.00159	0.05	0.06	0.00011	0.009	0.667	0.005	0	0	0.5
18:55:00	0.061	0.00008	0.006	0.628	0.004	0.00159	0.05	0.06	0.00007	0.006	0.667	0.004	0	0	0.5
19:00:00	0.06	0.00006	0.005	0.627	0.003	0.00159	0.05	0.06	0.00006	0.005	0.667	0.003	0	0	0.5
19:05:00	0.06	0.00006	0.005	0.627	0.003	0.00159	0.05	0.06	0.00006	0.005	0.667	0.003	0	0	0.5
19:10:00	0.06	0.00005	0.004	0.627	0.003	0.00159	0.05	0.06	0.00005	0.004	0.667	0.002	0	0	0.5
19:15:00	0.06	0.00004	0.003	0.627	0.002	0.00159	0.05	0.06	0.00004	0.003	0.667	0.002	0	0	0.5
19:20:00	0.06	0.00003	0.002	0.627	0.001	0.00159	0.05	0.06	0.00003	0.002	0.667	0.001	0	0	0.5
19:25:00	0.06	0.00002	0.002	0.627	0.001	0.00159	0.05	0.06	0.00002	0.002	0.667	0.001	0	0	0.5
19:30:00	0.06	0.00001	0.001	0.627	0.001	0.00159	0.05	0.06	0.00001	0.001	0.667	0	0	0	0.5
19:35:00	0.06	0.00001	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
19:40:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
19:45:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
19:50:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
19:55:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:00:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:05:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:10:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:15:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:20:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:25:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:30:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:35:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:40:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:45:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:50:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
20:55:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:00:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5

21:10:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:15:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:20:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:25:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:30:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:35:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:40:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:45:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:50:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
21:55:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:00:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:05:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:10:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:15:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:20:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:25:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:30:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:35:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:40:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:45:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:50:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
22:55:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:00:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:05:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:10:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:15:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:20:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:25:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:30:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:35:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:40:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:45:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:50:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
23:55:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5
0:00:00	0.06	0	0	0.627	0	0.00159	0.05	0.06	0	0	0.667	0	0	0	0.5

TRAMO C





Link		P_B31.15.01.1	P_B31.15.02.1	P_B31.15.03.1	P_B31.15.04.1	P_B31.15.05.1	P_B31.15.06.1	P_B31.15.07.1	-	P_B31.15.09.1	P_B31.15.10.1	B31.15.1	B31.16.1	B31.17.1	-	B31.1	B32.1	B33.1	B34.1	B35.1	P_B36.1	
Node	-	P_B31.15.02	P_B31.15.03	P_B31.15.04	P_B31.15.05	P_B31.15.06	P_B31.15.07	-	-	P_B31.15.10	B31.15	B31.16	B31.17	B31.18	B31	B32	B33	B34	B35	P_B36	A18

	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
0:05:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
0:10:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
0:15:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
0:20:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
0:25:00	0.023	0.00024	0.214	-0.03	0.081	0.00232	0.08	0.033	0.00087	0.388	0.034	0.181	0	0	0.1
0:30:00	0.06	0.00712	0.954	0.024	0.606	0.00294	0.21	0.086	0.00866	0.572	0.095	0.439	0	0	0.5
0:35:00	0.09	0.01617	0.978	0.066	0.769	0.00307	0.3	0.119	0.01672	0.581	0.134	0.533	0	0	0.8
0:40:00	0.098	0.01919	0.982	0.077	0.809	0.00314	0.32	0.129	0.01934	0.576	0.144	0.552	0	0	0.8
0:45:00	0.1	0.02005	0.983	0.08	0.819	0.00317	0.33	0.132	0.02009	0.574	0.148	0.557	0	0	0.9
0:50:00	0.1	0.02026	0.983	0.081	0.821	0.00317	0.33	0.132	0.02027	0.574	0.148	0.558	0	0	0.9
0:55:00	0.1	0.0203	0.983	0.081	0.822	0.00317	0.33	0.133	0.0203	0.574	0.148	0.558	0	0	0.9
1:00:00	0.1	0.02031	0.983	0.081	0.822	0.00317	0.33	0.133	0.02031	0.574	0.148	0.558	0	0	0.9
1:05:00	0.101	0.0204	0.983	0.081	0.823	0.00318	0.33	0.133	0.02043	0.574	0.149	0.56	0	0	0.9
1:10:00	0.102	0.02115	0.984	0.084	0.832	0.0032	0.34	0.136	0.02126	0.575	0.152	0.567	0	0	0.9
1:15:00	0.106	0.02257	0.985	0.089	0.847	0.00324	0.35	0.14	0.02271	0.578	0.157	0.58	0	0	0.9
1:20:00	0.109	0.0237	0.986	0.092	0.859	0.00325	0.36	0.143	0.02376	0.581	0.161	0.59	0	0	1
1:25:00	0.11	0.02412	0.986	0.094	0.864	0.00325	0.36	0.144	0.02414	0.582	0.162	0.593	0	0	1
1:30:00	0.11	0.02422	0.986	0.094	0.865	0.00325	0.36	0.144	0.02423	0.582	0.162	0.594	0	0	1
1:35:00	0.11	0.02424	0.986	0.094	0.865	0.00325	0.36	0.144	0.02424	0.582	0.162	0.594	0	0	1
1:40:00	0.11	0.02425	0.986	0.094	0.865	0.00325	0.36	0.144	0.02425	0.582	0.162	0.594	0	0	1
1:45:00	0.11	0.02425	0.986	0.094	0.865	0.00325	0.36	0.144	0.02425	0.582	0.162	0.594	0	0	1
1:50:00	0.11	0.02425	0.986	0.094	0.865	0.00325	0.36	0.144	0.02425	0.582	0.162	0.594	0	0	1
1:55:00	0.11	0.02425	0.986	0.094	0.865	0.00325	0.36	0.144	0.02425	0.582	0.162	0.594	0	0	1
2:00:00	0.11	0.02425	0.986	0.094	0.865	0.00325	0.36	0.144	0.02425	0.582	0.162	0.594	0	0	1
2:05:00	0.11	0.02439	0.986	0.094	0.867	0.00326	0.36	0.145	0.02444	0.583	0.163	0.596	0	0	1
2:10:00	0.113	0.02559	0.987	0.098	0.879	0.00328	0.37	0.148	0.02575	0.589	0.167	0.61	0	0	1
2:15:00	0.117	0.02765	0.988	0.105	0.899	0.00332	0.38	0.154	0.02781	0.591	0.174	0.625	0	0	1.1

2:20:00	0.12	0.02897	0.988	0.109	0.911	0.00336	0.39	0.157	0.02904	0.589	0.178	0.632	0	0	1.1
2:25:00	0.121	0.02944	0.989	0.11	0.915	0.00337	0.4	0.159	0.02946	0.588	0.179	0.634	0	0	1.1
2:30:00	0.121	0.02956	0.989	0.11	0.917	0.00337	0.4	0.159	0.02957	0.588	0.18	0.635	0	0	1.1
2:35:00	0.122	0.02959	0.989	0.11	0.917	0.00337	0.4	0.159	0.02959	0.588	0.18	0.635	0	0	1.1
2:40:00	0.122	0.02959	0.989	0.11	0.917	0.00337	0.4	0.159	0.02959	0.588	0.18	0.635	0	0	1.1
2:45:00	0.122	0.02959	0.989	0.11	0.917	0.00337	0.4	0.159	0.02959	0.588	0.18	0.635	0	0	1.1
2:50:00	0.122	0.02959	0.989	0.11	0.917	0.00337	0.4	0.159	0.02959	0.588	0.18	0.635	0	0	1.1
2:55:00	0.122	0.02959	0.989	0.11	0.917	0.00337	0.4	0.159	0.02959	0.588	0.18	0.635	0	0	1.1
3:00:00	0.122	0.02959	0.989	0.11	0.917	0.00337	0.4	0.159	0.02959	0.588	0.18	0.635	0	0	1.1
3:05:00	0.122	0.02982	0.989	0.111	0.919	0.00338	0.4	0.16	0.02988	0.588	0.181	0.637	0	0	1.1
3:10:00	0.126	0.03169	0.989	0.116	0.935	0.00344	0.41	0.165	0.03193	0.589	0.187	0.651	0	0	1.2
3:15:00	0.132	0.0347	0.99	0.125	0.961	0.00348	0.43	0.172	0.0349	0.594	0.196	0.673	0	0	1.2
3:20:00	0.135	0.03641	0.991	0.13	0.975	0.0035	0.44	0.176	0.03649	0.596	0.2	0.684	0	0	1.3
3:25:00	0.136	0.03699	0.991	0.131	0.979	0.00351	0.44	0.178	0.03702	0.596	0.202	0.687	0	0	1.3
3:30:00	0.137	0.03714	0.991	0.132	0.981	0.00351	0.44	0.178	0.03715	0.596	0.202	0.688	0	0	1.3
3:35:00	0.137	0.03718	0.991	0.132	0.981	0.00351	0.44	0.178	0.03718	0.596	0.202	0.688	0	0	1.3
3:40:00	0.137	0.03718	0.991	0.132	0.981	0.00351	0.44	0.178	0.03718	0.596	0.202	0.688	0	0	1.3
3:45:00	0.137	0.03718	0.991	0.132	0.981	0.00351	0.44	0.178	0.03718	0.596	0.202	0.688	0	0	1.3
3:50:00	0.137	0.03718	0.991	0.132	0.981	0.00351	0.44	0.178	0.03718	0.596	0.202	0.688	0	0	1.3
3:55:00	0.137	0.03718	0.991	0.132	0.981	0.00351	0.44	0.178	0.03718	0.596	0.202	0.688	0	0	1.3
4:00:00	0.137	0.03718	0.991	0.132	0.981	0.00351	0.44	0.178	0.03718	0.596	0.202	0.688	0	0	1.3
4:05:00	0.137	0.03761	0.991	0.133	0.984	0.00352	0.45	0.179	0.03771	0.597	0.203	0.692	0	0	1.3
4:10:00	0.143	0.04063	0.992	0.141	1.007	0.0036	0.47	0.187	0.04093	0.598	0.213	0.711	0	0	1.4
4:15:00	0.151	0.04511	0.992	0.152	1.04	0.00371	0.49	0.198	0.0454	0.595	0.225	0.733	0	0	1.5
4:20:00	0.155	0.04766	0.993	0.158	1.057	0.00373	0.51	0.203	0.04775	0.598	0.231	0.748	0	0	1.5
4:25:00	0.156	0.04835	0.993	0.16	1.062	0.00374	0.51	0.204	0.04837	0.598	0.233	0.751	0	0	1.5
4:30:00	0.157	0.04851	0.993	0.16	1.063	0.00374	0.51	0.204	0.04851	0.598	0.233	0.752	0	0	1.5
4:35:00	0.157	0.04853	0.993	0.16	1.063	0.00374	0.51	0.204	0.04853	0.598	0.233	0.752	0	0	1.5
4:40:00	0.157	0.04853	0.993	0.16	1.063	0.00374	0.51	0.204	0.04853	0.598	0.233	0.752	0	0	1.5
4:45:00	0.157	0.04854	0.993	0.16	1.063	0.00374	0.51	0.204	0.04854	0.598	0.233	0.752	0	0	1.5
4:50:00	0.157	0.04854	0.993	0.16	1.063	0.00374	0.51	0.204	0.04854	0.598	0.233	0.752	0	0	1.5
4:55:00	0.157	0.04854	0.993	0.16	1.063	0.00374	0.51	0.204	0.04854	0.598	0.233	0.752	0	0	1.5
5:00:00	0.157	0.04854	0.993	0.16	1.063	0.00374	0.51	0.204	0.04854	0.598	0.233	0.752	0	0	1.5
5:05:00	0.158	0.04946	0.993	0.163	1.069	0.00376	0.52	0.206	0.04966	0.6	0.236	0.76	0	0	1.6
5:10:00	0.168	0.05542	0.994	0.176	1.108	0.00391	0.55	0.22	0.05597	0.598	0.252	0.79	0	0	1.7
5:15:00	0.179	0.06269	0.994	0.192	1.151	0.00403	0.59	0.234	0.06289	0.597	0.269	0.823	0	0	1.8
5:20:00	0.183	0.06563	0.995	0.199	1.169	0.00407	0.6	0.24	0.06573	0.596	0.275	0.836	0	0	1.9
5:25:00	0.184	0.06648	0.995	0.201	1.174	0.00409	0.6	0.242	0.06651	0.594	0.277	0.838	0	0	1.9
5:30:00	0.185	0.06669	0.995	0.201	1.175	0.0041	0.6	0.242	0.06669	0.594	0.278	0.839	0	0	1.9
5:35:00	0.185	0.06673	0.995	0.201	1.175	0.0041	0.61	0.242	0.06673	0.594	0.278	0.839	0	0	1.9
5:40:00	0.185	0.06674	0.995	0.201	1.175	0.0041	0.61	0.242	0.06674	0.594	0.278	0.839	0	0	1.9
5:45:00	0.185	0.06674	0.995	0.201	1.176	0.0041	0.61	0.242	0.06674	0.594	0.278	0.839	0	0	1.9
5:50:00	0.185	0.06674	0.995	0.201	1.176	0.0041	0.61	0.242	0.06674	0.594	0.278	0.839	0	0	1.9
5:55:00	0.185	0.06674	0.995	0.201	1.176	0.0041	0.61	0.242	0.06674	0.594	0.278	0.839	0	0	1.9
6:00:00	0.185	0.06674	0.995	0.201	1.176	0.0041	0.61	0.242	0.06674	0.594	0.278	0.839	0	0	1.9

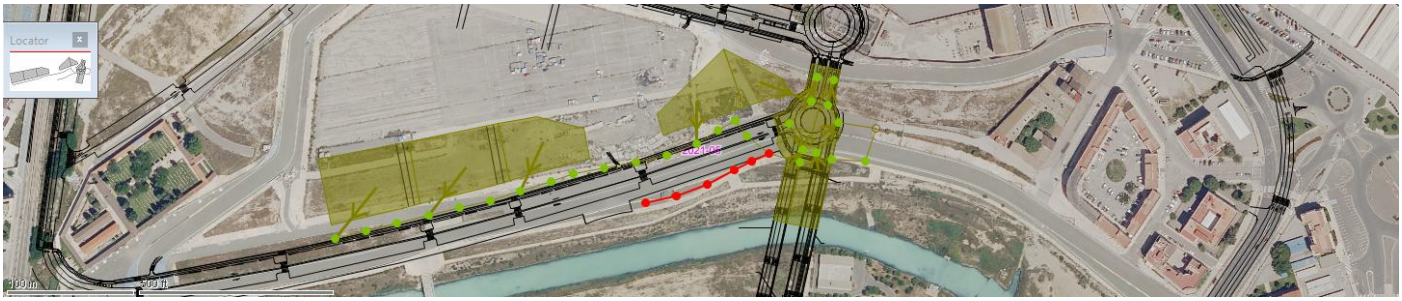
6:05:00	0.188	0.06877	0.995	0.206	1.187	0.00416	0.62	0.247	0.06914	0.593	0.284	0.849	0	0	1.9
6:10:00	0.204	0.08072	0.995	0.23	1.252	0.00442	0.68	0.27	0.08146	0.586	0.312	0.901	0	0	2.2
6:15:00	0.219	0.09251	0.996	0.253	1.313	0.00467	0.73	0.292	0.09292	0.574	0.338	0.945	0	0	2.4
6:20:00	0.225	0.09694	0.996	0.261	1.335	0.0048	0.75	0.301	0.09708	0.564	0.348	0.957	0	0	2.4
6:25:00	0.226	0.09838	0.997	0.264	1.342	0.00485	0.76	0.304	0.09842	0.56	0.351	0.96	0	0	2.5
6:30:00	0.227	0.0988	0.997	0.265	1.344	0.00486	0.76	0.305	0.09882	0.559	0.352	0.961	0	0	2.5
6:35:00	0.227	0.09893	0.997	0.265	1.345	0.00487	0.76	0.305	0.09893	0.559	0.352	0.962	0	0	2.5
6:40:00	0.227	0.09896	0.997	0.265	1.345	0.00487	0.76	0.305	0.09896	0.558	0.352	0.962	0	0	2.5
6:45:00	0.227	0.09897	0.997	0.265	1.345	0.00487	0.76	0.305	0.09897	0.558	0.352	0.962	0	0	2.5
6:50:00	0.227	0.09897	0.997	0.265	1.345	0.00487	0.76	0.305	0.09897	0.558	0.352	0.962	0	0	2.5
6:55:00	0.227	0.09897	0.997	0.265	1.345	0.00487	0.76	0.305	0.09897	0.558	0.352	0.962	0	0	2.5
7:00:00	0.227	0.09897	0.997	0.265	1.345	0.00487	0.76	0.305	0.09897	0.558	0.352	0.962	0	0	2.5
7:05:00	0.234	0.10509	0.997	0.277	1.375	0.00505	0.79	0.317	0.10585	0.55	0.367	0.99	0	0	2.5
7:10:00	0.259	0.12763	0.997	0.317	1.482	0.00618	0.93	0.373	0.12862	0.434	0.43	1.054	0	0	2.9
7:15:00	0.276	0.14425	0.998	0.346	1.561	0.00736	2	0.422	0.14468	0.285	0.486	1.121	0	0	3.1
7:20:00	0.285	0.15346	0.998	0.362	1.605	0.00805	2	0.449	0.15374	0.15	0.52	1.179	0	0	3.2
7:25:00	0.289	0.15829	0.998	0.37	1.628	0.00845	2	0.465	0.15839	0.096	0.54	1.213	0	0	3.2
7:30:00	0.292	0.16105	0.998	0.375	1.641	0.00868	2	0.473	0.1611	0.097	0.551	1.233	0	0	3.3
7:35:00	0.293	0.16268	0.998	0.378	1.649	0.00882	2	0.479	0.16271	0.098	0.558	1.245	0	0	3.3
7:40:00	0.294	0.16367	0.998	0.379	1.654	0.00891	2	0.482	0.16369	0.099	0.562	1.252	0	0	3.3
7:45:00	0.294	0.16427	0.998	0.38	1.657	0.00896	2	0.484	0.16429	0.099	0.564	1.257	0	0	3.3
7:50:00	0.295	0.16466	0.998	0.381	1.659	0.009	2	0.485	0.16467	0.1	0.566	1.26	0	0	3.3
7:55:00	0.295	0.1649	0.998	0.381	1.66	0.00902	2	0.486	0.1649	0.1	0.567	1.261	0	0	3.3
8:00:00	0.295	0.16504	0.998	0.382	1.661	0.00903	2	0.486	0.16504	0.1	0.568	1.262	0	0	3.3
8:05:00	0.305	0.1768	0.998	0.402	1.719	0.01024	2	0.529	0.1773	0.107	0.623	1.353	0	0	3.4
8:10:00	0.334	0.21484	0.998	0.467	1.918	0.01455	2	0.675	0.21511	0.128	0.81	1.627	0	0	3.5
8:15:00	0.353	0.24824	0.999	0.527	2.114	0.0193	2	0.823	0.24834	0.146	1	1.861	0	0	3.5
8:20:00	0.36	0.27245	1.036	0.573	2.287	0.02328	2	0.938	0.27249	0.158	1.148	2.028	0	0	3.5
8:25:00	0.36	0.28978	1.102	0.608	2.433	0.02637	2	1.022	0.2898	0.167	1.257	2.146	0	0	3.6
8:30:00	0.36	0.30204	1.149	0.634	2.535	0.02869	2	1.085	0.30206	0.173	1.338	2.229	0	0	3.6
8:35:00	0.36	0.31083	1.182	0.653	2.609	0.03041	2	1.132	0.31085	0.177	1.399	2.287	0	0	3.6
8:40:00	0.36	0.31729	1.207	0.668	2.664	0.03171	2	1.167	0.3173	0.18	1.444	2.33	0	0	3.6
8:45:00	0.36	0.32229	1.226	0.679	2.705	0.03274	2	1.195	0.3223	0.183	1.48	2.363	0	0	3.6
8:50:00	0.36	0.32611	1.24	0.688	2.737	0.03353	2	1.217	0.32611	0.185	1.507	2.388	0	0	3.6
8:55:00	0.36	0.32909	1.252	0.695	2.763	0.03417	2	1.234	0.3291	0.186	1.529	2.407	0	0	3.6
9:00:00	0.36	0.3315	1.261	0.701	2.783	0.03468	2	1.248	0.3315	0.187	1.547	2.423	0	0	3.6
9:05:00	0.36	0.32812	1.248	0.693	2.754	0.03394	2	1.228	0.3281	0.185	1.522	2.401	0	0	3.6
9:10:00	0.36	0.31487	1.198	0.662	2.643	0.03118	2	1.153	0.31484	0.179	1.426	2.314	0	0	3.6
9:15:00	0.36	0.29801	1.134	0.625	2.502	0.02787	2	1.063	0.29798	0.171	1.31	2.202	0	0	3.6
9:20:00	0.36	0.28247	1.075	0.593	2.371	0.02498	2	0.985	0.28244	0.163	1.209	2.097	0	0	3.6
9:25:00	0.36	0.26912	1.024	0.566	2.259	0.02264	2	0.921	0.2691	0.156	1.126	2.005	0	0	3.5
9:30:00	0.358	0.25888	0.998	0.547	2.18	0.02096	2	0.874	0.25883	0.151	1.064	1.934	0	0	3.5
9:35:00	0.355	0.25115	0.999	0.532	2.132	0.01968	2	0.835	0.25113	0.147	1.016	1.881	0	0	3.5
9:40:00	0.352	0.24526	0.999	0.521	2.095	0.01876	2	0.807	0.24524	0.144	0.98	1.84	0	0	3.5
9:45:00	0.349	0.24093	0.999	0.514	2.069	0.0181	2	0.787	0.24091	0.142	0.954	1.809	0	0	3.5

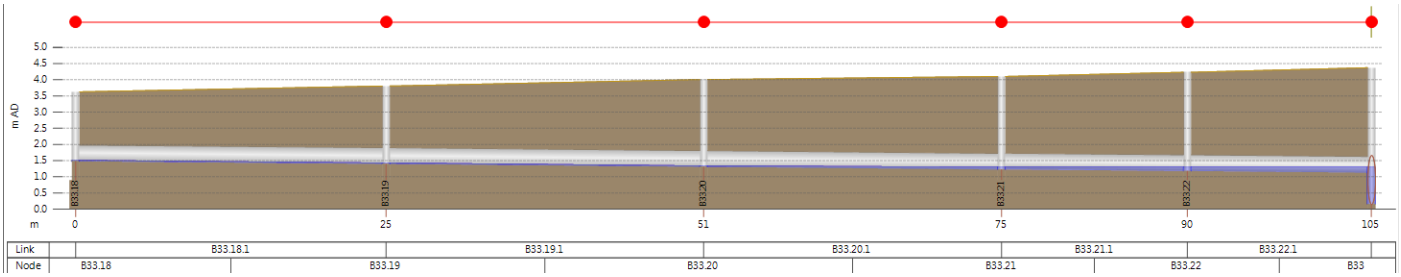
9:50:00	0.348	0.23775	0.999	0.508	2.05	0.01762	2	0.772	0.23774	0.14	0.935	1.787	0	0	3.5
9:55:00	0.346	0.23546	0.999	0.504	2.036	0.01728	2	0.762	0.23545	0.139	0.922	1.771	0	0	3.5
10:00:00	0.345	0.2338	0.999	0.501	2.026	0.01704	2	0.754	0.23379	0.138	0.912	1.759	0	0	3.5
10:05:00	0.341	0.227	0.998	0.489	1.987	0.01605	2	0.723	0.22694	0.134	0.872	1.711	0	0	3.5
10:10:00	0.328	0.20691	0.998	0.453	1.875	0.0134	2	0.638	0.20672	0.123	0.763	1.567	0	0	3.5
10:15:00	0.31	0.18267	0.998	0.412	1.748	0.0107	2	0.547	0.18238	0.11	0.645	1.39	0	0	3.4
10:20:00	0.293	0.16279	0.998	0.378	1.65	0.00879	2	0.478	0.16235	0.098	0.556	1.242	0	0	3.3
10:25:00	0.279	0.14768	0.998	0.352	1.577	0.00754	2	0.43	0.14723	0.249	0.496	1.136	0	0	3.1
10:30:00	0.269	0.13715	0.997	0.334	1.527	0.00683	2	0.4	0.13679	0.36	0.46	1.08	0	0	3
10:35:00	0.263	0.13155	0.997	0.324	1.501	0.0064	0.96	0.383	0.13133	0.409	0.44	1.06	0	0	2.9
10:40:00	0.26	0.12849	0.997	0.318	1.486	0.00619	0.94	0.374	0.12829	0.429	0.43	1.05	0	0	2.9
10:45:00	0.258	0.12686	0.997	0.316	1.479	0.0061	0.92	0.37	0.12681	0.44	0.426	1.045	0	0	2.9
10:50:00	0.257	0.12617	0.997	0.314	1.475	0.00606	0.92	0.368	0.12615	0.445	0.424	1.043	0	0	2.9
10:55:00	0.257	0.12587	0.997	0.314	1.474	0.00605	0.92	0.367	0.12586	0.448	0.423	1.042	0	0	2.9
11:00:00	0.257	0.12574	0.997	0.314	1.473	0.00604	0.92	0.367	0.12574	0.448	0.422	1.041	0	0	2.9
11:05:00	0.253	0.12185	0.997	0.307	1.455	0.00586	0.9	0.358	0.12146	0.47	0.411	1.024	0	0	2.8
11:10:00	0.238	0.1081	0.997	0.282	1.389	0.0051	0.81	0.322	0.1071	0.538	0.372	0.987	0	0	2.6
11:15:00	0.218	0.09159	0.996	0.251	1.308	0.00462	0.72	0.29	0.09088	0.571	0.334	0.933	0	0	2.3
11:20:00	0.208	0.08351	0.996	0.236	1.267	0.00447	0.69	0.275	0.0833	0.579	0.317	0.904	0	0	2.2
11:25:00	0.205	0.08116	0.996	0.231	1.254	0.00441	0.68	0.27	0.0811	0.583	0.311	0.897	0	0	2.2
11:30:00	0.204	0.08058	0.996	0.23	1.251	0.0044	0.67	0.269	0.08056	0.584	0.31	0.895	0	0	2.2
11:35:00	0.204	0.08045	0.996	0.229	1.251	0.00439	0.67	0.269	0.08045	0.584	0.31	0.895	0	0	2.2
11:40:00	0.204	0.08043	0.996	0.229	1.25	0.00439	0.67	0.269	0.08043	0.584	0.31	0.895	0	0	2.2
11:45:00	0.204	0.08042	0.996	0.229	1.25	0.00439	0.67	0.269	0.08042	0.584	0.31	0.895	0	0	2.2
11:50:00	0.204	0.08042	0.996	0.229	1.25	0.00439	0.67	0.269	0.08042	0.584	0.31	0.895	0	0	2.2
11:55:00	0.204	0.08042	0.996	0.229	1.25	0.00439	0.67	0.269	0.08042	0.584	0.31	0.895	0	0	2.2
12:00:00	0.204	0.08042	0.996	0.229	1.25	0.00439	0.67	0.269	0.08042	0.584	0.31	0.895	0	0	2.2
12:05:00	0.201	0.07874	0.996	0.226	1.242	0.00435	0.66	0.266	0.07848	0.584	0.306	0.886	0	0	2.1
12:10:00	0.19	0.07067	0.995	0.21	1.198	0.00418	0.63	0.25	0.0701	0.586	0.287	0.848	0	0	2
12:15:00	0.178	0.06205	0.994	0.191	1.148	0.004	0.58	0.233	0.06165	0.593	0.266	0.813	0	0	1.8
12:20:00	0.172	0.05799	0.994	0.182	1.124	0.00395	0.56	0.225	0.05784	0.592	0.257	0.794	0	0	1.7
12:25:00	0.17	0.05686	0.994	0.18	1.117	0.00393	0.56	0.223	0.05682	0.593	0.255	0.79	0	0	1.7
12:30:00	0.17	0.05659	0.994	0.179	1.115	0.00392	0.56	0.222	0.05658	0.594	0.254	0.79	0	0	1.7
12:35:00	0.17	0.05653	0.994	0.179	1.115	0.00392	0.56	0.222	0.05653	0.594	0.254	0.789	0	0	1.7
12:40:00	0.17	0.05652	0.994	0.179	1.115	0.00392	0.55	0.222	0.05652	0.594	0.254	0.789	0	0	1.7
12:45:00	0.17	0.05652	0.994	0.179	1.115	0.00392	0.55	0.222	0.05652	0.594	0.254	0.789	0	0	1.7
12:50:00	0.17	0.05652	0.994	0.179	1.115	0.00392	0.55	0.222	0.05652	0.594	0.254	0.789	0	0	1.7
12:55:00	0.17	0.05652	0.994	0.179	1.115	0.00392	0.55	0.222	0.05652	0.594	0.254	0.789	0	0	1.7
13:00:00	0.17	0.05652	0.994	0.179	1.115	0.00392	0.55	0.222	0.05652	0.594	0.254	0.789	0	0	1.7
13:05:00	0.168	0.05575	0.994	0.177	1.11	0.00389	0.55	0.22	0.05559	0.594	0.251	0.784	0	0	1.7
13:10:00	0.161	0.0514	0.993	0.167	1.082	0.00377	0.52	0.21	0.051	0.597	0.24	0.764	0	0	1.6
13:15:00	0.152	0.04603	0.993	0.154	1.046	0.0037	0.5	0.199	0.04575	0.592	0.226	0.733	0	0	1.5
13:20:00	0.148	0.04346	0.992	0.148	1.028	0.00366	0.48	0.194	0.04335	0.592	0.22	0.72	0	0	1.4
13:25:00	0.146	0.04258	0.992	0.146	1.022	0.00364	0.48	0.191	0.04255	0.593	0.218	0.716	0	0	1.4
13:30:00	0.146	0.04234	0.992	0.145	1.02	0.00364	0.48	0.191	0.04233	0.594	0.217	0.715	0	0	1.4

13:35:00	0.146	0.04229	0.992	0.145	1.019	0.00364	0.48	0.191	0.04229	0.594	0.217	0.715	0	0	1.4
13:40:00	0.146	0.04228	0.992	0.145	1.019	0.00364	0.48	0.191	0.04228	0.594	0.217	0.715	0	0	1.4
13:45:00	0.146	0.04227	0.992	0.145	1.019	0.00364	0.48	0.191	0.04227	0.594	0.217	0.715	0	0	1.4
13:50:00	0.146	0.04227	0.992	0.145	1.019	0.00364	0.48	0.191	0.04227	0.594	0.217	0.715	0	0	1.4
13:55:00	0.146	0.04227	0.992	0.145	1.019	0.00364	0.48	0.191	0.04227	0.594	0.217	0.715	0	0	1.4
14:00:00	0.146	0.04227	0.992	0.145	1.019	0.00364	0.48	0.191	0.04227	0.594	0.217	0.715	0	0	1.4
14:05:00	0.145	0.04191	0.992	0.144	1.017	0.00362	0.47	0.19	0.04183	0.594	0.216	0.713	0	0	1.4
14:10:00	0.141	0.03957	0.991	0.138	0.999	0.00355	0.46	0.184	0.03932	0.594	0.208	0.699	0	0	1.4
14:15:00	0.135	0.03614	0.991	0.129	0.973	0.00348	0.44	0.175	0.0359	0.593	0.199	0.678	0	0	1.3
14:20:00	0.13	0.034	0.99	0.123	0.955	0.00347	0.43	0.171	0.0339	0.589	0.193	0.663	0	0	1.2
14:25:00	0.129	0.03328	0.99	0.121	0.949	0.00346	0.42	0.169	0.03325	0.588	0.191	0.658	0	0	1.2
14:30:00	0.129	0.0331	0.99	0.12	0.948	0.00346	0.42	0.169	0.03309	0.588	0.191	0.657	0	0	1.2
14:35:00	0.129	0.03306	0.99	0.12	0.947	0.00346	0.42	0.169	0.03306	0.588	0.191	0.657	0	0	1.2
14:40:00	0.129	0.03305	0.99	0.12	0.947	0.00346	0.42	0.169	0.03305	0.588	0.191	0.657	0	0	1.2
14:45:00	0.129	0.03305	0.99	0.12	0.947	0.00346	0.42	0.169	0.03305	0.588	0.191	0.657	0	0	1.2
14:50:00	0.129	0.03305	0.99	0.12	0.947	0.00346	0.42	0.169	0.03305	0.588	0.191	0.657	0	0	1.2
14:55:00	0.129	0.03305	0.99	0.12	0.947	0.00346	0.42	0.169	0.03305	0.588	0.191	0.657	0	0	1.2
15:00:00	0.129	0.03305	0.99	0.12	0.947	0.00346	0.42	0.169	0.03305	0.588	0.191	0.657	0	0	1.2
15:05:00	0.128	0.03284	0.99	0.12	0.945	0.00345	0.42	0.168	0.03278	0.587	0.19	0.655	0	0	1.2
15:10:00	0.125	0.03132	0.989	0.115	0.932	0.00341	0.41	0.164	0.03112	0.585	0.185	0.643	0	0	1.2
15:15:00	0.12	0.02901	0.988	0.109	0.912	0.00335	0.39	0.157	0.02883	0.586	0.177	0.629	0	0	1.1
15:20:00	0.117	0.02746	0.988	0.104	0.897	0.00331	0.38	0.153	0.02738	0.588	0.172	0.62	0	0	1.1
15:25:00	0.116	0.02689	0.987	0.102	0.892	0.0033	0.38	0.151	0.02687	0.588	0.171	0.617	0	0	1.1
15:30:00	0.115	0.02675	0.987	0.102	0.89	0.00329	0.38	0.151	0.02674	0.588	0.17	0.616	0	0	1
15:35:00	0.115	0.02672	0.987	0.102	0.89	0.00329	0.38	0.151	0.02672	0.588	0.17	0.616	0	0	1
15:40:00	0.115	0.02671	0.987	0.102	0.89	0.00329	0.38	0.151	0.02671	0.588	0.17	0.616	0	0	1
15:45:00	0.115	0.02671	0.987	0.102	0.89	0.00329	0.38	0.151	0.02671	0.588	0.17	0.616	0	0	1
15:50:00	0.115	0.02671	0.987	0.102	0.89	0.00329	0.38	0.151	0.02671	0.588	0.17	0.616	0	0	1
15:55:00	0.115	0.02671	0.987	0.102	0.89	0.00329	0.38	0.151	0.02671	0.588	0.17	0.616	0	0	1
16:00:00	0.115	0.02671	0.987	0.102	0.89	0.00329	0.38	0.151	0.02671	0.588	0.17	0.616	0	0	1
16:05:00	0.115	0.02659	0.987	0.101	0.889	0.00329	0.38	0.15	0.02655	0.588	0.17	0.615	0	0	1
16:10:00	0.113	0.02558	0.987	0.098	0.879	0.00326	0.37	0.148	0.02545	0.585	0.166	0.605	0	0	1
16:15:00	0.109	0.02391	0.986	0.093	0.862	0.00324	0.36	0.143	0.02377	0.579	0.161	0.588	0	0	1
16:20:00	0.106	0.02278	0.985	0.089	0.85	0.00323	0.35	0.14	0.02271	0.575	0.157	0.578	0	0	0.9
16:25:00	0.105	0.02232	0.985	0.088	0.845	0.00323	0.35	0.139	0.0223	0.575	0.156	0.575	0	0	0.9
16:30:00	0.105	0.02219	0.985	0.087	0.843	0.00323	0.35	0.139	0.02218	0.575	0.155	0.574	0	0	0.9
16:35:00	0.105	0.02216	0.985	0.087	0.843	0.00322	0.35	0.139	0.02216	0.575	0.155	0.574	0	0	0.9
16:40:00	0.105	0.02215	0.985	0.087	0.843	0.00322	0.35	0.139	0.02215	0.575	0.155	0.574	0	0	0.9
16:45:00	0.105	0.02215	0.985	0.087	0.843	0.00322	0.35	0.138	0.02215	0.575	0.155	0.574	0	0	0.9
16:50:00	0.105	0.02215	0.985	0.087	0.843	0.00322	0.35	0.138	0.02215	0.575	0.155	0.574	0	0	0.9
16:55:00	0.105	0.02215	0.985	0.087	0.843	0.00322	0.35	0.138	0.02215	0.575	0.155	0.574	0	0	0.9
17:00:00	0.105	0.02215	0.985	0.087	0.843	0.00322	0.35	0.138	0.02215	0.575	0.155	0.574	0	0	0.9
17:05:00	0.105	0.02207	0.985	0.087	0.842	0.00322	0.35	0.138	0.02204	0.574	0.155	0.572	0	0	0.9
17:10:00	0.103	0.02142	0.984	0.085	0.835	0.0032	0.34	0.136	0.02133	0.573	0.152	0.566	0	0	0.9
17:15:00	0.1	0.02027	0.983	0.081	0.821	0.00316	0.33	0.132	0.02016	0.572	0.148	0.556	0	0	0.9

17:20:00	0.098	0.01934	0.983	0.077	0.81	0.00313	0.32	0.129	0.01927	0.573	0.144	0.55	0	0	0.8
17:25:00	0.097	0.01892	0.982	0.076	0.805	0.00312	0.32	0.128	0.01889	0.574	0.143	0.547	0	0	0.8
17:30:00	0.097	0.01879	0.982	0.075	0.804	0.00312	0.32	0.127	0.01878	0.574	0.142	0.546	0	0	0.8
17:35:00	0.096	0.01876	0.982	0.075	0.803	0.00312	0.32	0.127	0.01876	0.575	0.142	0.546	0	0	0.8
17:40:00	0.096	0.01875	0.982	0.075	0.803	0.00312	0.32	0.127	0.01875	0.575	0.142	0.546	0	0	0.8
17:45:00	0.096	0.01875	0.982	0.075	0.803	0.00312	0.32	0.127	0.01875	0.575	0.142	0.546	0	0	0.8
17:50:00	0.096	0.01875	0.982	0.075	0.803	0.00312	0.32	0.127	0.01875	0.575	0.142	0.546	0	0	0.8
17:55:00	0.096	0.01875	0.982	0.075	0.803	0.00312	0.32	0.127	0.01875	0.575	0.142	0.546	0	0	0.8
18:00:00	0.096	0.01875	0.982	0.075	0.803	0.00312	0.32	0.127	0.01875	0.575	0.142	0.546	0	0	0.8
18:05:00	0.095	0.01836	0.982	0.074	0.798	0.00309	0.31	0.125	0.01822	0.573	0.14	0.54	0	0	0.8
18:10:00	0.086	0.01498	0.977	0.061	0.752	0.00299	0.28	0.114	0.01444	0.551	0.126	0.492	0	0	0.7
18:15:00	0.069	0.00956	0.963	0.037	0.66	0.00277	0.23	0.09	0.00894	0.531	0.099	0.42	0	0	0.5
18:20:00	0.051	0.00507	0.934	0.012	0.546	0.0026	0.17	0.067	0.00459	0.484	0.073	0.327	0	0	0.3
18:25:00	0.038	0.00255	0.833	-0.007	0.42	0.00246	0.13	0.051	0.00225	0.417	0.054	0.243	0	0	0.2
18:30:00	0.031	0.00125	0.605	-0.019	0.276	0.00221	0.09	0.037	0.00103	0.352	0.039	0.175	0	0	0.2
18:35:00	0.026	0.00055	0.387	-0.027	0.158	0.00207	0.07	0.028	0.00044	0.259	0.029	0.112	0	0	0.1
18:40:00	0.023	0.00024	0.223	-0.03	0.084	0.00202	0.06	0.024	0.00019	0.158	0.024	0.061	0	0	0.1
18:45:00	0.022	0.00011	0.118	-0.032	0.042	0.002	0.05	0.022	0.00008	0.084	0.022	0.031	0	0	0.1
18:50:00	0.021	0.00005	0.06	-0.033	0.021	0.002	0.05	0.021	0.00004	0.045	0.021	0.016	0	0	0.1
18:55:00	0.02	0.00003	0.035	-0.034	0.012	0.00199	0.05	0.021	0.00002	0.03	0.021	0.01	0	0	0.1
19:00:00	0.02	0.00002	0.027	-0.034	0.009	0.00199	0.05	0.02	0.00002	0.025	0.021	0.009	0	0	0.1
19:05:00	0.02	0.00002	0.025	-0.034	0.009	0.00199	0.05	0.02	0.00002	0.024	0.02	0.008	0	0	0.1
19:10:00	0.02	0.00002	0.024	-0.034	0.008	0.00199	0.05	0.02	0.00002	0.022	0.02	0.008	0	0	0.1
19:15:00	0.02	0.00002	0.021	-0.034	0.007	0.00199	0.05	0.02	0.00002	0.019	0.02	0.007	0	0	0.1
19:20:00	0.02	0.00001	0.017	-0.034	0.006	0.00199	0.05	0.02	0.00001	0.015	0.02	0.005	0	0	0.1
19:25:00	0.02	0.00001	0.013	-0.034	0.004	0.00199	0.05	0.02	0.00001	0.01	0.02	0.004	0	0	0.1
19:30:00	0.02	0.00001	0.008	-0.034	0.003	0.00199	0.05	0.02	0	0.006	0.02	0.002	0	0	0.1
19:35:00	0.02	0	0.004	-0.034	0.001	0.00199	0.05	0.02	0	0.003	0.02	0.001	0	0	0.1
19:40:00	0.02	0	0.001	-0.034	0	0.00199	0.05	0.02	0	0.001	0.02	0	0	0	0.1
19:45:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
19:50:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
19:55:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:00:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:05:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:10:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:15:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:20:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:25:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:30:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:35:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:40:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:45:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:50:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
20:55:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:00:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1

21:05:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:10:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:15:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:20:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:25:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:30:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:35:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:40:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:45:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:50:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
21:55:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:00:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:05:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:10:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:15:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:20:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:25:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:30:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:35:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:40:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:45:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:50:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
22:55:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:00:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:05:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:10:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:15:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:20:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:25:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:30:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:35:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:40:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:45:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:50:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
23:55:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1
0:00:00	0.02	0	0	-0.034	0	0.00199	0.05	0.02	0	0	0.02	0	0	0	0.1





	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
1:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1

2:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
2:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
3:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
4:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
5:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1

6:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
6:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
7:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
8:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
8:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
8:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
8:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
8:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
8:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
8:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
8:35:00	0.044	-0.00017	0.036	1.174	-0.02	0.00207	0.09	0.025	0	0	1.205	0	0	0	0.1
8:40:00	0.081	-0.00062	0.04	1.211	-0.03	0.00006	0.16	0.032	-0.00012	0.051	1.212	-0.023	0	0	0.2
8:45:00	0.11	-0.00084	0.03	1.24	-0.026	0	0.22	0.06	-0.00036	0.043	1.24	-0.027	0	0	0.3
8:50:00	0.133	-0.00101	0.025	1.263	-0.024	0.00001	0.27	0.083	-0.00059	0.037	1.263	-0.028	0	0	0.5
8:55:00	0.151	-0.00088	0.017	1.281	-0.018	0	0.3	0.101	-0.00054	0.023	1.281	-0.019	0	0	0.6
9:00:00	0.165	-0.00082	0.013	1.295	-0.015	0	0.33	0.115	-0.00053	0.017	1.295	-0.015	0	0	0.7
9:05:00	0.144	0.00269	0.057	1.274	0.057	0.00008	0.29	0.096	0.00158	0.074	1.276	0.06	0	0	0.5
9:10:00	0.067	0.00156	0.15	1.197	0.1	0.00109	0.13	0.033	0.00043	0.172	1.213	0.079	0	0	0.1
9:15:00	0.025	-0.00001	0	1.155	0	0.00337	0.05	0.025	0	0.001	1.205	0.001	0	0	0.1
9:20:00	0.025	0	0.001	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
9:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
9:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
9:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1

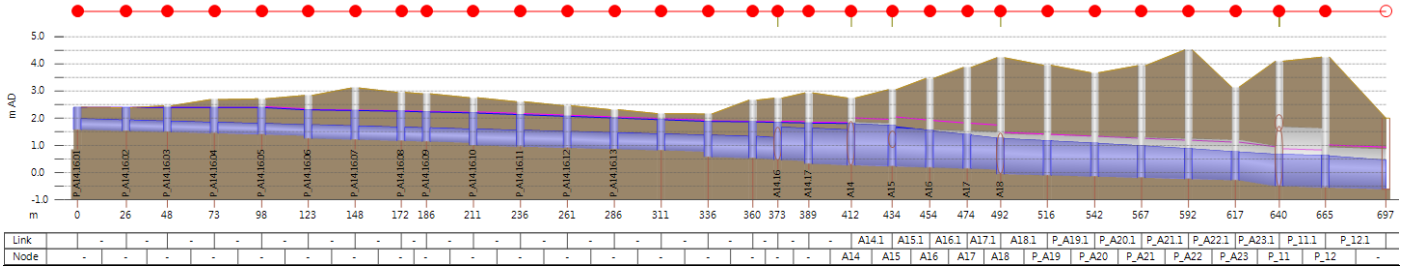
9:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
9:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
9:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
9:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
10:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
11:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
12:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1

13:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
13:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
14:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
15:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
16:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1

17:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
17:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
18:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
19:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
20:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1

20:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
21:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
22:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:05:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:10:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:15:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:20:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:25:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:30:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:35:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:40:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:45:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:50:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
23:55:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1
0:00:00	0.025	0	0	1.155	0	0.00335	0.05	0.025	0	0	1.205	0	0	0	0.1

TRAMO D



	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.075	0	0	-0.54	0	0.00199	0.05	0.075	0	0	-0.476	0	0	0	1
0:05:00	0.075	0	0	-0.54	0	0.00199	0.05	0.075	0	0	-0.476	0	0	0	1
0:10:00	0.075	0	0	-0.54	0	0.00199	0.05	0.075	0	0	-0.476	0	0	0	1
0:15:00	0.075	0	0	-0.54	0	0.00199	0.05	0.075	0	0	-0.476	0	0	0	1
0:20:00	0.08	0.00308	0.126	-0.535	0.087	0.00204	0.05	0.082	0.00367	0.144	-0.469	0.1	0	0	1.2
0:25:00	0.103	0.02117	0.491	-0.504	0.402	0.00232	0.08	0.113	0.02575	0.487	-0.428	0.423	0	0	1.8
0:30:00	0.154	0.08378	0.86	-0.422	0.874	0.00272	0.12	0.178	0.08989	0.697	-0.344	0.762	0	0	3.5
0:35:00	0.213	0.1707	0.926	-0.339	1.111	0.00277	0.16	0.238	0.17654	0.77	-0.264	0.978	0	0	5.4
0:40:00	0.253	0.24369	0.947	-0.284	1.241	0.00279	0.19	0.278	0.24744	0.795	-0.212	1.096	0	0	6.9
0:45:00	0.275	0.29021	0.955	-0.253	1.308	0.0028	0.2	0.301	0.29208	0.805	-0.182	1.156	0	0	7.7
0:50:00	0.284	0.31009	0.958	-0.24	1.334	0.0028	0.21	0.31	0.31073	0.808	-0.17	1.178	0	0	8
0:55:00	0.287	0.3162	0.959	-0.237	1.342	0.0028	0.21	0.313	0.31637	0.808	-0.167	1.185	0	0	8.1
1:00:00	0.287	0.31774	0.959	-0.236	1.344	0.0028	0.21	0.313	0.31778	0.809	-0.166	1.186	0	0	8.2
1:05:00	0.288	0.31993	0.959	-0.234	1.347	0.00281	0.21	0.314	0.32024	0.81	-0.164	1.19	0	0	8.2
1:10:00	0.293	0.3308	0.96	-0.228	1.36	0.00281	0.21	0.319	0.33169	0.813	-0.158	1.205	0	0	8.4
1:15:00	0.3	0.34796	0.962	-0.217	1.381	0.00282	0.22	0.327	0.34895	0.817	-0.147	1.226	0	0	8.7
1:20:00	0.307	0.3631	0.964	-0.209	1.398	0.00282	0.22	0.334	0.36378	0.819	-0.139	1.243	0	0	8.9
1:25:00	0.311	0.37249	0.965	-0.203	1.409	0.00283	0.23	0.338	0.37285	0.821	-0.134	1.253	0	0	9.1
1:30:00	0.312	0.37696	0.965	-0.201	1.414	0.00283	0.23	0.339	0.37711	0.821	-0.131	1.257	0	0	9.2
1:35:00	0.313	0.37862	0.965	-0.2	1.416	0.00283	0.23	0.34	0.37867	0.821	-0.13	1.259	0	0	9.2
1:40:00	0.313	0.37913	0.965	-0.199	1.416	0.00283	0.23	0.34	0.37914	0.821	-0.13	1.259	0	0	9.2
1:45:00	0.313	0.37925	0.965	-0.199	1.416	0.00283	0.23	0.34	0.37926	0.821	-0.13	1.259	0	0	9.2
1:50:00	0.313	0.37928	0.965	-0.199	1.416	0.00283	0.23	0.34	0.37928	0.821	-0.13	1.259	0	0	9.2
1:55:00	0.313	0.37929	0.965	-0.199	1.416	0.00283	0.23	0.34	0.37929	0.821	-0.13	1.259	0	0	9.2
2:00:00	0.313	0.37929	0.965	-0.199	1.416	0.00283	0.23	0.34	0.37929	0.821	-0.13	1.259	0	0	9.2
2:05:00	0.315	0.38245	0.966	-0.198	1.42	0.00283	0.23	0.342	0.38291	0.823	-0.128	1.264	0	0	9.3
2:10:00	0.321	0.39892	0.967	-0.188	1.438	0.00284	0.23	0.349	0.40016	0.827	-0.118	1.284	0	0	9.5
2:15:00	0.331	0.42367	0.969	-0.175	1.464	0.00285	0.24	0.359	0.42498	0.831	-0.105	1.31	0	0	9.9

2:20:00	0.339	0.44463	0.97	-0.164	1.485	0.00286	0.24	0.367	0.44551	0.833	-0.094	1.33	0	0	10.3
2:25:00	0.344	0.45699	0.971	-0.157	1.497	0.00286	0.25	0.372	0.45743	0.834	-0.088	1.341	0	0	10.5
2:30:00	0.346	0.46246	0.971	-0.154	1.502	0.00286	0.25	0.374	0.46263	0.835	-0.085	1.346	0	0	10.5
2:35:00	0.346	0.46438	0.972	-0.153	1.504	0.00286	0.25	0.374	0.46443	0.835	-0.084	1.347	0	0	10.6
2:40:00	0.347	0.46494	0.972	-0.153	1.504	0.00286	0.25	0.375	0.46495	0.835	-0.084	1.348	0	0	10.6
2:45:00	0.347	0.46508	0.972	-0.153	1.504	0.00286	0.25	0.375	0.46509	0.835	-0.084	1.348	0	0	10.6
2:50:00	0.347	0.46512	0.972	-0.153	1.504	0.00286	0.25	0.375	0.46512	0.835	-0.084	1.348	0	0	10.6
2:55:00	0.347	0.46512	0.972	-0.153	1.504	0.00286	0.25	0.375	0.46512	0.835	-0.084	1.348	0	0	10.6
3:00:00	0.347	0.46512	0.972	-0.153	1.504	0.00286	0.25	0.375	0.46512	0.835	-0.084	1.348	0	0	10.6
3:05:00	0.348	0.47	0.972	-0.15	1.509	0.00287	0.25	0.377	0.47067	0.836	-0.081	1.354	0	0	10.7
3:10:00	0.357	0.49446	0.973	-0.138	1.532	0.00288	0.26	0.386	0.49615	0.841	-0.068	1.379	0	0	11
3:15:00	0.37	0.52948	0.975	-0.121	1.563	0.00289	0.27	0.399	0.53117	0.845	-0.051	1.41	0	0	11.6
3:20:00	0.38	0.55759	0.976	-0.107	1.587	0.0029	0.27	0.409	0.55867	0.847	-0.038	1.433	0	0	12
3:25:00	0.385	0.57328	0.977	-0.1	1.6	0.0029	0.28	0.414	0.57378	0.848	-0.03	1.445	0	0	12.2
3:30:00	0.387	0.57987	0.977	-0.097	1.605	0.0029	0.28	0.416	0.58006	0.848	-0.028	1.449	0	0	12.3
3:35:00	0.388	0.58209	0.977	-0.096	1.607	0.0029	0.28	0.417	0.58214	0.848	-0.027	1.451	0	0	12.3
3:40:00	0.388	0.58271	0.977	-0.095	1.607	0.0029	0.28	0.417	0.58273	0.848	-0.026	1.451	0	0	12.3
3:45:00	0.388	0.58287	0.977	-0.095	1.608	0.0029	0.28	0.417	0.58287	0.848	-0.026	1.451	0	0	12.3
3:50:00	0.388	0.5829	0.977	-0.095	1.608	0.0029	0.28	0.417	0.5829	0.848	-0.026	1.451	0	0	12.3
3:55:00	0.388	0.5829	0.977	-0.095	1.608	0.0029	0.28	0.417	0.5829	0.848	-0.026	1.451	0	0	12.3
4:00:00	0.388	0.58291	0.977	-0.095	1.608	0.0029	0.28	0.417	0.58291	0.848	-0.026	1.451	0	0	12.3
4:05:00	0.391	0.59215	0.978	-0.091	1.615	0.00291	0.28	0.421	0.59327	0.85	-0.021	1.461	0	0	12.5
4:10:00	0.405	0.63339	0.979	-0.072	1.647	0.00293	0.29	0.435	0.63593	0.855	-0.002	1.496	0	0	13.1
4:15:00	0.422	0.68809	0.981	-0.048	1.688	0.00295	0.3	0.453	0.69048	0.859	0.022	1.536	0	0	13.8
4:20:00	0.435	0.72963	0.982	-0.03	1.718	0.00296	0.31	0.466	0.73106	0.86	0.039	1.564	0	0	14.4
4:25:00	0.441	0.75153	0.982	-0.021	1.733	0.00296	0.31	0.472	0.75216	0.861	0.048	1.577	0	0	14.7
4:30:00	0.444	0.76019	0.982	-0.017	1.739	0.00297	0.32	0.475	0.76041	0.861	0.052	1.582	0	0	14.8
4:35:00	0.445	0.76297	0.982	-0.016	1.74	0.00297	0.32	0.476	0.76303	0.861	0.053	1.584	0	0	14.9
4:40:00	0.445	0.76372	0.982	-0.016	1.741	0.00297	0.32	0.476	0.76374	0.861	0.053	1.584	0	0	14.9
4:45:00	0.445	0.76391	0.982	-0.016	1.741	0.00297	0.32	0.476	0.76391	0.861	0.053	1.584	0	0	14.9
4:50:00	0.445	0.76395	0.982	-0.016	1.741	0.00297	0.32	0.476	0.76395	0.861	0.053	1.584	0	0	14.9
4:55:00	0.445	0.76396	0.982	-0.016	1.741	0.00297	0.32	0.476	0.76396	0.861	0.053	1.584	0	0	14.9
5:00:00	0.445	0.76396	0.982	-0.016	1.741	0.00297	0.32	0.476	0.76396	0.861	0.053	1.584	0	0	14.9
5:05:00	0.45	0.78202	0.983	-0.008	1.753	0.00298	0.32	0.482	0.78396	0.864	0.061	1.6	0	0	15.1
5:10:00	0.471	0.85462	0.984	0.021	1.8	0.003	0.34	0.504	0.85854	0.869	0.091	1.649	0	0	16.1
5:15:00	0.495	0.94272	0.986	0.055	1.854	0.00303	0.35	0.529	0.94608	0.872	0.125	1.7	0	0	17.2
5:20:00	0.511	1.00486	0.987	0.078	1.889	0.00305	0.36	0.546	1.00673	0.872	0.148	1.733	0	0	17.9
5:25:00	0.519	1.03572	0.987	0.09	1.907	0.00306	0.37	0.554	1.0365	0.873	0.159	1.749	0	0	18.3
5:30:00	0.522	1.04742	0.987	0.094	1.913	0.00307	0.37	0.557	1.04768	0.873	0.163	1.754	0	0	18.5
5:35:00	0.523	1.05106	0.987	0.095	1.915	0.00307	0.37	0.558	1.05113	0.873	0.164	1.756	0	0	18.5
5:40:00	0.524	1.05204	0.987	0.096	1.916	0.00307	0.37	0.558	1.05206	0.873	0.164	1.756	0	0	18.5
5:45:00	0.524	1.05227	0.987	0.096	1.916	0.00307	0.37	0.558	1.05228	0.873	0.164	1.756	0	0	18.5
5:50:00	0.524	1.05233	0.987	0.096	1.916	0.00307	0.37	0.558	1.05233	0.873	0.165	1.756	0	0	18.5
5:55:00	0.524	1.05234	0.987	0.096	1.916	0.00307	0.37	0.558	1.05234	0.873	0.165	1.756	0	0	18.5
6:00:00	0.524	1.05234	0.987	0.096	1.916	0.00307	0.37	0.558	1.05234	0.873	0.165	1.756	0	0	18.5

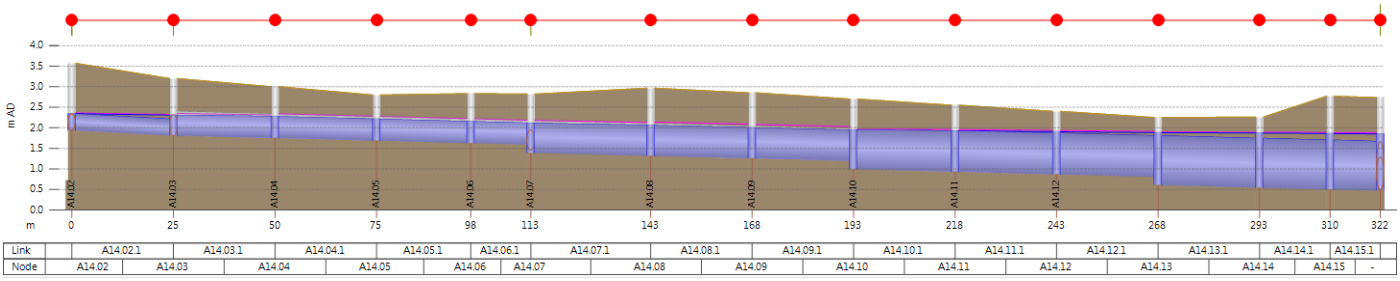
6:05:00	0.534	1.09311	0.988	0.11	1.938	0.00309	0.38	0.569	1.09681	0.876	0.18	1.783	0	0	19
6:10:00	0.568	1.23397	0.989	0.159	2.011	0.00314	0.4	0.605	1.24032	0.88	0.23	1.857	0	0	20.7
6:15:00	0.604	1.38731	0.99	0.21	2.085	0.0032	0.43	0.642	1.3923	0.882	0.281	1.927	0	0	22.4
6:20:00	0.626	1.48913	0.991	0.243	2.132	0.00324	0.44	0.666	1.49174	0.881	0.312	1.968	0	0	23.5
6:25:00	0.636	1.53639	0.991	0.258	2.153	0.00325	0.45	0.677	1.5374	0.881	0.327	1.987	0	0	24
6:30:00	0.64	1.55317	0.991	0.263	2.161	0.00326	0.45	0.681	1.55348	0.881	0.332	1.993	0	0	24.1
6:35:00	0.641	1.55808	0.991	0.264	2.163	0.00326	0.45	0.682	1.55816	0.881	0.333	1.995	0	0	24.2
6:40:00	0.641	1.55935	0.991	0.265	2.163	0.00326	0.45	0.682	1.55937	0.881	0.334	1.995	0	0	24.2
6:45:00	0.641	1.55965	0.991	0.265	2.164	0.00326	0.45	0.682	1.55965	0.881	0.334	1.995	0	0	24.2
6:50:00	0.641	1.55972	0.991	0.265	2.164	0.00326	0.45	0.682	1.55972	0.881	0.334	1.995	0	0	24.2
6:55:00	0.641	1.55974	0.991	0.265	2.164	0.00326	0.45	0.682	1.55974	0.881	0.334	1.995	0	0	24.2
7:00:00	0.641	1.55974	0.991	0.265	2.164	0.00326	0.45	0.682	1.55974	0.881	0.334	1.995	0	0	24.2
7:05:00	0.665	1.67333	0.992	0.299	2.213	0.00332	0.47	0.708	1.68149	0.885	0.371	2.051	0	0	25.4
7:10:00	0.72	1.94808	0.993	0.38	2.325	0.00343	0.51	0.766	1.95664	0.885	0.452	2.156	0	0	28.1
7:15:00	0.76	2.16571	0.994	0.441	2.409	0.00353	0.54	0.81	2.17105	0.883	0.512	2.231	0	0	30.2
7:20:00	0.782	2.28553	0.994	0.474	2.454	0.00359	0.56	0.833	2.28796	0.881	0.545	2.27	0	0	31.2
7:25:00	0.791	2.33661	0.994	0.488	2.473	0.00361	0.56	0.843	2.33753	0.881	0.558	2.286	0	0	31.7
7:30:00	0.794	2.35548	0.994	0.493	2.48	0.00362	0.56	0.847	2.35581	0.88	0.563	2.292	0	0	31.9
7:35:00	0.795	2.36209	0.994	0.494	2.482	0.00362	0.57	0.848	2.36221	0.88	0.565	2.294	0	0	31.9
7:40:00	0.796	2.36453	0.994	0.495	2.483	0.00362	0.57	0.848	2.36458	0.88	0.566	2.294	0	0	31.9
7:45:00	0.796	2.36557	0.994	0.495	2.484	0.00362	0.57	0.849	2.36559	0.88	0.566	2.295	0	0	31.9
7:50:00	0.796	2.36609	0.994	0.495	2.484	0.00362	0.57	0.849	2.3661	0.88	0.566	2.295	0	0	31.9
7:55:00	0.796	2.36638	0.994	0.496	2.484	0.00362	0.57	0.849	2.36638	0.88	0.566	2.295	0	0	32
8:00:00	0.796	2.36655	0.994	0.496	2.484	0.00362	0.57	0.849	2.36656	0.88	0.566	2.295	0	0	32
8:05:00	0.852	2.69526	0.995	0.582	2.602	0.00381	0.61	0.911	2.71211	0.881	0.657	2.416	0	0	34.8
8:10:00	0.949	3.31989	0.996	0.738	2.816	0.0042	0.68	1.02	3.33334	0.87	0.815	2.604	0	0	39.6
8:15:00	1.011	3.75463	0.996	0.844	2.962	0.00451	0.73	1.092	3.76178	0.857	0.921	2.728	0	0	42.6
8:20:00	1.04	3.96668	0.997	0.894	3.034	0.00469	0.75	1.127	3.96971	0.85	0.972	2.788	0	0	44
8:25:00	1.052	4.06053	0.997	0.916	3.066	0.00477	0.76	1.142	4.06176	0.846	0.994	2.814	0	0	44.6
8:30:00	1.058	4.10375	0.997	0.927	3.08	0.00481	0.77	1.149	4.10438	0.844	1.005	2.826	0	0	44.8
8:35:00	1.061	4.12398	0.997	0.931	3.087	0.00483	0.77	1.152	4.12427	0.843	1.01	2.832	0	0	44.9
8:40:00	1.062	4.13503	0.997	0.934	3.091	0.00484	0.77	1.154	4.1352	0.843	1.012	2.835	0	0	45
8:45:00	1.063	4.14138	0.997	0.936	3.093	0.00485	0.77	1.155	4.14148	0.843	1.014	2.837	0	0	45
8:50:00	1.063	4.14535	0.997	0.936	3.095	0.00485	0.77	1.155	4.14541	0.842	1.015	2.838	0	0	45.1
8:55:00	1.064	4.14804	0.997	0.937	3.096	0.00485	0.77	1.156	4.14809	0.842	1.016	2.839	0	0	45.1
9:00:00	1.064	4.15002	0.997	0.938	3.096	0.00485	0.77	1.156	4.15006	0.842	1.016	2.84	0	0	45.1
9:05:00	1.037	3.94176	0.997	0.888	3.026	0.00466	0.75	1.123	3.93504	0.849	0.964	2.774	0	0	43.8
9:10:00	0.992	3.61352	0.996	0.81	2.915	0.00439	0.71	1.069	3.60648	0.858	0.883	2.677	0	0	41.6
9:15:00	0.957	3.37374	0.996	0.752	2.834	0.00422	0.69	1.029	3.36924	0.864	0.824	2.608	0	0	40
9:20:00	0.938	3.24085	0.996	0.719	2.789	0.00413	0.67	1.006	3.23843	0.868	0.792	2.569	0	0	39
9:25:00	0.927	3.17239	0.996	0.702	2.766	0.00409	0.66	0.995	3.17114	0.869	0.775	2.549	0	0	38.5
9:30:00	0.922	3.13739	0.996	0.694	2.754	0.00406	0.66	0.989	3.13675	0.87	0.766	2.539	0	0	38.2
9:35:00	0.919	3.11919	0.996	0.689	2.748	0.00405	0.66	0.985	3.11886	0.87	0.762	2.534	0	0	38.1
9:40:00	0.918	3.11017	0.996	0.687	2.745	0.00405	0.66	0.984	3.11	0.871	0.759	2.531	0	0	38
9:45:00	0.917	3.10531	0.996	0.686	2.743	0.00404	0.66	0.983	3.10521	0.871	0.758	2.53	0	0	38

9:50:00	0.917	3.10219	0.996	0.685	2.742	0.00404	0.65	0.982	3.10212	0.871	0.757	2.529	0	0	38
9:55:00	0.916	3.10003	0.996	0.684	2.741	0.00404	0.65	0.982	3.09998	0.871	0.757	2.528	0	0	37.9
10:00:00	0.916	3.09848	0.996	0.684	2.741	0.00404	0.65	0.982	3.09844	0.871	0.757	2.528	0	0	37.9
10:05:00	0.888	2.91859	0.995	0.639	2.679	0.00392	0.63	0.95	2.91057	0.872	0.709	2.466	0	0	36.5
10:10:00	0.831	2.568	0.995	0.549	2.557	0.00372	0.59	0.886	2.55776	0.875	0.618	2.353	0	0	33.7
10:15:00	0.777	2.26079	0.994	0.467	2.445	0.00357	0.55	0.828	2.2532	0.878	0.536	2.252	0	0	31
10:20:00	0.744	2.07876	0.993	0.417	2.376	0.00348	0.53	0.792	2.07475	0.88	0.486	2.191	0	0	29.3
10:25:00	0.728	1.99387	0.993	0.393	2.343	0.00344	0.52	0.775	1.99213	0.881	0.462	2.163	0	0	28.5
10:30:00	0.722	1.95892	0.993	0.383	2.329	0.00343	0.51	0.768	1.95821	0.882	0.453	2.151	0	0	28.2
10:35:00	0.719	1.9446	0.993	0.379	2.324	0.00342	0.51	0.765	1.94429	0.882	0.449	2.146	0	0	28.1
10:40:00	0.718	1.93848	0.993	0.377	2.321	0.00342	0.51	0.764	1.93834	0.882	0.447	2.144	0	0	28
10:45:00	0.717	1.93575	0.993	0.377	2.32	0.00342	0.51	0.763	1.93569	0.882	0.446	2.143	0	0	28
10:50:00	0.717	1.93445	0.993	0.376	2.32	0.00342	0.51	0.763	1.93441	0.882	0.446	2.143	0	0	28
10:55:00	0.717	1.9338	0.993	0.376	2.319	0.00342	0.51	0.763	1.93379	0.882	0.446	2.142	0	0	28
11:00:00	0.717	1.93348	0.993	0.376	2.319	0.00342	0.51	0.763	1.93348	0.882	0.446	2.142	0	0	28
11:05:00	0.704	1.86784	0.993	0.357	2.293	0.00339	0.5	0.749	1.86379	0.88	0.426	2.114	0	0	27.3
11:10:00	0.669	1.69536	0.992	0.306	2.222	0.00331	0.47	0.712	1.68833	0.878	0.374	2.043	0	0	25.6
11:15:00	0.628	1.49969	0.991	0.246	2.137	0.00323	0.45	0.668	1.49337	0.877	0.313	1.962	0	0	23.6
11:20:00	0.599	1.36521	0.99	0.203	2.075	0.00318	0.42	0.637	1.3616	0.877	0.271	1.906	0	0	22.1
11:25:00	0.584	1.30086	0.99	0.182	2.044	0.00316	0.41	0.621	1.29937	0.877	0.25	1.879	0	0	21.4
11:30:00	0.578	1.27708	0.989	0.174	2.033	0.00315	0.41	0.616	1.27659	0.877	0.243	1.869	0	0	21.1
11:35:00	0.577	1.26981	0.989	0.171	2.029	0.00315	0.41	0.614	1.26967	0.877	0.24	1.866	0	0	21.1
11:40:00	0.576	1.26787	0.989	0.171	2.028	0.00315	0.41	0.613	1.26784	0.877	0.24	1.865	0	0	21
11:45:00	0.576	1.26749	0.989	0.171	2.028	0.00315	0.41	0.613	1.26739	0.877	0.24	1.865	0	0	21
11:50:00	0.576	1.26729	0.989	0.171	2.028	0.00315	0.41	0.613	1.26729	0.877	0.239	1.865	0	0	21
11:55:00	0.576	1.26727	0.989	0.171	2.028	0.00315	0.41	0.613	1.26727	0.877	0.239	1.865	0	0	21
12:00:00	0.576	1.26726	0.989	0.171	2.028	0.00315	0.41	0.613	1.26726	0.877	0.239	1.865	0	0	21
12:05:00	0.569	1.23603	0.989	0.16	2.012	0.00313	0.4	0.605	1.23348	0.875	0.228	1.846	0	0	20.7
12:10:00	0.545	1.13884	0.988	0.127	1.962	0.00309	0.39	0.581	1.13438	0.872	0.194	1.795	0	0	19.5
12:15:00	0.518	1.03025	0.987	0.088	1.904	0.00305	0.37	0.552	1.02625	0.869	0.155	1.738	0	0	18.3
12:20:00	0.498	0.95324	0.986	0.059	1.86	0.00303	0.35	0.531	0.95085	0.868	0.127	1.698	0	0	17.3
12:25:00	0.487	0.91435	0.985	0.044	1.837	0.00302	0.35	0.52	0.91325	0.867	0.113	1.677	0	0	16.8
12:30:00	0.483	0.89914	0.985	0.038	1.827	0.00301	0.34	0.516	0.89878	0.867	0.107	1.669	0	0	16.6
12:35:00	0.482	0.89435	0.985	0.037	1.825	0.00301	0.34	0.515	0.89425	0.867	0.105	1.667	0	0	16.6
12:40:00	0.482	0.89305	0.985	0.036	1.824	0.00301	0.34	0.514	0.89302	0.867	0.105	1.666	0	0	16.5
12:45:00	0.481	0.89273	0.985	0.036	1.824	0.00301	0.34	0.514	0.89272	0.867	0.105	1.666	0	0	16.5
12:50:00	0.481	0.89266	0.985	0.036	1.824	0.00301	0.34	0.514	0.89266	0.867	0.105	1.666	0	0	16.5
12:55:00	0.481	0.89264	0.985	0.036	1.824	0.00301	0.34	0.514	0.89264	0.867	0.105	1.666	0	0	16.5
13:00:00	0.481	0.89264	0.985	0.036	1.824	0.00301	0.34	0.514	0.89264	0.867	0.105	1.666	0	0	16.5
13:05:00	0.477	0.87762	0.985	0.03	1.814	0.003	0.34	0.51	0.87614	0.865	0.098	1.654	0	0	16.4
13:10:00	0.462	0.82309	0.984	0.008	1.78	0.00298	0.33	0.494	0.82018	0.862	0.076	1.618	0	0	15.6
13:15:00	0.443	0.75695	0.982	-0.019	1.736	0.00296	0.32	0.474	0.75418	0.858	0.049	1.575	0	0	14.8
13:20:00	0.428	0.70752	0.981	-0.039	1.702	0.00294	0.31	0.459	0.70579	0.856	0.029	1.542	0	0	14.1
13:25:00	0.42	0.68105	0.98	-0.051	1.683	0.00294	0.3	0.45	0.68026	0.855	0.018	1.525	0	0	13.7
13:30:00	0.416	0.67025	0.98	-0.056	1.675	0.00293	0.3	0.447	0.66996	0.855	0.013	1.518	0	0	13.6

13:35:00	0.415	0.66668	0.98	-0.057	1.672	0.00293	0.3	0.446	0.66659	0.855	0.012	1.516	0	0	13.5
13:40:00	0.415	0.66567	0.98	-0.058	1.672	0.00293	0.3	0.445	0.66565	0.855	0.011	1.515	0	0	13.5
13:45:00	0.415	0.66543	0.98	-0.058	1.671	0.00293	0.3	0.445	0.66542	0.855	0.011	1.515	0	0	13.5
13:50:00	0.415	0.66537	0.98	-0.058	1.671	0.00293	0.3	0.445	0.66537	0.855	0.011	1.515	0	0	13.5
13:55:00	0.415	0.66537	0.98	-0.058	1.671	0.00293	0.3	0.445	0.66536	0.855	0.011	1.515	0	0	13.5
14:00:00	0.415	0.66536	0.98	-0.058	1.671	0.00293	0.3	0.445	0.66536	0.855	0.011	1.515	0	0	13.5
14:05:00	0.412	0.65762	0.98	-0.061	1.666	0.00293	0.3	0.443	0.65672	0.853	0.007	1.508	0	0	13.4
14:10:00	0.402	0.62548	0.979	-0.076	1.641	0.00291	0.29	0.432	0.62353	0.849	-0.007	1.481	0	0	13
14:15:00	0.388	0.5834	0.977	-0.095	1.608	0.0029	0.28	0.417	0.58145	0.846	-0.027	1.448	0	0	12.4
14:20:00	0.377	0.55018	0.976	-0.111	1.58	0.00289	0.27	0.406	0.54881	0.843	-0.042	1.421	0	0	11.9
14:25:00	0.37	0.53131	0.975	-0.12	1.564	0.00288	0.27	0.399	0.53069	0.842	-0.051	1.407	0	0	11.6
14:30:00	0.368	0.52324	0.975	-0.124	1.557	0.00288	0.26	0.396	0.523	0.842	-0.055	1.4	0	0	11.5
14:35:00	0.367	0.52046	0.974	-0.125	1.555	0.00288	0.26	0.395	0.52038	0.842	-0.056	1.398	0	0	11.4
14:40:00	0.366	0.51966	0.974	-0.125	1.554	0.00288	0.26	0.395	0.51964	0.842	-0.056	1.398	0	0	11.4
14:45:00	0.366	0.51945	0.974	-0.126	1.554	0.00288	0.26	0.395	0.51945	0.842	-0.056	1.398	0	0	11.4
14:50:00	0.366	0.51941	0.974	-0.126	1.554	0.00288	0.26	0.395	0.51941	0.842	-0.056	1.398	0	0	11.4
14:55:00	0.366	0.51941	0.974	-0.126	1.554	0.00288	0.26	0.395	0.51941	0.842	-0.056	1.398	0	0	11.4
15:00:00	0.366	0.51941	0.974	-0.126	1.554	0.00288	0.26	0.395	0.51941	0.842	-0.056	1.398	0	0	11.4
15:05:00	0.365	0.51498	0.974	-0.128	1.55	0.00288	0.26	0.393	0.51441	0.84	-0.059	1.392	0	0	11.3
15:10:00	0.357	0.49459	0.973	-0.138	1.532	0.00287	0.26	0.386	0.49322	0.837	-0.069	1.372	0	0	11
15:15:00	0.347	0.46622	0.972	-0.152	1.505	0.00286	0.25	0.375	0.46479	0.833	-0.084	1.345	0	0	10.6
15:20:00	0.338	0.44278	0.97	-0.165	1.483	0.00285	0.24	0.366	0.44179	0.83	-0.096	1.324	0	0	10.2
15:25:00	0.333	0.42887	0.969	-0.172	1.469	0.00285	0.24	0.361	0.42836	0.829	-0.103	1.311	0	0	10
15:30:00	0.331	0.42256	0.969	-0.175	1.462	0.00284	0.24	0.358	0.42236	0.828	-0.106	1.305	0	0	9.9
15:35:00	0.33	0.42028	0.969	-0.177	1.46	0.00284	0.24	0.357	0.42022	0.828	-0.107	1.303	0	0	9.9
15:40:00	0.329	0.41968	0.969	-0.177	1.459	0.00284	0.24	0.357	0.41958	0.828	-0.108	1.303	0	0	9.9
15:45:00	0.329	0.41942	0.969	-0.177	1.459	0.00284	0.24	0.357	0.41941	0.828	-0.108	1.302	0	0	9.9
15:50:00	0.329	0.41938	0.969	-0.177	1.459	0.00284	0.24	0.357	0.41938	0.828	-0.108	1.302	0	0	9.9
15:55:00	0.329	0.41937	0.969	-0.177	1.459	0.00284	0.24	0.357	0.41937	0.828	-0.108	1.302	0	0	9.9
16:00:00	0.329	0.41937	0.969	-0.177	1.459	0.00284	0.24	0.357	0.41937	0.828	-0.108	1.302	0	0	9.9
16:05:00	0.328	0.41685	0.968	-0.179	1.457	0.00284	0.24	0.356	0.41648	0.827	-0.109	1.299	0	0	9.8
16:10:00	0.323	0.40371	0.967	-0.186	1.443	0.00283	0.23	0.35	0.40274	0.824	-0.117	1.283	0	0	9.6
16:15:00	0.315	0.38432	0.966	-0.197	1.422	0.00283	0.23	0.342	0.38326	0.821	-0.127	1.262	0	0	9.3
16:20:00	0.309	0.36762	0.964	-0.206	1.403	0.00282	0.22	0.335	0.36686	0.818	-0.137	1.244	0	0	9
16:25:00	0.304	0.35724	0.963	-0.212	1.391	0.00282	0.22	0.331	0.35683	0.816	-0.143	1.233	0	0	8.8
16:30:00	0.302	0.35226	0.963	-0.215	1.386	0.00282	0.22	0.329	0.35208	0.816	-0.145	1.228	0	0	8.8
16:35:00	0.301	0.35035	0.963	-0.216	1.383	0.00282	0.22	0.328	0.35029	0.816	-0.146	1.226	0	0	8.7
16:40:00	0.301	0.34975	0.963	-0.216	1.383	0.00282	0.22	0.328	0.34973	0.816	-0.147	1.225	0	0	8.7
16:45:00	0.301	0.34959	0.962	-0.217	1.383	0.00282	0.22	0.328	0.34958	0.816	-0.147	1.225	0	0	8.7
16:50:00	0.301	0.34955	0.962	-0.217	1.382	0.00282	0.22	0.328	0.34955	0.816	-0.147	1.225	0	0	8.7
16:55:00	0.301	0.34954	0.962	-0.217	1.382	0.00282	0.22	0.328	0.34954	0.816	-0.147	1.225	0	0	8.7
17:00:00	0.301	0.34954	0.962	-0.217	1.382	0.00282	0.22	0.328	0.34954	0.816	-0.147	1.225	0	0	8.7
17:05:00	0.3	0.34781	0.962	-0.218	1.38	0.00281	0.22	0.327	0.34754	0.815	-0.148	1.222	0	0	8.7
17:10:00	0.296	0.33841	0.961	-0.223	1.369	0.00281	0.22	0.323	0.33766	0.812	-0.154	1.21	0	0	8.5
17:15:00	0.29	0.32395	0.96	-0.232	1.352	0.0028	0.21	0.316	0.32311	0.808	-0.162	1.192	0	0	8.3

17:20:00	0.284	0.31107	0.958	-0.24	1.335	0.0028	0.21	0.31	0.31044	0.806	-0.17	1.176	0	0	8.1
17:25:00	0.281	0.30272	0.957	-0.245	1.324	0.0028	0.2	0.306	0.30236	0.804	-0.175	1.166	0	0	7.9
17:30:00	0.279	0.29856	0.956	-0.248	1.319	0.00279	0.2	0.305	0.29841	0.803	-0.178	1.161	0	0	7.8
17:35:00	0.278	0.29693	0.956	-0.249	1.317	0.00279	0.2	0.304	0.29688	0.803	-0.179	1.159	0	0	7.8
17:40:00	0.278	0.29641	0.956	-0.249	1.316	0.00279	0.2	0.304	0.29639	0.803	-0.179	1.158	0	0	7.8
17:45:00	0.278	0.29627	0.956	-0.249	1.316	0.00279	0.2	0.303	0.29626	0.803	-0.179	1.158	0	0	7.8
17:50:00	0.278	0.29624	0.956	-0.249	1.316	0.00279	0.2	0.303	0.29624	0.803	-0.179	1.158	0	0	7.8
17:55:00	0.278	0.29623	0.956	-0.249	1.316	0.00279	0.2	0.303	0.29623	0.803	-0.179	1.158	0	0	7.8
18:00:00	0.278	0.29622	0.956	-0.249	1.316	0.00279	0.2	0.303	0.29622	0.803	-0.179	1.158	0	0	7.8
18:05:00	0.274	0.28842	0.955	-0.254	1.305	0.00278	0.2	0.3	0.28711	0.798	-0.185	1.144	0	0	7.7
18:10:00	0.253	0.24433	0.947	-0.284	1.242	0.00275	0.18	0.277	0.24049	0.778	-0.215	1.07	0	0	6.8
18:15:00	0.217	0.17727	0.929	-0.334	1.124	0.0027	0.16	0.24	0.17272	0.743	-0.265	0.947	0	0	5.5
18:20:00	0.179	0.11668	0.895	-0.387	0.98	0.00265	0.13	0.2	0.11258	0.694	-0.318	0.804	0	0	4.2
18:25:00	0.145	0.07236	0.84	-0.435	0.827	0.00259	0.11	0.164	0.0692	0.627	-0.365	0.658	0	0	3.2
18:30:00	0.124	0.04299	0.68	-0.471	0.618	0.00237	0.09	0.136	0.0409	0.538	-0.401	0.513	0	0	2.5
18:35:00	0.107	0.02534	0.535	-0.497	0.451	0.00222	0.08	0.115	0.02385	0.442	-0.429	0.386	0	0	1.9
18:40:00	0.095	0.01414	0.393	-0.515	0.303	0.0021	0.07	0.098	0.01311	0.336	-0.449	0.266	0	0	1.6
18:45:00	0.087	0.00762	0.261	-0.527	0.189	0.00204	0.06	0.088	0.00704	0.23	-0.461	0.169	0	0	1.3
18:50:00	0.082	0.00429	0.167	-0.532	0.117	0.00202	0.06	0.083	0.00397	0.15	-0.468	0.106	0	0	1.2
18:55:00	0.079	0.00259	0.109	-0.535	0.074	0.00201	0.05	0.08	0.00242	0.1	-0.471	0.069	0	0	1.1
19:00:00	0.078	0.00174	0.076	-0.537	0.051	0.002	0.05	0.078	0.00166	0.071	-0.473	0.049	0	0	1.1
19:05:00	0.077	0.00132	0.059	-0.538	0.04	0.002	0.05	0.078	0.00128	0.056	-0.473	0.038	0	0	1.1
19:10:00	0.077	0.00108	0.049	-0.538	0.033	0.002	0.05	0.077	0.00106	0.047	-0.474	0.032	0	0	1.1
19:15:00	0.077	0.00091	0.041	-0.538	0.028	0.002	0.05	0.077	0.00088	0.04	-0.474	0.027	0	0	1.1
19:20:00	0.076	0.00076	0.035	-0.539	0.023	0.002	0.05	0.077	0.00074	0.034	-0.474	0.023	0	0	1.1
19:25:00	0.076	0.00063	0.029	-0.539	0.019	0.002	0.05	0.076	0.00061	0.028	-0.475	0.019	0	0	1
19:30:00	0.076	0.00051	0.024	-0.539	0.016	0.00199	0.05	0.076	0.00051	0.023	-0.475	0.015	0	0	1
19:35:00	0.076	0.00042	0.02	-0.539	0.013	0.00199	0.05	0.076	0.00041	0.019	-0.475	0.013	0	0	1
19:40:00	0.076	0.00036	0.017	-0.539	0.011	0.00199	0.05	0.076	0.00035	0.016	-0.475	0.011	0	0	1
19:45:00	0.076	0.00031	0.014	-0.539	0.01	0.00199	0.05	0.076	0.00031	0.014	-0.475	0.009	0	0	1
19:50:00	0.075	0.00026	0.012	-0.54	0.008	0.00199	0.05	0.076	0.00026	0.012	-0.475	0.008	0	0	1
19:55:00	0.075	0.00024	0.011	-0.54	0.007	0.00199	0.05	0.075	0.00024	0.011	-0.476	0.007	0	0	1
20:00:00	0.075	0.00022	0.01	-0.54	0.007	0.00199	0.05	0.075	0.00022	0.01	-0.476	0.007	0	0	1
20:05:00	0.075	0.00022	0.009	-0.54	0.006	0.00199	0.05	0.075	0.00022	0.009	-0.476	0.006	0	0	1
20:10:00	0.075	0.00019	0.009	-0.54	0.006	0.00199	0.05	0.075	0.00018	0.009	-0.476	0.006	0	0	1
20:15:00	0.075	0.00017	0.008	-0.54	0.005	0.00199	0.05	0.075	0.00017	0.008	-0.476	0.005	0	0	1
20:20:00	0.075	0.00016	0.008	-0.54	0.005	0.00199	0.05	0.075	0.00016	0.007	-0.476	0.005	0	0	1
20:25:00	0.075	0.00015	0.007	-0.54	0.005	0.00199	0.05	0.075	0.00015	0.007	-0.476	0.005	0	0	1
20:30:00	0.075	0.00015	0.007	-0.54	0.004	0.00199	0.05	0.075	0.00014	0.006	-0.476	0.004	0	0	1
20:35:00	0.075	0.00013	0.006	-0.54	0.004	0.00199	0.05	0.075	0.00013	0.006	-0.476	0.004	0	0	1
20:40:00	0.075	0.00012	0.006	-0.54	0.004	0.00199	0.05	0.075	0.00012	0.006	-0.476	0.004	0	0	1
20:45:00	0.075	0.00012	0.006	-0.54	0.004	0.00199	0.05	0.075	0.00012	0.006	-0.476	0.004	0	0	1
20:50:00	0.075	0.00011	0.005	-0.54	0.004	0.00199	0.05	0.075	0.00011	0.005	-0.476	0.003	0	0	1
20:55:00	0.075	0.00011	0.005	-0.54	0.003	0.00199	0.05	0.075	0.00011	0.005	-0.476	0.003	0	0	1

21:0															
5:00	0.075	0.0001	0.005	-0.54	0.003	0.00199	0.05	0.075	0.0001	0.005	-0.476	0.003	0	0	1
21:1															
0:00	0.075	0.0001	0.005	-0.54	0.003	0.00199	0.05	0.075	0.0001	0.005	-0.476	0.003	0	0	1
21:1															
5:00	0.075	0.0001	0.005	-0.54	0.003	0.00199	0.05	0.075	0.0001	0.005	-0.476	0.003	0	0	1
21:2		0.0000							0.0000						
0:00	0.075	9	0.004	-0.54	0.003	0.00199	0.05	0.075	9	0.004	-0.476	0.003	0	0	1
21:2		0.0000							0.0000						
5:00	0.075	9	0.004	-0.54	0.003	0.00199	0.05	0.075	9	0.004	-0.476	0.003	0	0	1
21:3		0.0000							0.0000						
0:00	0.075	9	0.004	-0.54	0.003	0.00199	0.05	0.075	9	0.004	-0.476	0.003	0	0	1
21:3		0.0000							0.0000						
5:00	0.075	8	0.004	-0.54	0.003	0.00199	0.05	0.075	8	0.004	-0.476	0.003	0	0	1
21:4		0.0000							0.0000						
0:00	0.075	8	0.004	-0.54	0.003	0.00199	0.05	0.075	8	0.004	-0.476	0.003	0	0	1
21:4		0.0000							0.0000						
5:00	0.075	8	0.004	-0.54	0.003	0.00199	0.05	0.075	8	0.004	-0.476	0.003	0	0	1
21:5		0.0000							0.0000						
0:00	0.075	8	0.004	-0.54	0.002	0.00199	0.05	0.075	8	0.004	-0.476	0.002	0	0	1
21:5		0.0000							0.0000						
5:00	0.075	7	0.003	-0.54	0.002	0.00199	0.05	0.075	7	0.003	-0.476	0.002	0	0	1
22:0		0.0000							0.0000						
0:00	0.075	7	0.003	-0.54	0.002	0.00199	0.05	0.075	7	0.003	-0.476	0.002	0	0	1
22:0		0.0000							0.0000						
5:00	0.075	7	0.003	-0.54	0.002	0.00199	0.05	0.075	7	0.003	-0.476	0.002	0	0	1
22:1		0.0000							0.0000						
0:00	0.075	7	0.003	-0.54	0.002	0.00199	0.05	0.075	7	0.003	-0.476	0.002	0	0	1
22:1		0.0000							0.0000						
5:00	0.075	7	0.003	-0.54	0.002	0.00199	0.05	0.075	7	0.003	-0.476	0.002	0	0	1
22:2		0.0000							0.0000						
0:00	0.075	6	0.003	-0.54	0.002	0.00199	0.05	0.075	6	0.003	-0.476	0.002	0	0	1
22:2		0.0000							0.0000						
5:00	0.075	6	0.003	-0.54	0.002	0.00199	0.05	0.075	6	0.003	-0.476	0.002	0	0	1
22:3		0.0000							0.0000						
0:00	0.075	6	0.003	-0.54	0.002	0.00199	0.05	0.075	6	0.003	-0.476	0.002	0	0	1
22:3		0.0000							0.0000						
5:00	0.075	6	0.003	-0.54	0.002	0.00199	0.05	0.075	6	0.003	-0.476	0.002	0	0	1
22:4		0.0000							0.0000						
0:00	0.075	6	0.003	-0.54	0.002	0.00199	0.05	0.075	6	0.003	-0.476	0.002	0	0	1
22:4		0.0000							0.0000						
5:00	0.075	6	0.003	-0.54	0.002	0.00199	0.05	0.075	6	0.003	-0.476	0.002	0	0	1
22:5		0.0000							0.0000						
0:00	0.075	6	0.003	-0.54	0.002	0.00199	0.05	0.075	6	0.003	-0.476	0.002	0	0	1
22:5		0.0000							0.0000						
5:00	0.075	5	0.002	-0.54	0.002	0.00199	0.05	0.075	5	0.002	-0.476	0.002	0	0	1
23:0		0.0000							0.0000						
0:00	0.075	5	0.002	-0.54	0.002	0.00199	0.05	0.075	5	0.002	-0.476	0.002	0	0	1
23:0		0.0000							0.0000						
5:00	0.075	5	0.002	-0.54	0.002	0.00199	0.05	0.075	5	0.002	-0.476	0.002	0	0	1
23:1		0.0000							0.0000						
0:00	0.075	5	0.002	-0.54	0.002	0.00199	0.05	0.075	5	0.002	-0.476	0.002	0	0	1
23:1		0.0000							0.0000						
5:00	0.075	5	0.002	-0.54	0.002	0.00199	0.05	0.075	5	0.002	-0.476	0.002	0	0	1
23:2		0.0000							0.0000						
0:00	0.075	5	0.002	-0.54	0.002	0.00199	0.05	0.075	5	0.002	-0.476	0.002	0	0	1
23:2		0.0000							0.0000						
5:00	0.075	5	0.002	-0.54	0.002	0.00199	0.05	0.075	5	0.002	-0.476	0.002	0	0	1
23:3		0.0000							0.0000						
0:00	0.075	5	0.002	-0.54	0.002	0.00199	0.05	0.075	5	0.002	-0.476	0.002	0	0	1
23:3		0.0000							0.0000						
5:00	0.075	5	0.002	-0.54	0.001	0.00199	0.05	0.075	5	0.002	-0.476	0.001	0	0	1
23:4		0.0000							0.0000						
0:00	0.075	4	0.002	-0.54	0.001	0.00199	0.05	0.075	4	0.002	-0.476	0.001	0	0	1
23:4		0.0000							0.0000						
5:00	0.075	4	0.002	-0.54	0.001	0.00199	0.05	0.075	4	0.002	-0.476	0.001	0	0	1
23:5		0.0000							0.0000						
0:00	0.075	4	0.002	-0.54	0.001	0.00199	0.05	0.075	4	0.002	-0.476	0.001	0	0	1
23:5		0.0000							0.0000						
5:00	0.075	4	0.002	-0.54	0.001	0.00199	0.05	0.075	4	0.002	-0.476	0.001	0	0	1
0:00		0.0000							0.0000						
:00	0.075	4	0.002	-0.54	0.001	0.00199	0.05	0.075	4	0.002	-0.476	0.001	0	0	1



	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
0:05:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
0:10:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
0:15:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
0:20:00	0.072	0.00417	0.229	0.542	0.152	0.00242	0.06	0.071	0.00472	0.269	0.572	0.177	0	0	0.3
0:25:00	0.106	0.01838	0.448	0.582	0.376	0.0021	0.09	0.101	0.01969	0.53	0.61	0.434	0	0	0.6
0:30:00	0.145	0.04143	0.538	0.629	0.532	0.00182	0.12	0.137	0.04208	0.616	0.655	0.59	0	0	0.9
0:35:00	0.155	0.04721	0.539	0.64	0.55	0.00171	0.13	0.145	0.04732	0.615	0.664	0.607	0	0	1
0:40:00	0.157	0.04805	0.538	0.641	0.552	0.00169	0.13	0.147	0.04806	0.614	0.666	0.609	0	0	1
0:45:00	0.157	0.04816	0.537	0.642	0.552	0.00169	0.13	0.147	0.04816	0.614	0.666	0.609	0	0	1
0:50:00	0.157	0.04817	0.537	0.642	0.552	0.00169	0.13	0.147	0.04817	0.614	0.666	0.609	0	0	1
0:55:00	0.157	0.04818	0.537	0.642	0.552	0.00169	0.13	0.147	0.04818	0.614	0.666	0.609	0	0	1
1:00:00	0.157	0.04818	0.537	0.642	0.552	0.00169	0.13	0.147	0.04818	0.614	0.666	0.609	0	0	1
1:05:00	0.159	0.04975	0.541	0.644	0.56	0.00169	0.13	0.149	0.04989	0.618	0.668	0.618	0	0	1
1:10:00	0.164	0.054	0.55	0.651	0.579	0.00168	0.14	0.154	0.05419	0.627	0.675	0.638	0	0	1.1
1:15:00	0.168	0.05677	0.553	0.655	0.589	0.00166	0.14	0.158	0.05683	0.629	0.679	0.648	0	0	1.1
1:20:00	0.17	0.05737	0.545	0.657	0.584	0.00161	0.14	0.159	0.05741	0.624	0.68	0.646	0	0	1.1
1:25:00	0.171	0.0575	0.54	0.657	0.581	0.00157	0.14	0.16	0.05752	0.621	0.681	0.643	0	0	1.2
1:30:00	0.172	0.05754	0.538	0.658	0.58	0.00156	0.14	0.16	0.05755	0.619	0.681	0.642	0	0	1.2
1:35:00	0.172	0.05755	0.538	0.658	0.579	0.00156	0.14	0.16	0.05755	0.619	0.681	0.642	0	0	1.2
1:40:00	0.172	0.05755	0.538	0.658	0.579	0.00156	0.14	0.16	0.05755	0.619	0.681	0.642	0	0	1.2
1:45:00	0.172	0.05755	0.538	0.658	0.579	0.00156	0.14	0.16	0.05755	0.619	0.681	0.642	0	0	1.2
1:50:00	0.172	0.05755	0.538	0.658	0.579	0.00156	0.14	0.16	0.05755	0.619	0.681	0.642	0	0	1.2
1:55:00	0.172	0.05755	0.538	0.658	0.579	0.00156	0.14	0.16	0.05755	0.619	0.681	0.642	0	0	1.2
2:00:00	0.172	0.05755	0.538	0.658	0.579	0.00156	0.14	0.16	0.05755	0.619	0.681	0.642	0	0	1.2
2:05:00	0.175	0.05985	0.542	0.661	0.588	0.00156	0.15	0.163	0.06003	0.624	0.685	0.653	0	0	1.2
2:10:00	0.182	0.06573	0.546	0.67	0.606	0.00152	0.15	0.17	0.06601	0.629	0.693	0.674	0	0	1.3
2:15:00	0.189	0.06918	0.537	0.676	0.608	0.00143	0.16	0.175	0.06932	0.622	0.699	0.677	0	0	1.3
2:20:00	0.192	0.07	0.528	0.679	0.601	0.00137	0.16	0.177	0.07006	0.614	0.7	0.673	0	0	1.4

2:25:00	0.193	0.07017	0.522	0.68	0.597	0.00133	0.16	0.178	0.0702	0.61	0.701	0.67	0	0	1.4
2:30:00	0.193	0.07022	0.521	0.68	0.596	0.00132	0.16	0.178	0.07023	0.608	0.701	0.668	0	0	1.4
2:35:00	0.193	0.07024	0.52	0.68	0.596	0.00132	0.16	0.179	0.07024	0.608	0.701	0.668	0	0	1.4
2:40:00	0.193	0.07024	0.52	0.68	0.595	0.00132	0.16	0.179	0.07024	0.608	0.701	0.668	0	0	1.4
2:45:00	0.193	0.07024	0.52	0.68	0.595	0.00132	0.16	0.179	0.07024	0.608	0.701	0.668	0	0	1.4
2:50:00	0.193	0.07024	0.52	0.68	0.595	0.00132	0.16	0.179	0.07024	0.608	0.701	0.668	0	0	1.4
2:55:00	0.193	0.07024	0.52	0.68	0.595	0.00132	0.16	0.179	0.07024	0.608	0.701	0.668	0	0	1.4
3:00:00	0.193	0.07024	0.52	0.68	0.595	0.00132	0.16	0.179	0.07024	0.608	0.701	0.668	0	0	1.4
3:05:00	0.197	0.07376	0.524	0.685	0.607	0.00132	0.16	0.183	0.07404	0.613	0.706	0.682	0	0	1.4
3:10:00	0.208	0.08236	0.526	0.697	0.627	0.00126	0.17	0.193	0.08275	0.615	0.718	0.704	0	0	1.5
3:15:00	0.217	0.08684	0.513	0.706	0.624	0.00115	0.18	0.2	0.08706	0.602	0.725	0.702	0	0	1.6
3:20:00	0.221	0.08788	0.5	0.709	0.614	0.00108	0.18	0.203	0.08798	0.59	0.728	0.693	0	0	1.7
3:25:00	0.223	0.08814	0.494	0.711	0.609	0.00104	0.19	0.205	0.08818	0.584	0.729	0.689	0	0	1.7
3:30:00	0.223	0.08822	0.492	0.711	0.607	0.00103	0.19	0.205	0.08823	0.582	0.729	0.687	0	0	1.7
3:35:00	0.223	0.08825	0.491	0.711	0.607	0.00103	0.19	0.205	0.08825	0.581	0.729	0.686	0	0	1.7
3:40:00	0.224	0.08825	0.491	0.711	0.607	0.00103	0.19	0.205	0.08825	0.581	0.729	0.686	0	0	1.7
3:45:00	0.224	0.08825	0.491	0.711	0.607	0.00103	0.19	0.205	0.08825	0.581	0.729	0.686	0	0	1.7
3:50:00	0.224	0.08825	0.491	0.711	0.607	0.00103	0.19	0.205	0.08825	0.581	0.729	0.686	0	0	1.7
3:55:00	0.224	0.08825	0.491	0.711	0.607	0.00103	0.19	0.205	0.08825	0.581	0.729	0.686	0	0	1.7
4:00:00	0.224	0.08825	0.491	0.711	0.607	0.00103	0.19	0.205	0.08825	0.581	0.729	0.686	0	0	1.7
4:05:00	0.23	0.09406	0.496	0.718	0.622	0.00102	0.19	0.211	0.09451	0.587	0.737	0.704	0	0	1.8
4:10:00	0.246	0.10703	0.494	0.736	0.642	0.00095	0.2	0.227	0.10764	0.583	0.753	0.726	0	0	1.9
4:15:00	0.258	0.11303	0.473	0.748	0.631	0.00082	0.22	0.238	0.1134	0.56	0.764	0.714	0	0	2.1
4:20:00	0.265	0.11452	0.457	0.753	0.618	0.00075	0.22	0.243	0.1147	0.541	0.768	0.699	0	0	2.2
4:25:00	0.268	0.11499	0.45	0.756	0.612	0.00072	0.22	0.245	0.11505	0.533	0.77	0.692	0	0	2.2
4:30:00	0.268	0.11514	0.448	0.756	0.61	0.00071	0.22	0.246	0.11516	0.531	0.77	0.69	0	0	2.2
4:35:00	0.269	0.11518	0.448	0.756	0.609	0.00071	0.22	0.246	0.11519	0.53	0.77	0.69	0	0	2.2
4:40:00	0.269	0.11519	0.448	0.756	0.609	0.00071	0.22	0.246	0.11519	0.53	0.771	0.689	0	0	2.2
4:45:00	0.269	0.11519	0.448	0.756	0.609	0.00071	0.22	0.246	0.11519	0.53	0.771	0.689	0	0	2.2
4:50:00	0.269	0.11519	0.448	0.756	0.609	0.00071	0.22	0.246	0.11519	0.53	0.771	0.689	0	0	2.2
4:55:00	0.269	0.1152	0.448	0.756	0.609	0.00071	0.22	0.246	0.1152	0.53	0.771	0.689	0	0	2.2
5:00:00	0.269	0.1152	0.448	0.756	0.609	0.00071	0.22	0.246	0.1152	0.53	0.771	0.689	0	0	2.2
5:05:00	0.279	0.12566	0.453	0.768	0.63	0.00071	0.23	0.257	0.12642	0.537	0.783	0.713	0	0	2.3
5:10:00	0.304	0.14629	0.446	0.795	0.649	0.00061	0.25	0.281	0.14732	0.524	0.808	0.731	0	0	2.6
5:15:00	0.324	0.15473	0.418	0.813	0.629	0.0005	0.27	0.299	0.15539	0.49	0.824	0.706	0	0	2.9
5:20:00	0.334	0.15707	0.4	0.822	0.612	0.00045	0.28	0.308	0.15737	0.468	0.832	0.685	0	0	3
5:25:00	0.337	0.15803	0.394	0.825	0.607	0.00044	0.28	0.312	0.15812	0.46	0.835	0.678	0	0	3
5:30:00	0.338	0.15831	0.393	0.826	0.605	0.00043	0.28	0.313	0.15833	0.458	0.836	0.676	0	0	3.1
5:35:00	0.338	0.15838	0.392	0.826	0.605	0.00043	0.28	0.313	0.15839	0.457	0.836	0.676	0	0	3.1
5:40:00	0.338	0.1584	0.392	0.826	0.605	0.00043	0.28	0.313	0.1584	0.457	0.836	0.675	0	0	3.1
5:45:00	0.338	0.1584	0.392	0.826	0.605	0.00043	0.28	0.313	0.1584	0.457	0.836	0.675	0	0	3.1
5:50:00	0.338	0.1584	0.392	0.826	0.605	0.00043	0.28	0.313	0.1584	0.457	0.836	0.675	0	0	3.1
5:55:00	0.338	0.1584	0.392	0.826	0.605	0.00043	0.28	0.313	0.1584	0.457	0.836	0.675	0	0	3.1
6:00:00	0.338	0.1584	0.392	0.826	0.605	0.00043	0.28	0.313	0.1584	0.457	0.836	0.675	0	0	3.1
6:05:00	0.358	0.1798	0.4	0.847	0.635	0.00044	0.3	0.332	0.18126	0.465	0.858	0.71	0	0	3.3

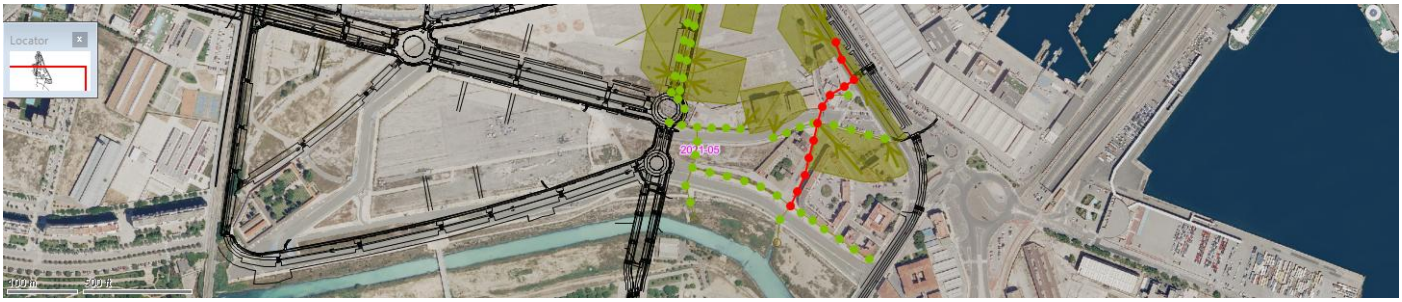
6:10:00	0.401	0.22515	0.384	0.891	0.65	0.00034	0.33	0.374	0.21706	0.443	0.901	0.721	0	0	3.9
6:15:00	0.432	0.22821	0.353	0.921	0.623	0.00027	0.36	0.404	0.22937	0.403	0.928	0.685	0	0	4.3
6:20:00	0.446	0.2327	0.338	0.934	0.608	0.00026	0.37	0.418	0.23314	0.384	0.941	0.665	0	0	4.5
6:25:00	0.45	0.2343	0.334	0.938	0.604	0.00026	0.38	0.423	0.23442	0.378	0.945	0.659	0	0	4.6
6:30:00	0.452	0.23474	0.333	0.939	0.603	0.00026	0.38	0.424	0.23477	0.376	0.946	0.657	0	0	4.6
6:35:00	0.452	0.23485	0.333	0.939	0.603	0.00026	0.38	0.424	0.23486	0.376	0.946	0.657	0	0	4.6
6:40:00	0.452	0.23488	0.333	0.939	0.603	0.00026	0.38	0.424	0.23488	0.376	0.946	0.657	0	0	4.6
6:45:00	0.452	0.23488	0.333	0.939	0.603	0.00026	0.38	0.424	0.23488	0.376	0.946	0.657	0	0	4.6
6:50:00	0.452	0.23488	0.333	0.939	0.603	0.00026	0.38	0.424	0.23488	0.376	0.946	0.657	0	0	4.6
6:55:00	0.452	0.23488	0.333	0.939	0.603	0.00026	0.38	0.424	0.23488	0.376	0.946	0.657	0	0	4.6
7:00:00	0.452	0.23488	0.333	0.939	0.603	0.00026	0.38	0.424	0.23488	0.376	0.946	0.657	0	0	4.6
7:05:00	0.495	0.28814	0.342	0.986	0.655	0.00028	0.41	0.467	0.29137	0.387	0.993	0.715	0	0	5.2
7:10:00	0.578	0.35606	0.315	1.069	0.661	0.00018	0.48	0.549	0.35999	0.351	1.075	0.713	0	0	6.4
7:15:00	0.633	0.37958	0.282	1.122	0.627	0.00016	0.53	0.604	0.38173	0.31	1.127	0.669	0	0	7.3
7:20:00	0.656	0.38691	0.269	1.144	0.612	0.00017	0.55	0.627	0.38765	0.293	1.148	0.649	0	0	7.6
7:25:00	0.663	0.39066	0.266	1.151	0.609	0.00018	0.55	0.634	0.39088	0.289	1.155	0.644	0	0	7.7
7:30:00	0.665	0.3918	0.265	1.153	0.609	0.00018	0.55	0.636	0.39186	0.288	1.157	0.643	0	0	7.7
7:35:00	0.666	0.39211	0.265	1.154	0.609	0.00018	0.55	0.637	0.39213	0.288	1.158	0.643	0	0	7.7
7:40:00	0.666	0.39219	0.264	1.154	0.609	0.00018	0.55	0.637	0.3922	0.288	1.158	0.643	0	0	7.7
7:45:00	0.666	0.39221	0.264	1.154	0.609	0.00018	0.55	0.637	0.39221	0.288	1.158	0.643	0	0	7.7
7:50:00	0.666	0.39222	0.264	1.154	0.609	0.00018	0.55	0.637	0.39222	0.288	1.158	0.643	0	0	7.7
7:55:00	0.666	0.39222	0.264	1.154	0.609	0.00018	0.55	0.637	0.39222	0.288	1.158	0.643	0	0	7.7
8:00:00	0.666	0.39222	0.264	1.154	0.609	0.00018	0.55	0.637	0.39222	0.288	1.158	0.643	0	0	7.7
8:05:00	0.804	0.55495	0.26	1.298	0.689	0.0002	0.67	0.776	0.5646	0.284	1.303	0.73	0	0	9.7
8:10:00	1.034	0.69048	0.19	1.525	0.666	0.00018	0.86	1.005	0.69863	0.206	1.529	0.691	0	0	12.6
8:15:00	1.198	0.73611	0.125	1.689	0.646	0.0003	1	1.171	0.73887	0.138	1.693	0.656	0	0	14
8:20:00	1.289	0.77524	0.085	1.781	0.665	0.0004	1	1.263	0.77599	0.099	1.786	0.669	0	0	14.4
8:25:00	1.338	0.7912	0.056	1.831	0.675	0.00044	1	1.313	0.7914	0.072	1.836	0.676	0	0	14.5
8:30:00	1.36	0.80246	0.041	1.853	0.683	0.00046	1	1.335	0.80249	0.059	1.859	0.684	0	0	14.5
8:35:00	1.373	0.80686	0.031	1.866	0.687	0.00046	1	1.347	0.80688	0.051	1.871	0.688	0	0	14.5
8:40:00	1.377	0.8096	0.031	1.871	0.689	0.00047	1	1.352	0.8096	0.047	1.876	0.69	0	0	14.5
8:45:00	1.38	0.81098	0.032	1.873	0.69	0.00047	1	1.355	0.81098	0.046	1.879	0.691	0	0	14.5
8:50:00	1.381	0.81152	0.032	1.874	0.691	0.00047	1	1.356	0.81152	0.045	1.88	0.691	0	0	14.5
8:55:00	1.382	0.81146	0.032	1.875	0.691	0.00047	1	1.357	0.81146	0.044	1.881	0.691	0	0	14.5
9:00:00	1.383	0.81184	0.032	1.876	0.691	0.00047	1	1.357	0.81185	0.044	1.882	0.692	0	0	14.5
9:05:00	1.205	0.75887	0.126	1.697	0.665	0.00035	1	1.179	0.75549	0.138	1.701	0.668	0	0	14
9:10:00	1.032	0.63691	0.176	1.52	0.616	0.00022	0.86	1.003	0.6317	0.187	1.523	0.625	0	0	12.6
9:15:00	0.943	0.57643	0.196	1.431	0.605	0.0002	0.79	0.915	0.57377	0.208	1.434	0.62	0	0	11.6
9:20:00	0.903	0.55838	0.208	1.391	0.611	0.00019	0.75	0.875	0.55708	0.221	1.395	0.631	0	0	11.1
9:25:00	0.885	0.55069	0.214	1.373	0.616	0.00019	0.74	0.856	0.55011	0.228	1.377	0.637	0	0	10.8
9:30:00	0.877	0.54744	0.217	1.365	0.618	0.00019	0.73	0.848	0.54717	0.231	1.369	0.641	0	0	10.7
9:35:00	0.874	0.54535	0.217	1.362	0.618	0.00018	0.73	0.845	0.54529	0.232	1.366	0.641	0	0	10.7
9:40:00	0.873	0.54491	0.217	1.362	0.618	0.00018	0.73	0.845	0.54489	0.232	1.365	0.641	0	0	10.7
9:45:00	0.873	0.5448	0.217	1.362	0.618	0.00018	0.73	0.844	0.54479	0.232	1.365	0.641	0	0	10.7
9:50:00	0.873	0.54477	0.217	1.362	0.618	0.00018	0.73	0.844	0.54477	0.232	1.365	0.641	0	0	10.7

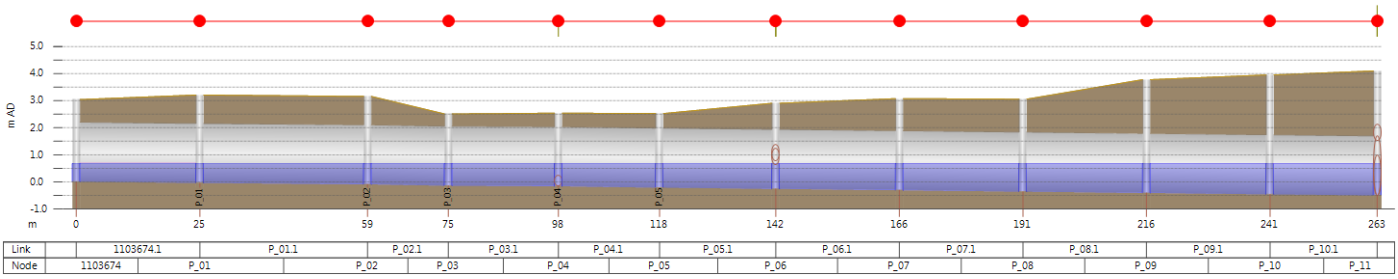
9:55:00	0.873	0.54476	0.217	1.362	0.618	0.00018	0.73	0.844	0.54476	0.232	1.365	0.641	0	0	10.7
10:00:00	0.873	0.54476	0.217	1.362	0.618	0.00018	0.73	0.844	0.54476	0.232	1.365	0.641	0	0	10.7
10:05:00	0.797	0.45793	0.218	1.283	0.574	0.00015	0.66	0.768	0.45291	0.232	1.286	0.592	0	0	9.6
10:10:00	0.675	0.36572	0.241	1.159	0.559	0.0002	0.56	0.646	0.35986	0.257	1.163	0.58	0	0	7.9
10:15:00	0.59	0.32085	0.272	1.077	0.579	0.00021	0.49	0.562	0.31753	0.296	1.081	0.611	0	0	6.6
10:20:00	0.554	0.30443	0.291	1.041	0.596	0.00022	0.46	0.526	0.30328	0.321	1.047	0.636	0	0	6.1
10:25:00	0.543	0.30015	0.299	1.03	0.604	0.00021	0.45	0.514	0.29981	0.331	1.036	0.647	0	0	5.9
10:30:00	0.54	0.2989	0.301	1.027	0.606	0.00021	0.45	0.511	0.29881	0.334	1.033	0.651	0	0	5.9
10:35:00	0.539	0.29857	0.302	1.026	0.607	0.00021	0.45	0.51	0.29855	0.335	1.032	0.651	0	0	5.9
10:40:00	0.539	0.29849	0.302	1.026	0.607	0.00021	0.45	0.51	0.29848	0.335	1.032	0.652	0	0	5.9
10:45:00	0.538	0.29847	0.302	1.026	0.607	0.00021	0.45	0.51	0.29847	0.335	1.032	0.652	0	0	5.9
10:50:00	0.538	0.29846	0.302	1.026	0.607	0.00021	0.45	0.51	0.29846	0.335	1.032	0.652	0	0	5.9
10:55:00	0.538	0.29846	0.302	1.026	0.607	0.00021	0.45	0.51	0.29846	0.335	1.032	0.652	0	0	5.9
11:00:00	0.538	0.29846	0.302	1.026	0.607	0.00021	0.45	0.51	0.29846	0.335	1.032	0.652	0	0	5.9
11:05:00	0.51	0.26328	0.295	0.996	0.574	0.0002	0.43	0.482	0.26121	0.327	1.001	0.615	0	0	5.4
11:10:00	0.456	0.21891	0.305	0.941	0.555	0.00024	0.38	0.428	0.21634	0.34	0.946	0.598	0	0	4.7
11:15:00	0.416	0.20002	0.332	0.902	0.574	0.0003	0.35	0.389	0.19854	0.376	0.909	0.626	0	0	4.1
11:20:00	0.397	0.19381	0.352	0.884	0.593	0.00032	0.33	0.37	0.19323	0.402	0.892	0.651	0	0	3.8
11:25:00	0.391	0.19182	0.36	0.878	0.6	0.00033	0.33	0.364	0.19164	0.412	0.886	0.662	0	0	3.8
11:30:00	0.389	0.19118	0.362	0.876	0.602	0.00033	0.32	0.362	0.19114	0.415	0.885	0.665	0	0	3.7
11:35:00	0.388	0.19103	0.362	0.876	0.603	0.00033	0.32	0.362	0.19102	0.416	0.884	0.665	0	0	3.7
11:40:00	0.388	0.19099	0.362	0.876	0.603	0.00033	0.32	0.361	0.19099	0.416	0.884	0.665	0	0	3.7
11:45:00	0.388	0.19099	0.362	0.876	0.603	0.00033	0.32	0.361	0.19099	0.416	0.884	0.666	0	0	3.7
11:50:00	0.388	0.19098	0.362	0.876	0.603	0.00033	0.32	0.361	0.19098	0.416	0.884	0.666	0	0	3.7
11:55:00	0.388	0.19098	0.362	0.876	0.603	0.00033	0.32	0.361	0.19098	0.416	0.884	0.666	0	0	3.7
12:00:00	0.388	0.19098	0.362	0.876	0.603	0.00033	0.32	0.361	0.19098	0.416	0.884	0.666	0	0	3.7
12:05:00	0.374	0.17527	0.357	0.861	0.582	0.00032	0.31	0.347	0.17424	0.41	0.868	0.641	0	0	3.5
12:10:00	0.343	0.15051	0.362	0.829	0.563	0.00038	0.29	0.317	0.14911	0.419	0.837	0.624	0	0	3.1
12:15:00	0.319	0.13919	0.388	0.805	0.578	0.00046	0.27	0.293	0.13835	0.453	0.815	0.646	0	0	2.8
12:20:00	0.306	0.13572	0.408	0.793	0.596	0.00052	0.26	0.282	0.13536	0.479	0.805	0.669	0	0	2.6
12:25:00	0.302	0.13465	0.417	0.789	0.604	0.00055	0.25	0.277	0.13453	0.491	0.801	0.68	0	0	2.6
12:30:00	0.3	0.13432	0.42	0.788	0.607	0.00056	0.25	0.276	0.13429	0.494	0.8	0.683	0	0	2.6
12:35:00	0.3	0.13424	0.421	0.788	0.607	0.00056	0.25	0.276	0.13423	0.495	0.8	0.684	0	0	2.6
12:40:00	0.3	0.13422	0.421	0.788	0.608	0.00056	0.25	0.276	0.13422	0.495	0.8	0.684	0	0	2.6
12:45:00	0.3	0.13421	0.421	0.788	0.608	0.00056	0.25	0.276	0.13421	0.496	0.8	0.684	0	0	2.6
12:50:00	0.3	0.13421	0.421	0.788	0.608	0.00056	0.25	0.276	0.13421	0.496	0.8	0.684	0	0	2.6
12:55:00	0.3	0.13421	0.421	0.788	0.608	0.00056	0.25	0.276	0.13421	0.496	0.8	0.684	0	0	2.6
13:00:00	0.3	0.13421	0.421	0.788	0.608	0.00056	0.25	0.276	0.13421	0.496	0.8	0.684	0	0	2.6
13:05:00	0.292	0.12603	0.416	0.779	0.593	0.00056	0.24	0.268	0.12544	0.49	0.79	0.667	0	0	2.5
13:10:00	0.272	0.11079	0.419	0.758	0.575	0.00061	0.23	0.249	0.10998	0.496	0.77	0.648	0	0	2.2
13:15:00	0.256	0.10327	0.44	0.743	0.584	0.00072	0.21	0.234	0.1028	0.522	0.757	0.661	0	0	2
13:20:00	0.248	0.10117	0.459	0.736	0.599	0.00081	0.21	0.227	0.10097	0.544	0.751	0.678	0	0	2
13:25:00	0.245	0.10063	0.467	0.733	0.606	0.00085	0.2	0.225	0.10053	0.554	0.749	0.687	0	0	1.9
13:30:00	0.244	0.10043	0.47	0.732	0.608	0.00086	0.2	0.224	0.10042	0.558	0.748	0.689	0	0	1.9
13:35:00	0.244	0.10039	0.471	0.732	0.609	0.00086	0.2	0.224	0.10038	0.558	0.748	0.69	0	0	1.9

13:40:00	0.244	0.10038	0.471	0.732	0.609	0.00087	0.2	0.224	0.10038	0.559	0.748	0.69	0	0	1.9
13:45:00	0.244	0.10038	0.471	0.732	0.609	0.00087	0.2	0.224	0.10038	0.559	0.748	0.69	0	0	1.9
13:50:00	0.244	0.10038	0.471	0.732	0.609	0.00087	0.2	0.224	0.10038	0.559	0.748	0.69	0	0	1.9
13:55:00	0.244	0.10038	0.471	0.732	0.609	0.00087	0.2	0.224	0.10038	0.559	0.748	0.69	0	0	1.9
14:00:00	0.244	0.10038	0.471	0.732	0.609	0.00087	0.2	0.224	0.10038	0.559	0.748	0.69	0	0	1.9
14:05:00	0.239	0.09563	0.467	0.726	0.598	0.00087	0.2	0.219	0.09527	0.554	0.742	0.677	0	0	1.9
14:10:00	0.226	0.08562	0.467	0.712	0.58	0.00092	0.19	0.206	0.08512	0.555	0.728	0.658	0	0	1.7
14:15:00	0.215	0.08033	0.482	0.702	0.583	0.00103	0.18	0.197	0.08003	0.572	0.719	0.661	0	0	1.6
14:20:00	0.21	0.07892	0.496	0.697	0.594	0.00112	0.18	0.193	0.07882	0.587	0.716	0.671	0	0	1.5
14:25:00	0.208	0.07866	0.504	0.695	0.599	0.00116	0.17	0.191	0.07856	0.594	0.715	0.676	0	0	1.5
14:30:00	0.207	0.07851	0.506	0.695	0.601	0.00117	0.17	0.191	0.07851	0.596	0.714	0.678	0	0	1.5
14:35:00	0.207	0.07848	0.507	0.695	0.602	0.00118	0.17	0.191	0.07848	0.597	0.714	0.678	0	0	1.5
14:40:00	0.207	0.07848	0.507	0.695	0.602	0.00118	0.17	0.191	0.07848	0.597	0.714	0.679	0	0	1.5
14:45:00	0.207	0.07848	0.507	0.695	0.602	0.00118	0.17	0.191	0.07848	0.597	0.714	0.679	0	0	1.5
14:50:00	0.207	0.07848	0.507	0.695	0.602	0.00118	0.17	0.191	0.07848	0.597	0.714	0.679	0	0	1.5
14:55:00	0.207	0.07848	0.507	0.695	0.602	0.00118	0.17	0.191	0.07848	0.597	0.714	0.679	0	0	1.5
15:00:00	0.207	0.07848	0.507	0.695	0.602	0.00118	0.17	0.191	0.07848	0.597	0.714	0.679	0	0	1.5
15:05:00	0.204	0.07551	0.504	0.691	0.593	0.00118	0.17	0.187	0.07527	0.593	0.71	0.668	0	0	1.5
15:10:00	0.195	0.06867	0.501	0.681	0.576	0.00122	0.16	0.179	0.06834	0.59	0.7	0.649	0	0	1.4
15:15:00	0.187	0.06473	0.51	0.673	0.574	0.00131	0.16	0.172	0.06456	0.598	0.694	0.646	0	0	1.3
15:20:00	0.184	0.06371	0.521	0.67	0.581	0.00138	0.15	0.17	0.06364	0.607	0.691	0.65	0	0	1.3
15:25:00	0.182	0.06357	0.527	0.669	0.585	0.00142	0.15	0.169	0.06347	0.612	0.691	0.654	0	0	1.3
15:30:00	0.182	0.06344	0.529	0.669	0.587	0.00144	0.15	0.169	0.06344	0.614	0.691	0.655	0	0	1.3
15:35:00	0.182	0.06343	0.529	0.668	0.587	0.00144	0.15	0.169	0.06343	0.615	0.691	0.655	0	0	1.3
15:40:00	0.182	0.06343	0.53	0.668	0.588	0.00144	0.15	0.169	0.06342	0.615	0.691	0.655	0	0	1.3
15:45:00	0.182	0.06342	0.53	0.668	0.588	0.00144	0.15	0.169	0.06342	0.615	0.691	0.656	0	0	1.3
15:50:00	0.182	0.06342	0.53	0.668	0.588	0.00144	0.15	0.169	0.06342	0.615	0.691	0.656	0	0	1.3
15:55:00	0.182	0.06342	0.53	0.668	0.588	0.00144	0.15	0.169	0.06342	0.615	0.691	0.656	0	0	1.3
16:00:00	0.182	0.06342	0.53	0.668	0.588	0.00144	0.15	0.169	0.06342	0.615	0.691	0.656	0	0	1.3
16:05:00	0.179	0.06145	0.527	0.666	0.58	0.00144	0.15	0.166	0.06129	0.611	0.688	0.647	0	0	1.2
16:10:00	0.173	0.05663	0.522	0.658	0.564	0.00147	0.14	0.16	0.05640	0.606	0.68	0.629	0	0	1.2
16:15:00	0.167	0.05361	0.527	0.652	0.56	0.00154	0.14	0.155	0.05349	0.609	0.675	0.623	0	0	1.1
16:20:00	0.165	0.05281	0.536	0.65	0.565	0.00161	0.14	0.154	0.05276	0.615	0.673	0.625	0	0	1.1
16:25:00	0.164	0.05265	0.542	0.649	0.569	0.00165	0.14	0.153	0.05263	0.619	0.673	0.627	0	0	1.1
16:30:00	0.163	0.05261	0.544	0.649	0.57	0.00166	0.14	0.153	0.0526	0.62	0.673	0.628	0	0	1.1
16:35:00	0.163	0.0526	0.545	0.649	0.571	0.00167	0.14	0.153	0.0526	0.621	0.673	0.629	0	0	1.1
16:40:00	0.163	0.0526	0.545	0.649	0.571	0.00167	0.14	0.153	0.0526	0.621	0.673	0.629	0	0	1.1
16:45:00	0.163	0.05259	0.545	0.649	0.571	0.00167	0.14	0.153	0.05259	0.621	0.673	0.629	0	0	1.1
16:50:00	0.163	0.05259	0.545	0.649	0.571	0.00167	0.14	0.153	0.05259	0.621	0.673	0.629	0	0	1.1
16:55:00	0.163	0.05259	0.545	0.649	0.571	0.00167	0.14	0.153	0.05259	0.621	0.673	0.629	0	0	1.1
17:00:00	0.163	0.05259	0.545	0.649	0.571	0.00167	0.14	0.153	0.05259	0.621	0.673	0.629	0	0	1.1
17:05:00	0.161	0.05122	0.542	0.647	0.565	0.00167	0.13	0.151	0.05116	0.617	0.671	0.621	0	0	1.1
17:10:00	0.157	0.04769	0.534	0.641	0.548	0.00167	0.13	0.146	0.04753	0.609	0.665	0.604	0	0	1
17:15:00	0.153	0.04533	0.53	0.637	0.538	0.00169	0.13	0.143	0.04523	0.606	0.661	0.594	0	0	1
17:20:00	0.152	0.04465	0.53	0.636	0.536	0.0017	0.13	0.142	0.04463	0.606	0.66	0.592	0	0	1

17:25:00	0.152	0.04454	0.53	0.636	0.536	0.0017	0.13	0.142	0.04453	0.606	0.66	0.591	0	0	1
17:30:00	0.152	0.04452	0.53	0.636	0.536	0.0017	0.13	0.142	0.04452	0.606	0.66	0.591	0	0	1
17:35:00	0.152	0.04452	0.53	0.636	0.536	0.0017	0.13	0.142	0.04452	0.606	0.66	0.591	0	0	1
17:40:00	0.152	0.04452	0.53	0.636	0.536	0.0017	0.13	0.142	0.04452	0.606	0.66	0.591	0	0	1
17:45:00	0.152	0.04452	0.53	0.636	0.536	0.0017	0.13	0.142	0.04452	0.606	0.66	0.591	0	0	1
17:50:00	0.152	0.04452	0.53	0.636	0.536	0.0017	0.13	0.142	0.04452	0.606	0.66	0.591	0	0	1
17:55:00	0.152	0.04452	0.53	0.636	0.536	0.0017	0.13	0.142	0.04452	0.606	0.66	0.591	0	0	1
18:00:00	0.152	0.04452	0.53	0.636	0.536	0.0017	0.13	0.142	0.04452	0.606	0.66	0.591	0	0	1
18:05:00	0.143	0.03781	0.508	0.625	0.497	0.00169	0.12	0.133	0.03721	0.578	0.648	0.545	0	0	0.9
18:10:00	0.117	0.02153	0.43	0.593	0.38	0.00171	0.1	0.107	0.02069	0.493	0.616	0.416	0	0	0.7
18:15:00	0.09	0.00908	0.306	0.562	0.237	0.00186	0.07	0.082	0.00852	0.351	0.585	0.255	0	0	0.4
18:20:00	0.072	0.00308	0.167	0.542	0.112	0.00215	0.06	0.068	0.00283	0.178	0.568	0.114	0	0	0.3
18:25:00	0.064	0.00089	0.063	0.533	0.039	0.00235	0.05	0.062	0.0008	0.061	0.562	0.037	0	0	0.3
18:30:00	0.061	0.00026	0.02	0.53	0.012	0.00246	0.05	0.061	0.00023	0.019	0.561	0.011	0	0	0.3
18:35:00	0.061	0.00011	0.009	0.53	0.005	0.00249	0.05	0.06	0.0001	0.009	0.56	0.005	0	0	0.3
18:40:00	0.06	0.00008	0.007	0.529	0.004	0.0025	0.05	0.06	0.00008	0.007	0.56	0.004	0	0	0.3
18:45:00	0.06	0.00008	0.007	0.529	0.004	0.00251	0.05	0.06	0.00008	0.007	0.56	0.004	0	0	0.3
18:50:00	0.06	0.00008	0.007	0.529	0.004	0.00251	0.05	0.06	0.00008	0.007	0.56	0.004	0	0	0.3
18:55:00	0.06	0.00008	0.007	0.529	0.004	0.00251	0.05	0.06	0.00008	0.007	0.56	0.004	0	0	0.3
19:00:00	0.06	0.00008	0.007	0.529	0.004	0.00251	0.05	0.06	0.00008	0.007	0.56	0.004	0	0	0.3
19:00:00	0.06	0.00007	0.006	0.529	0.004	0.00251	0.05	0.06	0.00007	0.006	0.56	0.003	0	0	0.3
19:10:00	0.06	0.00006	0.005	0.529	0.003	0.00251	0.05	0.06	0.00006	0.005	0.56	0.003	0	0	0.3
19:15:00	0.06	0.00003	0.003	0.529	0.002	0.00251	0.05	0.06	0.00003	0.003	0.56	0.002	0	0	0.3
19:20:00	0.06	0.00001	0.001	0.529	0.001	0.00251	0.05	0.06	0.00001	0.001	0.56	0.001	0	0	0.3
19:25:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
19:30:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
19:35:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
19:40:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
19:45:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
19:50:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
19:55:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:00:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:05:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:10:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:15:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:20:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:25:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:30:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:35:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:40:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:45:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:50:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
20:55:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:00:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3

21:10:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:15:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:20:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:25:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:30:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:35:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:40:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:45:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:50:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
21:55:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:00:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:05:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:10:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:15:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:20:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:25:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:30:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:35:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:40:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:45:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:50:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
22:55:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:00:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:05:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:10:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:15:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:20:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:25:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:30:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:35:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:40:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:45:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:50:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
23:55:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3
0:00:00	0.06	0	0	0.529	0	0.00251	0.05	0.06	0	0	0.56	0	0	0	0.3





	DS depth (m)	DS flow (m3/s)	DS Froude number	DS total head (m AD)	DS velocity (m/s)	Hydraulic gradient	Surcharge state	US depth (m)	US flow (m3/s)	US Froude number	US total head (m AD)	US velocity (m/s)	Infiltration loss (m3/s)	Lateral inflow (m3/s)	Volume (m3)
0:00:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
0:05:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
0:10:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
0:15:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
0:20:00	0.114	0.0011	0.018	-0.387	0.015	0.00187	0.05	0.112	0.0014	0.026	-0.346	0.021	0	0	1.5
0:25:00	0.137	0.01771	0.198	-0.363	0.182	0.00169	0.06	0.13	0.0202	0.251	-0.325	0.224	0	0	2
0:30:00	0.185	0.02929	0.172	-0.314	0.191	0.00063	0.08	0.156	0.03326	0.276	-0.298	0.28	0	0	2.9
0:35:00	0.238	0.02799	0.1	-0.262	0.126	0.00012	0.11	0.198	0.03228	0.166	-0.258	0.19	0	0	4.2
0:40:00	0.275	0.02949	0.079	-0.225	0.107	0.00006	0.13	0.234	0.0324	0.12	-0.223	0.15	0	0	5.3
0:45:00	0.296	0.03354	0.078	-0.204	0.11	0.00006	0.13	0.255	0.03499	0.109	-0.202	0.143	0	0	6
0:50:00	0.305	0.03742	0.082	-0.196	0.118	0.00007	0.14	0.263	0.03791	0.111	-0.194	0.147	0	0	6.2
0:55:00	0.307	0.03908	0.084	-0.193	0.121	0.00007	0.14	0.266	0.03921	0.113	-0.191	0.15	0	0	6.3
1:00:00	0.308	0.03957	0.085	-0.192	0.122	0.00007	0.14	0.266	0.0396	0.113	-0.191	0.151	0	0	6.3
1:05:00	0.309	0.04024	0.086	-0.191	0.124	0.00007	0.14	0.267	0.04052	0.115	-0.189	0.154	0	0	6.4
1:10:00	0.314	0.04256	0.088	-0.186	0.128	0.00006	0.14	0.272	0.04329	0.119	-0.184	0.16	0	0	6.5
1:15:00	0.321	0.04363	0.086	-0.179	0.127	0.00006	0.15	0.279	0.04443	0.116	-0.177	0.158	0	0	6.8
1:20:00	0.327	0.04482	0.085	-0.173	0.127	0.00005	0.15	0.286	0.04537	0.113	-0.171	0.157	0	0	7
1:25:00	0.331	0.046	0.085	-0.169	0.128	0.00005	0.15	0.289	0.04629	0.112	-0.167	0.157	0	0	7.1
1:30:00	0.333	0.04683	0.086	-0.167	0.129	0.00005	0.15	0.291	0.04695	0.113	-0.166	0.158	0	0	7.1
1:35:00	0.334	0.04724	0.087	-0.166	0.13	0.00005	0.15	0.292	0.04728	0.113	-0.165	0.158	0	0	7.2
1:40:00	0.334	0.04739	0.087	-0.166	0.13	0.00005	0.15	0.292	0.0474	0.113	-0.165	0.158	0	0	7.2
1:45:00	0.334	0.04744	0.087	-0.166	0.13	0.00005	0.15	0.292	0.04744	0.113	-0.165	0.158	0	0	7.2
1:50:00	0.334	0.04745	0.087	-0.166	0.13	0.00005	0.15	0.292	0.04745	0.113	-0.165	0.158	0	0	7.2
1:55:00	0.334	0.04745	0.087	-0.166	0.13	0.00005	0.15	0.292	0.04745	0.113	-0.165	0.158	0	0	7.2
2:00:00	0.334	0.04745	0.087	-0.166	0.13	0.00005	0.15	0.292	0.04745	0.113	-0.165	0.158	0	0	7.2
2:05:00	0.335	0.04815	0.087	-0.165	0.132	0.00006	0.15	0.294	0.04856	0.115	-0.163	0.161	0	0	7.2
2:10:00	0.342	0.05094	0.089	-0.158	0.135	0.00005	0.16	0.3	0.05197	0.117	-0.156	0.167	0	0	7.5
2:15:00	0.352	0.05225	0.086	-0.148	0.133	0.00004	0.16	0.31	0.05333	0.113	-0.147	0.163	0	0	7.8
2:20:00	0.36	0.05405	0.085	-0.14	0.133	0.00004	0.16	0.318	0.05478	0.11	-0.139	0.162	0	0	8.1
2:25:00	0.365	0.05592	0.086	-0.136	0.135	0.00004	0.17	0.322	0.05627	0.11	-0.134	0.163	0	0	8.2

2:30:00	0.366	0.05712	0.087	-0.134	0.137	0.00004	0.17	0.324	0.05725	0.111	-0.132	0.164	0	0	8.3
2:35:00	0.367	0.05766	0.087	-0.133	0.138	0.00004	0.17	0.325	0.0577	0.111	-0.131	0.165	0	0	8.3
2:40:00	0.367	0.05784	0.088	-0.133	0.139	0.00004	0.17	0.325	0.05785	0.111	-0.131	0.165	0	0	8.3
2:45:00	0.367	0.05789	0.088	-0.133	0.139	0.00004	0.17	0.325	0.05789	0.111	-0.131	0.165	0	0	8.3
2:50:00	0.367	0.05791	0.088	-0.133	0.139	0.00004	0.17	0.325	0.05791	0.111	-0.131	0.165	0	0	8.3
2:55:00	0.367	0.05791	0.088	-0.133	0.139	0.00004	0.17	0.325	0.05791	0.111	-0.131	0.165	0	0	8.3
3:00:00	0.367	0.05791	0.088	-0.133	0.139	0.00004	0.17	0.325	0.05791	0.111	-0.131	0.165	0	0	8.3
3:05:00	0.369	0.0591	0.089	-0.131	0.14	0.00004	0.17	0.327	0.05969	0.113	-0.129	0.169	0	0	8.4
3:10:00	0.379	0.0627	0.09	-0.121	0.144	0.00004	0.17	0.336	0.06412	0.116	-0.12	0.174	0	0	8.7
3:15:00	0.391	0.0644	0.086	-0.109	0.141	0.00003	0.18	0.349	0.06582	0.11	-0.108	0.17	0	0	9.1
3:20:00	0.401	0.06725	0.086	-0.099	0.142	0.00003	0.18	0.359	0.06815	0.108	-0.098	0.169	0	0	9.5
3:25:00	0.406	0.07005	0.087	-0.094	0.145	0.00003	0.18	0.364	0.07047	0.109	-0.093	0.171	0	0	9.7
3:30:00	0.408	0.07173	0.088	-0.092	0.147	0.00004	0.19	0.366	0.07188	0.11	-0.09	0.173	0	0	9.8
3:35:00	0.409	0.07244	0.089	-0.091	0.149	0.00004	0.19	0.367	0.07249	0.11	-0.09	0.174	0	0	9.8
3:40:00	0.409	0.07268	0.089	-0.091	0.149	0.00004	0.19	0.367	0.07269	0.11	-0.089	0.174	0	0	9.8
3:45:00	0.409	0.07274	0.089	-0.091	0.149	0.00004	0.19	0.367	0.07274	0.11	-0.089	0.174	0	0	9.8
3:50:00	0.409	0.07276	0.089	-0.09	0.149	0.00004	0.19	0.367	0.07276	0.11	-0.089	0.174	0	0	9.8
3:55:00	0.409	0.07276	0.089	-0.09	0.149	0.00004	0.19	0.367	0.07276	0.11	-0.089	0.174	0	0	9.8
4:00:00	0.409	0.07276	0.089	-0.09	0.149	0.00004	0.19	0.367	0.07276	0.11	-0.089	0.174	0	0	9.8
4:05:00	0.413	0.07445	0.09	-0.087	0.151	0.00004	0.19	0.371	0.07545	0.112	-0.086	0.178	0	0	9.9
4:10:00	0.427	0.07884	0.089	-0.073	0.152	0.00002	0.19	0.384	0.08101	0.112	-0.072	0.182	0	0	10.4
4:15:00	0.444	0.08107	0.085	-0.056	0.148	0.00002	0.2	0.402	0.08311	0.106	-0.055	0.175	0	0	11.1
4:20:00	0.457	0.08603	0.085	-0.043	0.151	0.00003	0.21	0.415	0.08726	0.104	-0.042	0.176	0	0	11.6
4:25:00	0.464	0.0908	0.087	-0.036	0.156	0.00003	0.21	0.421	0.09133	0.106	-0.035	0.18	0	0	11.8
4:30:00	0.466	0.09348	0.089	-0.034	0.159	0.00003	0.21	0.424	0.09366	0.107	-0.033	0.183	0	0	11.9
4:35:00	0.467	0.09453	0.09	-0.033	0.16	0.00003	0.21	0.425	0.09458	0.108	-0.032	0.184	0	0	12
4:40:00	0.467	0.09486	0.09	-0.032	0.161	0.00003	0.21	0.425	0.09487	0.108	-0.031	0.184	0	0	12
4:45:00	0.467	0.09495	0.09	-0.032	0.161	0.00003	0.21	0.425	0.09495	0.108	-0.031	0.184	0	0	12
4:50:00	0.467	0.09497	0.09	-0.032	0.161	0.00003	0.21	0.425	0.09497	0.108	-0.031	0.184	0	0	12
4:55:00	0.467	0.09497	0.09	-0.032	0.161	0.00003	0.21	0.425	0.09497	0.108	-0.031	0.184	0	0	12
5:00:00	0.467	0.09497	0.09	-0.032	0.161	0.00003	0.21	0.425	0.09497	0.108	-0.031	0.184	0	0	12
5:05:00	0.473	0.0979	0.09	-0.027	0.163	0.00003	0.22	0.431	0.09963	0.111	-0.026	0.19	0	0	12.2
5:10:00	0.495	0.10264	0.087	-0.005	0.161	0.00001	0.22	0.452	0.10606	0.107	-0.004	0.189	0	0	13
5:15:00	0.519	0.1059	0.081	0.02	0.155	0.00001	0.24	0.477	0.10885	0.099	0.02	0.179	0	0	14
5:20:00	0.536	0.11538	0.083	0.036	0.161	0.00002	0.24	0.494	0.11703	0.099	0.037	0.184	0	0	14.7
5:25:00	0.544	0.1239	0.087	0.045	0.169	0.00002	0.25	0.502	0.12459	0.103	0.046	0.191	0	0	15
5:30:00	0.547	0.12831	0.089	0.048	0.174	0.00002	0.25	0.505	0.12854	0.105	0.049	0.195	0	0	15.1
5:35:00	0.548	0.12994	0.09	0.049	0.176	0.00002	0.25	0.506	0.13001	0.105	0.05	0.197	0	0	15.2
5:40:00	0.548	0.13043	0.09	0.049	0.176	0.00002	0.25	0.506	0.13045	0.106	0.05	0.198	0	0	15.2
5:45:00	0.549	0.13056	0.09	0.049	0.176	0.00002	0.25	0.506	0.13056	0.106	0.05	0.198	0	0	15.2
5:50:00	0.549	0.13059	0.09	0.049	0.176	0.00002	0.25	0.506	0.13059	0.106	0.05	0.198	0	0	15.2
5:55:00	0.549	0.13059	0.09	0.049	0.176	0.00002	0.25	0.506	0.13059	0.106	0.05	0.198	0	0	15.2
6:00:00	0.549	0.1306	0.09	0.049	0.176	0.00002	0.25	0.506	0.1306	0.106	0.05	0.198	0	0	15.2
6:05:00	0.56	0.13609	0.09	0.06	0.179	0.00002	0.25	0.517	0.13944	0.108	0.061	0.205	0	0	15.6
6:10:00	0.596	0.13815	0.081	0.096	0.166	0	0.27	0.553	0.14389	0.098	0.096	0.192	0	0	17.1

6:15:00	0.632	0.14448	0.076	0.133	0.16	0.00001	0.29	0.59	0.14905	0.09	0.133	0.182	0	0	18.7
6:20:00	0.656	0.16596	0.081	0.156	0.175	0.00002	0.3	0.613	0.16837	0.094	0.157	0.194	0	0	19.7
6:25:00	0.667	0.18265	0.087	0.167	0.188	0.00002	0.3	0.624	0.18358	0.099	0.168	0.207	0	0	20.1
6:30:00	0.67	0.19021	0.089	0.171	0.194	0.00002	0.3	0.628	0.1905	0.101	0.172	0.213	0	0	20.3
6:35:00	0.671	0.19272	0.09	0.172	0.196	0.00002	0.31	0.629	0.1928	0.102	0.173	0.215	0	0	20.4
6:40:00	0.672	0.19342	0.09	0.173	0.197	0.00002	0.31	0.629	0.19344	0.103	0.173	0.216	0	0	20.4
6:45:00	0.672	0.1936	0.09	0.173	0.197	0.00002	0.31	0.629	0.1936	0.103	0.173	0.216	0	0	20.4
6:50:00	0.672	0.19363	0.09	0.173	0.197	0.00002	0.31	0.629	0.19364	0.103	0.173	0.216	0	0	20.4
6:55:00	0.672	0.19364	0.09	0.173	0.197	0.00002	0.31	0.629	0.19364	0.103	0.173	0.216	0	0	20.4
7:00:00	0.672	0.19365	0.09	0.173	0.197	0.00002	0.31	0.629	0.19365	0.103	0.173	0.216	0	0	20.4
7:05:00	0.697	0.20343	0.088	0.198	0.197	0.00001	0.32	0.655	0.2111	0.104	0.199	0.223	0	0	21.5
7:10:00	0.756	0.21723	0.081	0.257	0.188	0	0.34	0.713	0.22571	0.094	0.257	0.211	0	0	24.1
7:15:00	0.801	0.25513	0.085	0.302	0.204	0.00002	0.36	0.758	0.26054	0.096	0.303	0.224	0	0	26.1
7:20:00	0.825	0.29205	0.092	0.327	0.224	0.00002	0.38	0.783	0.29455	0.102	0.328	0.243	0	0	27.2
7:25:00	0.835	0.31118	0.095	0.337	0.235	0.00002	0.38	0.793	0.31214	0.106	0.338	0.253	0	0	27.7
7:30:00	0.839	0.31911	0.097	0.341	0.24	0.00002	0.38	0.796	0.31945	0.107	0.342	0.257	0	0	27.9
7:35:00	0.84	0.32186	0.097	0.342	0.241	0.00002	0.38	0.798	0.32198	0.108	0.343	0.259	0	0	27.9
7:40:00	0.841	0.32277	0.098	0.343	0.242	0.00002	0.38	0.798	0.32282	0.108	0.344	0.259	0	0	28
7:45:00	0.841	0.32309	0.098	0.343	0.242	0.00002	0.38	0.798	0.32311	0.108	0.344	0.259	0	0	28
7:50:00	0.841	0.32322	0.098	0.343	0.242	0.00002	0.38	0.799	0.32323	0.108	0.344	0.259	0	0	28
7:55:00	0.841	0.32327	0.098	0.343	0.242	0.00002	0.38	0.799	0.32328	0.108	0.344	0.259	0	0	28
8:00:00	0.841	0.32331	0.098	0.343	0.242	0.00002	0.38	0.799	0.32331	0.108	0.344	0.259	0	0	28
8:05:00	0.906	0.38966	0.102	0.408	0.264	0	0.41	0.863	0.4077	0.117	0.409	0.295	0	0	31
8:10:00	1.021	0.43619	0.091	0.523	0.253	0.00001	0.46	0.978	0.45215	0.102	0.524	0.277	0	0	36.4
8:15:00	1.098	0.55195	0.1	0.602	0.291	0.00002	0.5	1.056	0.56099	0.11	0.603	0.311	0	0	40.1
8:20:00	1.136	0.61426	0.104	0.64	0.31	0.00003	0.52	1.094	0.61834	0.113	0.641	0.328	0	0	41.9
8:25:00	1.153	0.64572	0.107	0.657	0.32	0.00003	0.52	1.11	0.64746	0.115	0.658	0.337	0	0	42.7
8:30:00	1.161	0.65784	0.107	0.665	0.323	0.00003	0.53	1.118	0.65869	0.115	0.666	0.339	0	0	43.1
8:35:00	1.164	0.66399	0.108	0.669	0.325	0.00003	0.53	1.122	0.66441	0.116	0.67	0.341	0	0	43.2
8:40:00	1.166	0.66647	0.108	0.671	0.326	0.00003	0.53	1.124	0.66671	0.116	0.672	0.341	0	0	43.3
8:45:00	1.167	0.66771	0.108	0.672	0.326	0.00003	0.53	1.125	0.66786	0.116	0.673	0.342	0	0	43.4
8:50:00	1.168	0.66839	0.108	0.672	0.326	0.00003	0.53	1.126	0.66848	0.116	0.673	0.342	0	0	43.4
8:55:00	1.168	0.66876	0.108	0.673	0.326	0.00003	0.53	1.126	0.66883	0.116	0.674	0.342	0	0	43.4
9:00:00	1.169	0.66894	0.108	0.673	0.326	0.00003	0.53	1.126	0.66899	0.116	0.674	0.342	0	0	43.5
9:05:00	1.132	0.61762	0.106	0.636	0.313	0.00003	0.51	1.089	0.60864	0.112	0.637	0.324	0	0	41.7
9:10:00	1.073	0.56897	0.108	0.577	0.309	0.00003	0.49	1.031	0.56024	0.115	0.578	0.32	0	0	38.9
9:15:00	1.03	0.51914	0.106	0.534	0.297	0.00002	0.47	0.988	0.51377	0.114	0.535	0.31	0	0	36.9
9:20:00	1.006	0.48547	0.104	0.51	0.286	0.00002	0.46	0.964	0.48265	0.112	0.511	0.301	0	0	35.7
9:25:00	0.994	0.46779	0.103	0.497	0.28	0.00002	0.45	0.951	0.46635	0.111	0.498	0.296	0	0	35.1
9:30:00	0.988	0.45854	0.102	0.491	0.277	0.00002	0.45	0.945	0.4578	0.111	0.491	0.293	0	0	34.8
9:35:00	0.984	0.45413	0.102	0.487	0.276	0.00002	0.45	0.942	0.45375	0.11	0.488	0.292	0	0	34.7
9:40:00	0.983	0.45153	0.101	0.486	0.275	0.00002	0.45	0.94	0.45134	0.11	0.486	0.291	0	0	34.6
9:45:00	0.982	0.45058	0.101	0.485	0.275	0.00002	0.45	0.939	0.45046	0.11	0.486	0.291	0	0	34.6
9:50:00	0.981	0.45012	0.101	0.484	0.274	0.00002	0.45	0.939	0.45002	0.11	0.485	0.291	0	0	34.5
9:55:00	0.981	0.44981	0.101	0.484	0.274	0.00002	0.45	0.938	0.44976	0.11	0.485	0.291	0	0	34.5

10:00	0.981	0.44962	0.101	0.483	0.274	0.00002	0.45	0.938	0.44958	0.11	0.484	0.291	0	0	34.5
10:05	0.947	0.41229	0.099	0.45	0.263	0.00003	0.43	0.905	0.40336	0.106	0.451	0.274	0	0	32.9
10:10:00	0.88	0.39016	0.108	0.383	0.275	0.00004	0.4	0.838	0.37924	0.115	0.384	0.285	0	0	29.8
10:15:00	0.82	0.34493	0.11	0.322	0.267	0.00003	0.37	0.777	0.33713	0.119	0.323	0.281	0	0	27
10:20:00	0.783	0.29659	0.103	0.285	0.245	0.00002	0.36	0.74	0.29257	0.113	0.286	0.26	0	0	25.3
10:25:00	0.765	0.26754	0.097	0.267	0.228	0.00002	0.35	0.723	0.26581	0.108	0.268	0.245	0	0	24.5
10:30:00	0.758	0.25462	0.094	0.259	0.219	0.00002	0.34	0.715	0.25392	0.105	0.26	0.237	0	0	24.2
10:35:00	0.755	0.24971	0.093	0.256	0.216	0.00002	0.34	0.712	0.2494	0.104	0.257	0.234	0	0	24
10:40:00	0.754	0.24763	0.092	0.255	0.215	0.00002	0.34	0.711	0.2475	0.103	0.256	0.233	0	0	24
10:45:00	0.753	0.24679	0.092	0.254	0.215	0.00002	0.34	0.71	0.24673	0.103	0.255	0.232	0	0	24
10:50:00	0.753	0.24642	0.092	0.254	0.214	0.00002	0.34	0.71	0.24639	0.103	0.255	0.232	0	0	24
10:55:00	0.753	0.24624	0.092	0.254	0.214	0.00002	0.34	0.71	0.24623	0.103	0.255	0.232	0	0	23.9
11:00:00	0.753	0.24615	0.092	0.254	0.214	0.00002	0.34	0.71	0.24614	0.103	0.255	0.232	0	0	23.9
11:00:00	0.738	0.23303	0.091	0.24	0.208	0.00002	0.34	0.696	0.22907	0.1	0.24	0.222	0	0	23.3
11:10:00	0.701	0.23418	0.101	0.203	0.225	0.00004	0.32	0.659	0.22753	0.11	0.204	0.238	0	0	21.7
11:15:00	0.658	0.22412	0.109	0.159	0.235	0.00003	0.3	0.615	0.21826	0.121	0.161	0.251	0	0	19.8
11:20:00	0.626	0.19412	0.104	0.128	0.218	0.00002	0.28	0.584	0.19082	0.117	0.129	0.236	0	0	18.4
11:25:00	0.611	0.17239	0.097	0.112	0.2	0.00002	0.28	0.569	0.17104	0.11	0.113	0.22	0	0	17.8
11:30:00	0.606	0.16233	0.093	0.106	0.191	0.00002	0.28	0.563	0.16189	0.106	0.107	0.211	0	0	17.5
11:35:00	0.604	0.15882	0.091	0.105	0.187	0.00002	0.27	0.561	0.15869	0.105	0.105	0.208	0	0	17.5
11:40:00	0.603	0.15787	0.091	0.104	0.186	0.00002	0.27	0.561	0.15777	0.105	0.105	0.207	0	0	17.4
11:45:00	0.603	0.15754	0.091	0.104	0.186	0.00002	0.27	0.561	0.15753	0.104	0.105	0.206	0	0	17.4
11:50:00	0.603	0.15747	0.091	0.104	0.186	0.00002	0.27	0.561	0.15747	0.104	0.105	0.206	0	0	17.4
11:55:00	0.603	0.15746	0.091	0.104	0.186	0.00002	0.27	0.561	0.15746	0.104	0.105	0.206	0	0	17.4
12:00:00	0.603	0.15746	0.091	0.104	0.186	0.00002	0.27	0.561	0.15746	0.104	0.105	0.206	0	0	17.4
12:05:00	0.595	0.15367	0.091	0.096	0.185	0.00002	0.27	0.553	0.15127	0.103	0.097	0.202	0	0	17.1
12:10:00	0.571	0.15118	0.097	0.071	0.193	0.00004	0.26	0.528	0.14717	0.109	0.073	0.21	0	0	16.1
12:15:00	0.542	0.14385	0.102	0.043	0.197	0.00003	0.25	0.5	0.14031	0.116	0.044	0.216	0	0	14.9
12:20:00	0.522	0.12971	0.099	0.022	0.188	0.00003	0.24	0.479	0.12762	0.115	0.023	0.209	0	0	14.1
12:25:00	0.511	0.11887	0.094	0.011	0.178	0.00003	0.23	0.468	0.11796	0.111	0.012	0.199	0	0	13.7
12:30:00	0.507	0.11348	0.092	0.007	0.171	0.00003	0.23	0.464	0.11317	0.108	0.008	0.194	0	0	13.5
12:35:00	0.505	0.11147	0.09	0.006	0.169	0.00003	0.23	0.463	0.11138	0.107	0.007	0.191	0	0	13.4
12:40:00	0.505	0.11086	0.09	0.005	0.168	0.00003	0.23	0.463	0.11084	0.107	0.006	0.191	0	0	13.4
12:45:00	0.505	0.11079	0.09	0.005	0.168	0.00003	0.23	0.462	0.11069	0.107	0.006	0.19	0	0	13.4
12:50:00	0.505	0.11066	0.09	0.005	0.168	0.00003	0.23	0.462	0.11066	0.107	0.006	0.19	0	0	13.4
12:55:00	0.505	0.11065	0.09	0.005	0.168	0.00003	0.23	0.462	0.11065	0.107	0.006	0.19	0	0	13.4
13:00:00	0.505	0.11065	0.09	0.005	0.168	0.00003	0.23	0.462	0.11065	0.107	0.006	0.19	0	0	13.4
13:05:00	0.5	0.10854	0.09	0.001	0.167	0.00003	0.23	0.458	0.10721	0.105	0.002	0.187	0	0	13.3
13:10:00	0.484	0.1049	0.092	-0.015	0.169	0.00004	0.22	0.442	0.10235	0.108	-0.014	0.188	0	0	12.6
13:15:00	0.465	0.10097	0.097	-0.035	0.173	0.00004	0.21	0.423	0.09858	0.114	-0.034	0.193	0	0	11.9
13:20:00	0.45	0.09372	0.096	-0.05	0.168	0.00003	0.2	0.407	0.09223	0.114	-0.049	0.19	0	0	11.3
13:25:00	0.441	0.08772	0.093	-0.058	0.161	0.00003	0.2	0.399	0.08705	0.112	-0.057	0.185	0	0	11
13:30:00	0.438	0.08455	0.091	-0.062	0.157	0.00003	0.2	0.396	0.08431	0.11	-0.061	0.181	0	0	10.9
13:35:00	0.437	0.08332	0.09	-0.063	0.155	0.00003	0.2	0.395	0.08322	0.11	-0.062	0.18	0	0	10.8
13:40:00	0.437	0.08298	0.09	-0.063	0.155	0.00003	0.2	0.394	0.08288	0.109	-0.062	0.179	0	0	10.8

13:45:00	0.437	0.08279	0.089	-0.063	0.155	0.00003	0.2	0.394	0.08278	0.109	-0.062	0.179	0	0	10.8
13:50:00	0.437	0.08276	0.089	-0.063	0.155	0.00003	0.2	0.394	0.08276	0.109	-0.062	0.179	0	0	10.8
13:55:00	0.437	0.08275	0.089	-0.063	0.155	0.00003	0.2	0.394	0.08275	0.109	-0.062	0.179	0	0	10.8
14:00:00	0.437	0.08275	0.089	-0.063	0.155	0.00003	0.2	0.394	0.08275	0.109	-0.062	0.179	0	0	10.8
14:00:00	0.434	0.08136	0.089	-0.066	0.153	0.00003	0.2	0.392	0.08057	0.108	-0.065	0.176	0	0	10.7
14:10:00	0.423	0.0779	0.089	-0.077	0.152	0.00004	0.19	0.381	0.07622	0.108	-0.075	0.173	0	0	10.3
14:15:00	0.409	0.07542	0.093	-0.091	0.155	0.00004	0.19	0.367	0.07377	0.112	-0.089	0.177	0	0	9.8
14:20:00	0.398	0.07143	0.093	-0.102	0.153	0.00004	0.18	0.356	0.07035	0.114	-0.101	0.176	0	0	9.4
14:25:00	0.391	0.06792	0.091	-0.109	0.148	0.00004	0.18	0.349	0.0674	0.113	-0.107	0.174	0	0	9.2
14:30:00	0.389	0.06593	0.09	-0.111	0.146	0.00004	0.18	0.346	0.06573	0.112	-0.11	0.171	0	0	9.1
14:35:00	0.388	0.06508	0.089	-0.112	0.144	0.00004	0.18	0.345	0.06502	0.111	-0.111	0.17	0	0	9
14:40:00	0.387	0.0648	0.089	-0.113	0.144	0.00004	0.18	0.345	0.06479	0.111	-0.111	0.17	0	0	9
14:45:00	0.387	0.06472	0.088	-0.113	0.144	0.00004	0.18	0.345	0.06472	0.111	-0.111	0.17	0	0	9
14:50:00	0.387	0.0647	0.088	-0.113	0.144	0.00004	0.18	0.345	0.0647	0.111	-0.111	0.17	0	0	9
14:55:00	0.387	0.0647	0.088	-0.113	0.144	0.00004	0.18	0.345	0.0647	0.111	-0.111	0.17	0	0	9
15:00:00	0.387	0.0647	0.088	-0.113	0.144	0.00004	0.18	0.345	0.0647	0.111	-0.111	0.17	0	0	9
15:00:00	0.386	0.06377	0.088	-0.114	0.142	0.00004	0.18	0.343	0.06326	0.109	-0.113	0.167	0	0	8.9
15:10:00	0.378	0.06089	0.087	-0.122	0.14	0.00005	0.17	0.336	0.05973	0.108	-0.121	0.163	0	0	8.7
15:15:00	0.367	0.05912	0.09	-0.132	0.142	0.00005	0.17	0.326	0.05793	0.111	-0.131	0.165	0	0	8.3
15:20:00	0.359	0.05672	0.09	-0.141	0.141	0.00005	0.16	0.317	0.0559	0.113	-0.14	0.166	0	0	8
15:25:00	0.353	0.05453	0.089	-0.147	0.138	0.00005	0.16	0.312	0.05412	0.113	-0.145	0.165	0	0	7.8
15:30:00	0.351	0.05319	0.088	-0.149	0.136	0.00005	0.16	0.309	0.05302	0.113	-0.147	0.163	0	0	7.8
15:35:00	0.35	0.05258	0.088	-0.15	0.135	0.00005	0.16	0.308	0.05253	0.112	-0.148	0.162	0	0	7.7
15:40:00	0.35	0.05237	0.087	-0.15	0.134	0.00005	0.16	0.308	0.05236	0.112	-0.149	0.162	0	0	7.7
15:45:00	0.35	0.05231	0.087	-0.15	0.134	0.00005	0.16	0.308	0.05231	0.112	-0.149	0.162	0	0	7.7
15:50:00	0.35	0.05229	0.087	-0.15	0.134	0.00005	0.16	0.308	0.05229	0.112	-0.149	0.162	0	0	7.7
15:55:00	0.35	0.05229	0.087	-0.15	0.134	0.00005	0.16	0.308	0.05229	0.112	-0.149	0.162	0	0	7.7
16:00:00	0.35	0.05229	0.087	-0.15	0.134	0.00005	0.16	0.308	0.05229	0.112	-0.149	0.162	0	0	7.7
16:00:00	0.349	0.05158	0.087	-0.151	0.133	0.00005	0.16	0.307	0.05126	0.111	-0.15	0.159	0	0	7.7
16:10:00	0.343	0.04921	0.085	-0.157	0.13	0.00005	0.16	0.302	0.04841	0.108	-0.155	0.154	0	0	7.5
16:15:00	0.336	0.04787	0.087	-0.164	0.131	0.00006	0.15	0.294	0.04701	0.111	-0.163	0.156	0	0	7.2
16:20:00	0.329	0.04637	0.087	-0.171	0.13	0.00006	0.15	0.287	0.04575	0.113	-0.17	0.157	0	0	7
16:25:00	0.325	0.04496	0.087	-0.175	0.129	0.00006	0.15	0.283	0.04463	0.113	-0.174	0.156	0	0	6.9
16:30:00	0.323	0.04404	0.086	-0.178	0.127	0.00006	0.15	0.281	0.04394	0.113	-0.176	0.155	0	0	6.8
16:35:00	0.322	0.0436	0.086	-0.178	0.126	0.00006	0.15	0.28	0.04355	0.113	-0.177	0.155	0	0	6.8
16:40:00	0.322	0.04343	0.086	-0.179	0.126	0.00006	0.15	0.28	0.04342	0.112	-0.177	0.154	0	0	6.8
16:45:00	0.322	0.04338	0.085	-0.179	0.126	0.00006	0.15	0.28	0.04338	0.112	-0.177	0.154	0	0	6.8
16:50:00	0.322	0.04337	0.085	-0.179	0.126	0.00006	0.15	0.28	0.04336	0.112	-0.177	0.154	0	0	6.8
16:55:00	0.322	0.04336	0.085	-0.179	0.126	0.00006	0.15	0.28	0.04336	0.112	-0.177	0.154	0	0	6.8
17:00:00	0.322	0.04336	0.085	-0.179	0.126	0.00006	0.15	0.28	0.04336	0.112	-0.177	0.154	0	0	6.8
17:00:00	0.321	0.04296	0.085	-0.179	0.125	0.00006	0.15	0.279	0.04266	0.111	-0.178	0.152	0	0	6.7
17:10:00	0.317	0.04101	0.083	-0.184	0.122	0.00006	0.14	0.275	0.04041	0.108	-0.182	0.147	0	0	6.6
17:15:00	0.31	0.03995	0.084	-0.19	0.122	0.00007	0.14	0.269	0.03927	0.11	-0.188	0.148	0	0	6.4
17:20:00	0.305	0.03892	0.085	-0.196	0.122	0.00007	0.14	0.263	0.03842	0.112	-0.194	0.149	0	0	6.2
17:25:00	0.301	0.03793	0.085	-0.199	0.121	0.00007	0.14	0.26	0.03765	0.113	-0.197	0.149	0	0	6.1

17:30:00	0.299	0.03724	0.085	-0.201	0.12	0.00007	0.14	0.258	0.03712	0.113	-0.199	0.149	0	0	6.1
17:35:00	0.299	0.03689	0.084	-0.202	0.119	0.00007	0.14	0.257	0.03685	0.113	-0.2	0.148	0	0	6
17:40:00	0.298	0.03676	0.084	-0.202	0.119	0.00007	0.14	0.257	0.03675	0.113	-0.2	0.148	0	0	6
17:45:00	0.298	0.03672	0.084	-0.202	0.119	0.00007	0.14	0.257	0.03671	0.113	-0.2	0.148	0	0	6
17:50:00	0.298	0.03671	0.084	-0.202	0.119	0.00007	0.14	0.257	0.03671	0.113	-0.2	0.148	0	0	6
17:55:00	0.298	0.0367	0.084	-0.202	0.119	0.00007	0.14	0.257	0.0367	0.113	-0.2	0.148	0	0	6
18:00:00	0.298	0.0367	0.084	-0.202	0.119	0.00007	0.14	0.257	0.0367	0.113	-0.2	0.148	0	0	6
18:05:00	0.294	0.03447	0.081	-0.206	0.114	0.00007	0.13	0.253	0.03331	0.106	-0.204	0.137	0	0	5.9
18:10:00	0.272	0.02371	0.065	-0.229	0.088	0.00009	0.12	0.231	0.02057	0.078	-0.227	0.097	0	0	5.2
18:15:00	0.236	0.01525	0.055	-0.265	0.07	0.00014	0.11	0.196	0.01175	0.061	-0.262	0.07	0	0	4.2
18:20:00	0.199	0.00883	0.045	-0.302	0.052	0.00025	0.09	0.161	0.00589	0.045	-0.297	0.047	0	0	3.2
18:25:00	0.168	0.00459	0.033	-0.333	0.035	0.00047	0.08	0.135	0.00251	0.029	-0.323	0.026	0	0	2.4
18:30:00	0.145	0.00189	0.018	-0.356	0.018	0.00084	0.07	0.12	0.00084	0.012	-0.338	0.011	0	0	2
18:35:00	0.132	0.00092	0.011	-0.369	0.01	0.00121	0.06	0.115	0.00034	0.006	-0.343	0.005	0	0	1.8
18:40:00	0.122	0.00052	0.007	-0.379	0.006	0.00152	0.06	0.112	0.00019	0.003	-0.346	0.003	0	0	1.6
18:45:00	0.117	0.00028	0.004	-0.384	0.004	0.00172	0.05	0.111	0.00012	0.002	-0.347	0.002	0	0	1.6
18:50:00	0.114	0.00017	0.003	-0.387	0.002	0.00183	0.05	0.111	0.00009	0.002	-0.347	0.001	0	0	1.5
18:55:00	0.112	0.00011	0.002	-0.389	0.002	0.00189	0.05	0.11	0.00008	0.001	-0.348	0.001	0	0	1.5
19:00:00	0.112	0.00009	0.002	-0.389	0.001	0.00192	0.05	0.11	0.00007	0.001	-0.348	0.001	0	0	1.5
19:05:00	0.111	0.00007	0.001	-0.39	0.001	0.00193	0.05	0.11	0.00006	0.001	-0.348	0.001	0	0	1.5
19:10:00	0.111	0.00004	0.001	-0.39	0.001	0.00194	0.05	0.11	0.00004	0.001	-0.348	0.001	0	0	1.5
19:15:00	0.111	0.00002	0	-0.39	0	0.00195	0.05	0.11	0.00001	0	-0.348	0	0	0	1.5
19:20:00	0.111	0.00001	0	-0.39	0	0.00195	0.05	0.11	0	0	-0.348	0	0	0	1.5
19:25:00	0.111	0.00001	0	-0.39	0	0.00196	0.05	0.11	0	0	-0.348	0	0	0	1.5
19:30:00	0.111	0	0	-0.39	0	0.00196	0.05	0.11	0	0	-0.348	0	0	0	1.5
19:35:00	0.11	0	0	-0.391	0	0.00197	0.05	0.11	0	0	-0.348	0	0	0	1.5
19:40:00	0.11	0	0	-0.391	0	0.00197	0.05	0.11	0	0	-0.348	0	0	0	1.5
19:45:00	0.11	0	0	-0.391	0	0.00197	0.05	0.11	0	0	-0.348	0	0	0	1.5
19:50:00	0.11	0	0	-0.391	0	0.00197	0.05	0.11	0	0	-0.348	0	0	0	1.5
19:55:00	0.11	0	0	-0.391	0	0.00197	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:00:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:05:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:10:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:15:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:20:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:25:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:30:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:35:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:40:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:45:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:50:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
20:55:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:00:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:05:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5

21:15:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:20:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:25:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:30:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:35:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:40:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:45:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:50:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
21:55:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:00:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:05:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:10:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:15:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:20:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:25:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:30:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:35:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:40:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:45:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:50:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
22:55:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:00:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:05:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:10:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:15:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:20:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:25:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:30:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:35:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:40:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:45:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:50:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
23:55:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5
0:00:00	0.11	0	0	-0.391	0	0.00198	0.05	0.11	0	0	-0.348	0	0	0	1.5

JLL55

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.316
Depth (m)	0.300
Base Elevation (m)	3.016
Top Area (m²)	464.75
Side Slope (%)	29.2
Base Area (m²)	360.72
Freeboard (mm)	0
Porosity (%)	100
Length (m)	50.565
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	165.527

Filter Area

Base Elevation (m)	2.516

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (3)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	115.397
Top Perimeter (m)	119.512

JLL56

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.524
Depth (m)	0.300
Base Elevation (m)	3.224
Top Area (m²)	1117.80
Side Slope (%)	31.5
Base Area (m²)	885.78
Freeboard (mm)	0
Porosity (%)	100
Length (m)	121.848
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	402.626

Filter Area

Base Elevation (m)	2.724

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (4)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	258.235
Top Perimeter (m)	262.043

JLL57 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.491
Depth (m)	0.300
Base Elevation (m)	3.191
Top Area (m²)	1020.94
Side Slope (%)	31.4
Base Area (m²)	807.87
Freeboard (mm)	0
Porosity (%)	100
Length (m)	111.352
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	367.451

Filter Area

Base Elevation (m)	2.691

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (5)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	237.215
Top Perimeter (m)	241.042

JLL58 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.270
Depth (m)	0.300
Base Elevation (m)	2.970
Top Area (m²)	542.74
Side Slope (%)	30.0
Base Area (m²)	423.22
Freeboard (mm)	0
Porosity (%)	100
Length (m)	59.713
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	193.788

Filter Area

Base Elevation (m)	2.470

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (6)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	133.601
Top Perimeter (m)	137.604

JLL2 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.493
Depth (m)	0.300
Base Elevation (m)	3.193
Top Area (m²)	55.39
Side Slope (%)	38.5
Base Area (m²)	16.26
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.5
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	12.767

Filter Area

Base Elevation (m)	2.693

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (1)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (50)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (2)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.544
Top Perimeter (m)	54.659

JLL1

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.190
Depth (m)	0.300
Base Elevation (m)	2.890
Top Area (m²)	62.51
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.5
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.833

Filter Area

Base Elevation (m)	2.390

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (1)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (51)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (2)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.543
Top Perimeter (m)	55.226

JLL3 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.818
Depth (m)	0.300
Base Elevation (m)	3.518
Top Area (m²)	62.51
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.838

Filter Area

Base Elevation (m)	3.018

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (3)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (49)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (7)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.543
Top Perimeter (m)	55.226

JLL4

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.680
Depth (m)	0.300
Base Elevation (m)	3.380
Top Area (m²)	62.51
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.838

Filter Area

Base Elevation (m)	2.880

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (4)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (8)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (48)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.543
Top Perimeter (m)	55.226

JLL5 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.542
Depth (m)	0.300
Base Elevation (m)	3.242
Top Area (m²)	62.51
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.838

Filter Area

Base Elevation (m)	2.742

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (5)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (47)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (9)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.543
Top Perimeter (m)	55.226

JLL6

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.386
Depth (m)	0.300
Base Elevation (m)	3.086
Top Area (m²)	72.30
Side Slope (%)	32.7
Base Area (m²)	18.99
Freeboard (mm)	0
Porosity (%)	100
Length (m)	29.021
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	16.056

Filter Area

Base Elevation (m)	2.586

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (6)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (46)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (10)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	59.351
Top Perimeter (m)	63.025

JLL7 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.220
Depth (m)	0.300
Base Elevation (m)	2.920
Top Area (m²)	62.51
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.838

Filter Area

Base Elevation (m)	2.420

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (7)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (11)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (43)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.543
Top Perimeter (m)	55.226

JLL8

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.082
Depth (m)	0.300
Base Elevation (m)	2.782
Top Area (m²)	62.51
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.838

Filter Area

Base Elevation (m)	2.282

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (8)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (12)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (42)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.543
Top Perimeter (m)	55.226

JLL9 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.048
Depth (m)	0.300
Base Elevation (m)	2.748
Top Area (m²)	62.51
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.838

Filter Area

Base Elevation (m)	2.248

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (9)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (41)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (13)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.543
Top Perimeter (m)	55.226

JLL10

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.064
Depth (m)	0.300
Base Elevation (m)	2.764
Top Area (m²)	60.51
Side Slope (%)	32.6
Base Area (m²)	15.69
Freeboard (mm)	0
Porosity (%)	100
Length (m)	24.327
Long. Slope (%)	0.45
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.384

Filter Area

Base Elevation (m)	2.264

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (40)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (14)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (10)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	49.945
Top Perimeter (m)	53.630

JLL22 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.561
Depth (m)	0.300
Base Elevation (m)	3.261
Top Area (m²)	121.23
Side Slope (%)	34.5
Base Area (m²)	50.43
Freeboard (mm)	0
Porosity (%)	100
Length (m)	40.715
Long. Slope (%)	0.6
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	31.698

Filter Area

Base Elevation (m)	2.761

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (22)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (27)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	83.907
Top Perimeter (m)	87.385

JLL23

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.678
Depth (m)	0.300
Base Elevation (m)	3.378
Top Area (m²)	67.44
Side Slope (%)	31.5
Base Area (m²)	30.38
Freeboard (mm)	0
Porosity (%)	100
Length (m)	19.426
Long. Slope (%)	0.42
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	18.286

Filter Area

Base Elevation (m)	2.878

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (15)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (23)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	41.979
Top Perimeter (m)	45.794

JLL11 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.180
Depth (m)	0.300
Base Elevation (m)	2.880
Top Area (m²)	226.31
Side Slope (%)	32.6
Base Area (m²)	120.46
Freeboard (mm)	0
Porosity (%)	100
Length (m)	57.517
Long. Slope (%)	0.33
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	66.140

Filter Area

Base Elevation (m)	2.380

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (16)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (12)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (11)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	119.222
Top Perimeter (m)	122.903

JLL12

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.476
Depth (m)	0.300
Base Elevation (m)	3.176
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.9
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.778

Filter Area

Base Elevation (m)	2.676

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (17)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (13)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL13 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.915
Depth (m)	0.300
Base Elevation (m)	3.615
Top Area (m²)	40.00
Side Slope (%)	32.3
Base Area (m²)	9.94
Freeboard (mm)	0
Porosity (%)	100
Length (m)	16.194
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	8.734

Filter Area

Base Elevation (m)	3.115

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (14)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (18)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	33.616
Top Perimeter (m)	37.328

JLL14

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.978
Depth (m)	0.300
Base Elevation (m)	3.678
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	3.178

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (19)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL15 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.847
Depth (m)	0.300
Base Elevation (m)	3.547
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	3.047

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (20)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (15)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL16

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.697
Depth (m)	0.300
Base Elevation (m)	3.397
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	2.897

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (21)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (16)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL17 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.525
Depth (m)	0.300
Base Elevation (m)	3.225
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	2.725

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (22)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (17)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL18

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.339
Depth (m)	0.300
Base Elevation (m)	3.039
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	2.539

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (23)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (18)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL19 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.211
Depth (m)	0.300
Base Elevation (m)	2.911
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	2.411

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (19)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (24)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL20

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.186
Depth (m)	0.300
Base Elevation (m)	2.886
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	2.386

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (25)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (20)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL21 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.247
Depth (m)	0.300
Base Elevation (m)	2.947
Top Area (m²)	40.00
Side Slope (%)	32.3
Base Area (m²)	9.94
Freeboard (mm)	0
Porosity (%)	100
Length (m)	16.194
Long. Slope (%)	0.32
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	8.734

Filter Area

Base Elevation (m)	2.447

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (26)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (21)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	33.616
Top Perimeter (m)	37.328

JLL25

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.935
Depth (m)	0.300
Base Elevation (m)	3.635
Top Area (m²)	52.22
Side Slope (%)	32.9
Base Area (m²)	11.89
Freeboard (mm)	0
Porosity (%)	100
Length (m)	22.127
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	11.121

Filter Area

Base Elevation (m)	3.135

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (29)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (24)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (112)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	45.330
Top Perimeter (m)	48.975

JLL26 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.894
Depth (m)	0.300
Base Elevation (m)	3.594
Top Area (m²)	55.00
Side Slope (%)	32.5
Base Area (m²)	14.14
Freeboard (mm)	0
Porosity (%)	100
Length (m)	22.154
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	12.133

Filter Area

Base Elevation (m)	3.094

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (30)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (111)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (25)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	45.584
Top Perimeter (m)	49.272

JLL27

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.906
Depth (m)	0.300
Base Elevation (m)	3.606
Top Area (m²)	55.00
Side Slope (%)	32.5
Base Area (m²)	14.14
Freeboard (mm)	0
Porosity (%)	100
Length (m)	22.154
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	12.133

Filter Area

Base Elevation (m)	3.106

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (31)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (110)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (26)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	45.584
Top Perimeter (m)	49.272

JLL28 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.994
Depth (m)	0.300
Base Elevation (m)	3.694
Top Area (m²)	55.00
Side Slope (%)	32.5
Base Area (m²)	14.14
Freeboard (mm)	0
Porosity (%)	100
Length (m)	22.154
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	12.133

Filter Area

Base Elevation (m)	3.194

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (32)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (109)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (27)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	45.584
Top Perimeter (m)	49.272

JLL24

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	4.124
Depth (m)	0.300
Base Elevation (m)	3.824
Top Area (m²)	75.67
Side Slope (%)	36.9
Base Area (m²)	28.65
Freeboard (mm)	0
Porosity (%)	100
Length (m)	28.929
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	19.119

Filter Area

Base Elevation (m)	3.324

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (28)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (93)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (94)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	59.839
Top Perimeter (m)	63.090

JLL39 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	4.376
Depth (m)	0.300
Base Elevation (m)	4.076
Top Area (m²)	141.74
Side Slope (%)	34.3
Base Area (m²)	73.23
Freeboard (mm)	0
Porosity (%)	100
Length (m)	39.121
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	40.881

Filter Area

Base Elevation (m)	3.576

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (65)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (33)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (64)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	81.986
Top Perimeter (m)	85.488

JLL40

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.914
Depth (m)	0.300
Base Elevation (m)	3.614
Top Area (m²)	249.44
Side Slope (%)	35.4
Base Area (m²)	137.57
Freeboard (mm)	0
Porosity (%)	100
Length (m)	65.915
Long. Slope (%)	0.17
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	74.275

Filter Area

Base Elevation (m)	3.114

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (67)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (66)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (34)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	136.003
Top Perimeter (m)	139.398

JLL41 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.754
Depth (m)	0.300
Base Elevation (m)	3.454
Top Area (m²)	117.41
Side Slope (%)	37.6
Base Area (m²)	53.36
Freeboard (mm)	0
Porosity (%)	100
Length (m)	40.165
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	31.967

Filter Area

Base Elevation (m)	2.954

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (68)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (35)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (69)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	82.987
Top Perimeter (m)	86.176

JLL29

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	4.147
Depth (m)	0.300
Base Elevation (m)	3.847
Top Area (m²)	49.61
Side Slope (%)	38.2
Base Area (m²)	10.13
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	10.282

Filter Area

Base Elevation (m)	3.347

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (44)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (55)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (108)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.056
Top Perimeter (m)	54.199

JLL30 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	4.152
Depth (m)	0.300
Base Elevation (m)	3.852
Top Area (m²)	82.88
Side Slope (%)	35.2
Base Area (m²)	19.91
Freeboard (mm)	0
Porosity (%)	100
Length (m)	36.928
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	17.917

Filter Area

Base Elevation (m)	3.352

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (45)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (56)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (107)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	74.935
Top Perimeter (m)	78.345

JLL31

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.999
Depth (m)	0.300
Base Elevation (m)	3.699
Top Area (m²)	62.24
Side Slope (%)	34.0
Base Area (m²)	15.69
Freeboard (mm)	0
Porosity (%)	100
Length (m)	26.366
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.655

Filter Area

Base Elevation (m)	3.199

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (46)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (57)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (106)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	53.922
Top Perimeter (m)	57.453

JLL32 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.776
Depth (m)	0.300
Base Elevation (m)	3.476
Top Area (m²)	62.52
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.141
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.839

Filter Area

Base Elevation (m)	2.976

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (47)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (105)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (58)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.574
Top Perimeter (m)	55.255

JLL33

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.607
Depth (m)	0.300
Base Elevation (m)	3.307
Top Area (m²)	62.54
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.156
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.843

Filter Area

Base Elevation (m)	2.807

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (48)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (104)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (59)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.605
Top Perimeter (m)	55.285

JLL34 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.533
Depth (m)	0.300
Base Elevation (m)	3.233
Top Area (m²)	62.54
Side Slope (%)	32.6
Base Area (m²)	16.25
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.161
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.842

Filter Area

Base Elevation (m)	2.733

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (49)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (60)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (103)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.614
Top Perimeter (m)	55.293

JLL35

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.536
Depth (m)	0.300
Base Elevation (m)	3.236
Top Area (m²)	98.95
Side Slope (%)	34.8
Base Area (m²)	24.49
Freeboard (mm)	0
Porosity (%)	100
Length (m)	43.226
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	21.553

Filter Area

Base Elevation (m)	2.736

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (50)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (61)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (102)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	87.586
Top Perimeter (m)	91.031

JLL42 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	4.142
Depth (m)	0.300
Base Elevation (m)	3.842
Top Area (m²)	89.32
Side Slope (%)	43.9
Base Area (m²)	39.35
Freeboard (mm)	0
Porosity (%)	100
Length (m)	36.530
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	24.033

Filter Area

Base Elevation (m)	3.342

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (71)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (36)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (72)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	75.214
Top Perimeter (m)	77.950

JLL36

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.547
Depth (m)	0.300
Base Elevation (m)	3.247
Top Area (m²)	101.32
Side Slope (%)	37.6
Base Area (m²)	23.79
Freeboard (mm)	0
Porosity (%)	100
Length (m)	48.558
Long. Slope (%)	0.27
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	21.789

Filter Area

Base Elevation (m)	2.747

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (51)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (97)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (98)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	98.096
Top Perimeter (m)	101.290

JLL37 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.814
Depth (m)	0.300
Base Elevation (m)	3.514
Top Area (m²)	88.51
Side Slope (%)	34.5
Base Area (m²)	22.33
Freeboard (mm)	0
Porosity (%)	100
Length (m)	38.000
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	19.405

Filter Area

Base Elevation (m)	3.014

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (100)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (60)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (62)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	77.175
Top Perimeter (m)	80.659

JLL38

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	4.085
Depth (m)	0.300
Base Elevation (m)	3.785
Top Area (m²)	82.52
Side Slope (%)	32.7
Base Area (m²)	21.85
Freeboard (mm)	0
Porosity (%)	100
Length (m)	33.103
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	18.363

Filter Area

Base Elevation (m)	3.285

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (52)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (99)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (63)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	67.525
Top Perimeter (m)	71.191

JLL43 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	4.230
Depth (m)	0.300
Base Elevation (m)	3.930
Top Area (m²)	102.93
Side Slope (%)	37.5
Base Area (m²)	38.00
Freeboard (mm)	0
Porosity (%)	100
Length (m)	40.545
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	25.726

Filter Area

Base Elevation (m)	3.430

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (74)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (73)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (37)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	82.964
Top Perimeter (m)	86.167

JLL45

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.558
Depth (m)	0.300
Base Elevation (m)	3.258
Top Area (m²)	302.21
Side Slope (%)	34
Base Area (m²)	193.62
Freeboard (mm)	0
Porosity (%)	100
Length (m)	61.533
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	96.865

Filter Area

Base Elevation (m)	2.758

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (80)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (39)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (79)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (3)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (78)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	129.359
Top Perimeter (m)	132.888

JLL46

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.531
Depth (m)	0.300
Base Elevation (m)	3.231
Top Area (m²)	162.92
Side Slope (%)	36
Base Area (m²)	89.26
Freeboard (mm)	0
Porosity (%)	100
Length (m)	44.196
Long. Slope (%)	0.25
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	48.315

Filter Area

Base Elevation (m)	2.731

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (81)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (40)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (82)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	92.432
Top Perimeter (m)	95.765

JLL48 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.566
Depth (m)	0.300
Base Elevation (m)	3.266
Top Area (m²)	209.68
Side Slope (%)	34
Base Area (m²)	123.29
Freeboard (mm)	0
Porosity (%)	100
Length (m)	48.954
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	64.350

Filter Area

Base Elevation (m)	2.766

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (87)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (88)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (41)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (3)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (83)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	102.945
Top Perimeter (m)	106.475

JLL49

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.818
Depth (m)	0.300
Base Elevation (m)	3.518
Top Area (m²)	133.75
Side Slope (%)	18.8
Base Area (m²)	26.50
Freeboard (mm)	0
Porosity (%)	100
Length (m)	33.614
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	27.281

Filter Area

Base Elevation (m)	3.018

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (89)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (90)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (42)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	68.804
Top Perimeter (m)	75.185

JLL50 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	4.195
Depth (m)	0.300
Base Elevation (m)	3.895
Top Area (m²)	119.01
Side Slope (%)	34.9
Base Area (m²)	64.15
Freeboard (mm)	0
Porosity (%)	100
Length (m)	31.923
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	35.041

Filter Area

Base Elevation (m)	3.395

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (92)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (43)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (91)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	67.865
Top Perimeter (m)	71.302

JLL60

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.189
Depth (m)	0.300
Base Elevation (m)	2.889
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	2.389

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (54)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (57)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL61 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.325
Depth (m)	0.300
Base Elevation (m)	3.025
Top Area (m²)	62.50
Side Slope (%)	32.6
Base Area (m²)	16.24
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.125
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.834

Filter Area

Base Elevation (m)	2.525

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (58)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (52)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (53)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.542
Top Perimeter (m)	55.225

JLL59

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.118
Depth (m)	0.300
Base Elevation (m)	2.818
Top Area (m²)	156.02
Side Slope (%)	30.05
Base Area (m²)	103.85
Freeboard (mm)	0
Porosity (%)	100
Length (m)	26.132
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	51.084

Filter Area

Base Elevation (m)	2.318

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (120)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (121)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	60.211
Top Perimeter (m)	64.204

JLL62 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.786
Depth (m)	0.250
Base Elevation (m)	2.536
Top Area (m²)	60.00
Side Slope (%)	40.7
Base Area (m²)	23.04
Freeboard (mm)	0
Porosity (%)	100
Length (m)	30.067
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.211

Filter Area

Base Elevation (m)	2.036

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (53)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (85)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	61.666
Top Perimeter (m)	64.124

JLL63

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.083
Depth (m)	0.250
Base Elevation (m)	2.833
Top Area (m²)	60.00
Side Slope (%)	40.7
Base Area (m²)	23.04
Freeboard (mm)	0
Porosity (%)	100
Length (m)	30.067
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.211

Filter Area

Base Elevation (m)	2.333

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (54)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (86)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	61.666
Top Perimeter (m)	64.124

JLL64 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.466
Depth (m)	0.250
Base Elevation (m)	3.216
Top Area (m²)	60.00
Side Slope (%)	40.7
Base Area (m²)	23.04
Freeboard (mm)	0
Porosity (%)	100
Length (m)	30.067
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	13.211

Filter Area

Base Elevation (m)	2.716

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (61)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (122)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	61.666
Top Perimeter (m)	64.124

JLL65

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.502
Depth (m)	0.250
Base Elevation (m)	3.252
Top Area (m²)	37.92
Side Slope (%)	43.9
Base Area (m²)	12.70
Freeboard (mm)	0
Porosity (%)	100
Length (m)	22.158
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	7.925

Filter Area

Base Elevation (m)	2.752

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (62)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (123)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	45.463
Top Perimeter (m)	47.739

ZBIO1 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.638
Depth (m)	0.500
Base Elevation (m)	2.138
Top Area (m²)	176.95
Side Slope (%)	30
Base Area (m²)	98.13
Freeboard (mm)	0
Porosity (%)	100
Length (m)	23.644
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	87.561

Filter Area

Base Elevation (m)	1.138

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	800	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (44)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (45)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (3)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (55)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	55.588
Top Perimeter (m)	62.255

BJLL-2

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.165
Depth (m)	0.350
Base Elevation (m)	2.815
Top Area (m²)	393.92
Side Slope (%)	20
Base Area (m²)	212.95
Freeboard (mm)	0
Porosity (%)	100
Length (m)	51.707
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	131.010

Filter Area

Base Elevation (m)	2.315

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Point Inflow
Incoming Item(s)	CZV (63)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	111.650
Top Perimeter (m)	118.650

BJLL-3

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.500
Depth (m)	0.400
Base Elevation (m)	3.100
Top Area (m²)	139.97
Side Slope (%)	22
Base Area (m²)	30.72
Freeboard (mm)	0
Porosity (%)	100
Length (m)	30.045
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	37.855

Filter Area

Base Elevation (m)	2.600

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (64)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	62.135
Top Perimeter (m)	69.408

Ponding Area

Exceedance Elevation (m)	3.500
Depth (m)	0.400
Base Elevation (m)	3.100
Top Area (m²)	283.97
Side Slope (%)	22
Base Area (m²)	73.46
Freeboard (mm)	0
Porosity (%)	100
Length (m)	57.892
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	80.284

Filter Area

Base Elevation (m)	2.600

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Point Inflow
Incoming Item(s)	CIMP (131)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (65)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	118.321
Top Perimeter (m)	125.594

BJLL-5 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.400
Depth (m)	0.350
Base Elevation (m)	3.050
Top Area (m²)	212.41
Side Slope (%)	21
Base Area (m²)	34.66
Freeboard (mm)	0
Porosity (%)	100
Length (m)	53.326
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	47.552

Filter Area

Base Elevation (m)	2.550

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (66)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Point Inflow
Incoming Item(s)	CIMP (132)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	107.952
Top Perimeter (m)	114.618

BJLL-9

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.400
Depth (m)	0.350
Base Elevation (m)	3.050
Top Area (m²)	266.009
Side Slope (%)	22
Base Area (m²)	100.42
Freeboard (mm)	0
Porosity (%)	100
Length (m)	52.043
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	75.993

Filter Area

Base Elevation (m)	2.550

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (70)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	107.946
Top Perimeter (m)	114.309

BJLL-10 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.250
Depth (m)	0.350
Base Elevation (m)	2.900
Top Area (m²)	258.35
Side Slope (%)	20
Base Area (m²)	90.77
Freeboard (mm)	0
Porosity (%)	100
Length (m)	47.880
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	71.830

Filter Area

Base Elevation (m)	2.400

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (71)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	99.552
Top Perimeter (m)	106.552

Ponding Area

Exceedance Elevation (m)	2.700
Depth (m)	0.400
Base Elevation (m)	2.300
Top Area (m²)	490.79
Side Slope (%)	19
Base Area (m²)	232.55
Freeboard (mm)	0
Porosity (%)	100
Length (m)	61.331
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	171.779

Filter Area

Base Elevation (m)	1.800

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (134)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	130.246
Top Perimeter (m)	138.667

BJLL-8

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.700
Depth (m)	0.350
Base Elevation (m)	3.350
Top Area (m²)	208.14
Side Slope (%)	18
Base Area (m²)	109.16
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.452
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	68.238

Filter Area

Base Elevation (m)	2.850

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (67)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	59.482
Top Perimeter (m)	67.260

BJLL-1

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.300
Depth (m)	0.400
Base Elevation (m)	2.900
Top Area (m²)	445.42
Side Slope (%)	20
Base Area (m²)	276.66
Freeboard (mm)	0
Porosity (%)	100
Length (m)	42.191
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	176.492

Filter Area

Base Elevation (m)	2.400

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (56)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	97.497
Top Perimeter (m)	105.497

BJLL-6

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.400
Depth (m)	0.350
Base Elevation (m)	3.050
Top Area (m²)	145.42
Side Slope (%)	19
Base Area (m²)	61.38
Freeboard (mm)	0
Porosity (%)	100
Length (m)	22.811
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	43.390

Filter Area

Base Elevation (m)	2.550

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (68)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	51.003
Top Perimeter (m)	58.372

BJLL-7

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.500
Depth (m)	0.300
Base Elevation (m)	3.200
Top Area (m²)	132.78
Side Slope (%)	20
Base Area (m²)	62.12
Freeboard (mm)	0
Porosity (%)	100
Length (m)	23.552
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	36.524

Filter Area

Base Elevation (m)	2.700

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (69)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	52.380
Top Perimeter (m)	58.380

BJLL-16 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.600
Depth (m)	0.450
Base Elevation (m)	2.150
Top Area (m²)	234.85
Side Slope (%)	20
Base Area (m²)	87.02
Freeboard (mm)	0
Porosity (%)	100
Length (m)	32.851
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	82.631

Filter Area

Base Elevation (m)	1.650

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (76)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	71.000
Top Perimeter (m)	80.000

BJLL-13 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.300
Depth (m)	0.350
Base Elevation (m)	1.950
Top Area (m²)	427.66
Side Slope (%)	17
Base Area (m²)	292.42
Freeboard (mm)	0
Porosity (%)	100
Length (m)	32.845
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	159.836

Filter Area

Base Elevation (m)	1.450

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (87)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	83.496
Top Perimeter (m)	91.731

BJLL-12 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.500
Depth (m)	0.350
Base Elevation (m)	3.150
Top Area (m²)	167.83
Side Slope (%)	21
Base Area (m²)	55.87
Freeboard (mm)	0
Porosity (%)	100
Length (m)	33.587
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	45.781

Filter Area

Base Elevation (m)	2.650

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (72)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	70.501
Top Perimeter (m)	77.167

BJLL-14 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.900
Depth (m)	0.350
Base Elevation (m)	2.550
Top Area (m²)	316.03
Side Slope (%)	17
Base Area (m²)	169.10
Freeboard (mm)	0
Porosity (%)	100
Length (m)	35.684
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	104.564

Filter Area

Base Elevation (m)	2.050

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (73)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (3)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (74)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	80.845
Top Perimeter (m)	89.080

BJLL-19

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.700
Depth (m)	0.400
Base Elevation (m)	2.300
Top Area (m²)	247.89
Side Slope (%)	18
Base Area (m²)	111.76
Freeboard (mm)	0
Porosity (%)	100
Length (m)	30.629
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	84.970

Filter Area

Base Elevation (m)	1.800

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (81)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	68.556
Top Perimeter (m)	77.444

BJLL-15 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.500
Depth (m)	0.350
Base Elevation (m)	2.150
Top Area (m²)	523.79
Side Slope (%)	19
Base Area (m²)	159.48
Freeboard (mm)	0
Porosity (%)	100
Length (m)	98.884
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	138.362

Filter Area

Base Elevation (m)	1.650

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (75)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	200.995
Top Perimeter (m)	208.363

Ponding Area

Exceedance Elevation (m)	2.676
Depth (m)	0.400
Base Elevation (m)	2.276
Top Area (m²)	467.49
Side Slope (%)	18
Base Area (m²)	297.36
Freeboard (mm)	0
Porosity (%)	100
Length (m)	38.281
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	187.402

Filter Area

Base Elevation (m)	1.776

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (78)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	92.098
Top Perimeter (m)	100.987

BJLL-27

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.300
Depth (m)	0.300
Base Elevation (m)	3.000
Top Area (m²)	262.32
Side Slope (%)	33
Base Area (m²)	93.86
Freeboard (mm)	0
Porosity (%)	100
Length (m)	92.652
Long. Slope (%)	0.1
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	64.793

Filter Area

Base Elevation (m)	2.500

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (79)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	187.330
Top Perimeter (m)	190.966

BJLL-18

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.471
Depth (m)	0.350
Base Elevation (m)	2.121
Top Area (m²)	283.84
Side Slope (%)	19
Base Area (m²)	171.19
Freeboard (mm)	0
Porosity (%)	100
Length (m)	30.578
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	99.500

Filter Area

Base Elevation (m)	1.621

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (77)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	72.353
Top Perimeter (m)	79.721

BJLL-20

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.678
Depth (m)	0.350
Base Elevation (m)	2.328
Top Area (m²)	250.11
Side Slope (%)	17
Base Area (m²)	145.31
Freeboard (mm)	0
Porosity (%)	100
Length (m)	25.453
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	86.065

Filter Area

Base Elevation (m)	1.828

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (80)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	62.323
Top Perimeter (m)	70.558

BJLL-21

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.600
Depth (m)	0.350
Base Elevation (m)	2.250
Top Area (m²)	512.36
Side Slope (%)	20
Base Area (m²)	289.89
Freeboard (mm)	0
Porosity (%)	100
Length (m)	63.562
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	173.955

Filter Area

Base Elevation (m)	1.750

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (82)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (84)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	136.245
Top Perimeter (m)	143.245

BJLL-25 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.800
Depth (m)	0.350
Base Elevation (m)	3.450
Top Area (m²)	268.96
Side Slope (%)	20
Base Area (m²)	121.12
Freeboard (mm)	0
Porosity (%)	100
Length (m)	42.240
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	82.410

Filter Area

Base Elevation (m)	2.950

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (83)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	90.215
Top Perimeter (m)	97.215

BJLL-17 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.500
Depth (m)	0.350
Base Elevation (m)	2.150
Top Area (m²)	122.42
Side Slope (%)	19
Base Area (m²)	50.55
Freeboard (mm)	0
Porosity (%)	100
Length (m)	19.508
Long. Slope (%)	0.2
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	36.204

Filter Area

Base Elevation (m)	1.650

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (85)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	44.198
Top Perimeter (m)	51.566

BJLL-22

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.800
Depth (m)	0.400
Base Elevation (m)	2.400
Top Area (m²)	727.65
Side Slope (%)	19
Base Area (m²)	354.97
Freeboard (mm)	0
Porosity (%)	100
Length (m)	88.511
Long. Slope (%)	0.15
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	257.865

Filter Area

Base Elevation (m)	1.900

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (86)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	185.043
Top Perimeter (m)	193.464

BJLL-23

Type : Bioretention

Ponding Area

Exceedance Elevation (m)	2.600
Depth (m)	0.300
Base Elevation (m)	2.300
Top Area (m²)	420.96
Side Slope (%)	20
Base Area (m²)	152.19
Freeboard (mm)	0
Porosity (%)	100
Length (m)	89.590
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	103.699

Filter Area

Base Elevation (m)	1.800

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (88)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	182.578
Top Perimeter (m)	188.578

BJLL-24 Type : Bioretention

Ponding Area

Exceedance Elevation (m)	3.200
Depth (m)	0.400
Base Elevation (m)	2.800
Top Area (m²)	273.60
Side Slope (%)	20
Base Area (m²)	118.06
Freeboard (mm)	0
Porosity (%)	100
Length (m)	38.884
Long. Slope (%)	0.4
Filtration Rate (m/hr)	0.1
Friction Scheme	Manning's n
n	0.3
Total Volume (m³)	92.123

Filter Area

Base Elevation (m)	2.300

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Friction Scheme	Manning's n
n	0.015
Release Height (m)	0.000

Filtration Layers

Use	Name	Filtration Layer Depth (mm)	Porosity (%)	Conductivity (m/hr)	Soil Type
☑	Soil	300	15	0.1	Soil Type
	Storage	200	35	300.0	

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CZV (89)
Bypass Destination	(None)
Inlet Destination	Ponding Area
Capacity Type	No Restriction

Advanced

Ponding Area

Base Perimeter (m)	83.841
Top Perimeter (m)	91.841

PP2

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.912
Depth (m)	0.500
Base Elevation (m)	3.412
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	61.866
Long. Slope (%)	0.5
Width (m)	4.973
Total Volume (m³)	32.608

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (101)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (13)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP3-2

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	4.007
Depth (m)	0.500
Base Elevation (m)	3.507
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	61.656
Long. Slope (%)	0.5
Width (m)	4.992
Total Volume (m³)	32.619

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (115)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (114)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (15)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP4

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.589
Depth (m)	0.500
Base Elevation (m)	3.089
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	62.656
Long. Slope (%)	0.5
Width (m)	4.987
Total Volume (m³)	33.111

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (32)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (4)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (33)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP5-1

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.553
Depth (m)	0.500
Base Elevation (m)	3.053
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	69.570
Long. Slope (%)	0.5
Width (m)	4.975
Total Volume (m³)	36.645

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (34)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (35)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (5)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP6-1

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.563
Depth (m)	0.500
Base Elevation (m)	3.063
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	51.203
Long. Slope (%)	0.8
Width (m)	4.979
Total Volume (m³)	26.959

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (36)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (37)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (6)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	300.0

PP8

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.941
Depth (m)	0.500
Base Elevation (m)	3.441
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	60.977
Long. Slope (%)	0.5
Width (m)	4.985
Total Volume (m³)	32.221

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (14)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (113)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP9-2

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	4.025
Depth (m)	0.500
Base Elevation (m)	3.525
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	61.609
Long. Slope (%)	0.5
Width (m)	4.997
Total Volume (m³)	32.630

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (16)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (116)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP10

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.604
Depth (m)	0.500
Base Elevation (m)	3.104
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	62.688
Long. Slope (%)	0.5
Width (m)	4.980
Total Volume (m³)	33.082

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (75)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (10)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP11-1

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.551
Depth (m)	0.500
Base Elevation (m)	3.051
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	70.183
Long. Slope (%)	0.5
Width (m)	4.984
Total Volume (m³)	37.030

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (76)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (11)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP12

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.579
Depth (m)	0.500
Base Elevation (m)	3.079
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	100.266
Long. Slope (%)	0.8
Width (m)	4.996
Total Volume (m³)	52.792

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (77)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (12)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP1

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.921
Depth (m)	0.500
Base Elevation (m)	3.421
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	43.556
Long. Slope (%)	0.5
Width (m)	4.967
Total Volume (m³)	22.982

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (28)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (29)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (2)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP7

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.941
Depth (m)	0.500
Base Elevation (m)	3.441
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	44.434
Long. Slope (%)	0.5
Width (m)	4.967
Total Volume (m³)	23.446

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (8)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (39)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP3-1

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	4.158
Depth (m)	0.500
Base Elevation (m)	3.658
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	46.929
Long. Slope (%)	0.5
Width (m)	4.989
Total Volume (m³)	24.862

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (30) CPP (3)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (31)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP9-1

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	4.176
Depth (m)	0.500
Base Elevation (m)	3.676
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	46.990
Long. Slope (%)	0.5
Width (m)	4.974
Total Volume (m³)	24.823

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (70)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (9)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP5-2

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.563
Depth (m)	0.500
Base Elevation (m)	3.063
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	24.809
Long. Slope (%)	0.8
Width (m)	4.908
Total Volume (m³)	12.937

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (117)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (118)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (2)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (17)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP11-2

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.582
Depth (m)	0.500
Base Elevation (m)	3.082
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	24.255
Long. Slope (%)	0.8
Width (m)	4.882
Total Volume (m³)	12.584

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (119)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (18)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	1000.0

PP6-2

Type : Porous Paving

Dimensions

Exceedance Elevation (m)	3.995
Depth (m)	0.500
Base Elevation (m)	3.495
Paving Layer Depth (mm)	200
Membrane Percolation (m/hr)	4.5
Porosity (%)	35
Length (m)	49.329
Long. Slope (%)	0.8
Width (m)	4.976
Total Volume (m³)	25.963

Under Drain

Height Above Base (m)	0.000
Diameter (mm)	110
No. of Barrels	1
Release Height (m)	0.000
Friction Scheme	Manning's n
n	0.015

Inlets

Inlet

Inlet Type	Lateral Inflow
Incoming Item(s)	CPP (1)
Bypass Destination	(None)
Capacity Type	No Restriction

Inlet (1)

Inlet Type	Lateral Inflow
Incoming Item(s)	CIMP (124)
Bypass Destination	(None)
Capacity Type	No Restriction

Advanced

Conductivity (m/hr)	300.0

Proyecto:	Date:		
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025		
	Designed by: FMA	Checked by: GGA	Approved By:
Report Details: Type: Connections Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia		

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Name	From	To	Length (m)	Connection Type	Slope (%)	Manning's n	No. of Barrels	Diameter / Base Width (mm)	Upstream Cover Elevation (m)	Upstream Invert Elevation (m)	Downstream Cover Elevation (m)	Downstream Invert Elevation (m)
1.1	MH1	MH2	20.531	Pipe	0.48	0.011	1	335	4.355	2.900	4.232	2.801
1.2	MH2	MH3	25.052	Pipe	0.40	0.011	1	335	4.232	2.801	4.077	2.701
1.3	MH3	MH4	24.935	Pipe	0.40	0.011	1	335	4.077	2.701	3.981	2.601
1.4	MH4	MH5	24.791	Pipe	0.40	0.011	1	335	3.981	2.601	3.978	2.502
1.5	MH5	MH6	24.946	Pipe	0.40	0.011	1	335	3.978	2.502	4.087	2.402
1.6	MH6	MH7	24.870	Pipe	0.50	0.011	1	335	4.087	2.402	4.208	2.278
1.7	MH7	MH8	24.842	Pipe	0.50	0.011	1	335	4.208	2.278	4.310	2.154
1.8	MH8	MH9	24.983	Pipe	0.50	0.011	1	335	4.310	2.154	4.333	2.029
1.9	MH9	MH10	24.991	Pipe	0.50	0.011	1	335	4.333	2.029	4.243	1.904
1.10	MH10	MH11	25.003	Pipe	0.50	0.011	1	335	4.243	1.904	4.084	1.779
1.11	MH11	MH24	23.404	Pipe	0.50	0.011	1	335	4.084	1.779	3.944	1.662
1.12	MH24	MH25	8.279	Pipe	0.50	0.011	1	527	3.944	1.463	4.028	1.422
1.13	MH25	Vertido1	19.793	Pipe	1.00	0.011	2	335	4.028	0.900	3.086	0.702
RP7	PP7	MH4	5.189	Pipe	3.00	0.011	1	209	4.042	3.441	3.981	3.285
RP8	PP8	MH4	5.975	Pipe	3.00	0.011	1	209	4.016	3.441	3.981	3.261
RJ40	JLL40	MH4	6.180	Pipe	3.00	0.011	1	209	3.971	3.864	3.981	3.679
TD40	JLL40	MH4	5.863	Pipe	3.00	0.011	1	209	3.954	3.114	3.981	2.938
TD41	JLL41	MH6	6.235	Pipe	3.00	0.011	1	209	4.069	2.954	4.087	2.767
RJ41	JLL41	MH6	6.240	Pipe	3.00	0.011	1	209	4.083	3.704	4.087	3.517
RP9-1	PP9-1	MH7	4.798	Pipe	3.00	0.011	1	209	4.234	3.676	4.208	3.532
TD42	JLL42	MH7	7.803	Pipe	3.00	0.011	1	209	4.234	3.342	4.208	3.108
RJ42	JLL42	MH7	11.157	Pipe	3.00	0.011	1	209	4.243	4.092	4.208	3.757
TD43	JLL43	MH9	7.247	Pipe	3.00	0.011	1	209	4.366	3.430	4.333	3.213
RJ43	JLL43	MH9	7.179	Pipe	3.00	0.011	1	209	4.370	4.180	4.333	3.965
2.1	MH12	MH13	20.310	Pipe	0.55	0.011	1	335	4.145	2.795	4.047	2.683
2.2	MH13	MH14	22.274	Pipe	0.40	0.011	1	335	4.047	2.683	3.958	2.594
2.3	MH14	MH15	22.013	Pipe	0.40	0.011	1	335	3.958	2.594	3.949	2.506
2.4	MH15	MH16	24.823	Pipe	0.40	0.011	1	335	3.949	2.506	4.039	2.407
2.5	MH16	MH17	24.969	Pipe	0.40	0.011	1	335	4.039	2.407	4.164	2.307
2.6	MH17	MH18	24.576	Pipe	0.40	0.011	1	335	4.164	2.307	4.275	2.209
2.7	MH18	MH19	24.720	Pipe	0.40	0.011	1	418	4.275	2.126	4.319	2.027
2.8	MH19	MH20	24.216	Pipe	0.40	0.011	1	418	4.319	2.027	4.255	1.930
2.9	MH20	MH21	22.052	Pipe	0.40	0.011	1	418	4.255	1.930	4.129	1.842
2.10	MH21	MH22	19.910	Pipe	0.40	0.011	1	418	4.129	1.842	4.009	1.762

2.11	MH22	MH23	13.675	Pipe	0.40	0.011	1	418	4.009	1.762	3.992	1.707
2.12	MH23	MH24	13.079	Pipe	0.40	0.011	1	418	3.992	1.707	3.944	1.655
RJ24	JLL24	MH12	17.542	Pipe	3.00	0.011	1	209	4.219	4.074	4.145	3.548
TD24	JLL24	MH12	14.969	Pipe	3.00	0.011	1	209	4.177	3.324	4.145	2.875
TD25	JLL25	MH14	13.938	Pipe	3.00	0.011	1	209	3.983	3.135	3.958	2.716
RJ25	JLL25	MH14	12.149	Pipe	3.00	0.011	1	209	3.973	3.885	3.958	3.521
RP2-1	PP1	MH14	3.998	Pipe	3.00	0.011	1	209	3.928	3.421	3.958	3.302
RP2-2	PP2	MH14	5.772	Pipe	3.00	0.011	1	209	3.926	3.412	3.958	3.239
RJ27	JLL27	MH15	10.763	Pipe	3.00	0.011	1	209	3.947	3.856	3.949	3.533
TD27	JLL27	MH15	11.145	Pipe	3.00	0.011	1	209	3.953	3.106	3.949	2.772
RJ28	JLL28	MH16	10.655	Pipe	3.00	0.011	1	209	4.039	3.944	4.039	3.624
TD28	JLL28	MH16	10.661	Pipe	3.00	0.011	1	209	4.060	3.194	4.039	2.875
RJ29	JLL29	MH17	11.839	Pipe	3.00	0.011	1	209	4.191	4.097	4.164	3.742
TD29	JLL29	MH17	13.077	Pipe	3.00	0.011	1	209	4.209	3.347	4.164	2.954
RP3-1	PP3-1	MH18	19.275	Pipe	3.00	0.011	1	209	4.176	3.658	4.275	3.080
TD30	JLL30	MH21	16.724	Pipe	3.00	0.011	1	209	4.217	3.352	4.129	2.850
RJ30	JLL30	MH21	15.256	Pipe	3.00	0.011	1	209	4.195	4.102	4.129	3.644
TD31	JLL31	MH22	11.196	Pipe	3.00	0.011	1	209	4.042	3.199	4.009	2.863
RJ31	JLL31	MH22	10.590	Pipe	3.00	0.011	1	209	4.025	3.949	4.009	3.631
RP3-2	PP3-2	MH22	8.407	Pipe	3.00	0.011	1	209	4.035	3.507	4.009	3.255
RP9-2	PP9-2	MH11	9.339	Pipe	3.00	0.011	1	209	4.059	3.525	4.084	3.245
3.1	MH28	MH29	24.864	Pipe	0.50	0.011	1	335	3.624	2.224	3.574	2.099
3.2	MH29	MH30	24.906	Pipe	0.50	0.011	1	335	3.574	2.099	3.664	1.974
3.3	MH30	MH31	25.000	Pipe	0.50	0.011	1	335	3.664	1.974	3.700	1.849
3.4	MH31	MH32	25.000	Pipe	0.50	0.011	1	335	3.700	1.849	3.616	1.724
3.5	MH32	MH33	23.553	Pipe	0.53	0.011	1	335	3.616	1.724	3.667	1.599
RP10	PP10	MH28	7.266	Pipe	3.00	0.011	1	209	3.641	3.104	3.624	2.886
RJ45	JLL45	MH28	9.396	Pipe	3.00	0.011	1	209	3.728	3.508	3.624	3.226
TD45	JLL45	MH28	8.740	Pipe	3.00	0.011	1	209	3.728	2.758	3.624	2.495
TD46	JLL46	MH29	5.855	Pipe	3.00	0.011	1	209	3.611	2.731	3.574	2.556
RJ46	JLL46	MH29	6.921	Pipe	3.00	0.011	1	209	3.621	3.481	3.574	3.273
RJ48	JLL48	MH32	8.597	Pipe	3.00	0.011	1	209	3.566	3.516	3.616	3.258
TD48	JLL48	MH32	10.031	Pipe	3.00	0.011	1	209	3.568	2.766	3.616	2.465
RJ49	JLL49	MH34	6.864	Pipe	3.64	0.011	1	209	3.879	3.768	3.869	3.518
TD49	JLL49	MH34	8.325	Pipe	3.00	0.011	1	209	3.909	3.018	3.869	2.768
RJ50	JLL50	MH35	6.188	Pipe	3.00	0.011	1	209	4.213	4.145	4.210	3.959

TD50	JLL50	MH35	6.910	Pipe	3.00	0.011	1	209	4.223	3.395	4.210	3.188
RP11-1	PP11-1	MH31	8.127	Pipe	3.00	0.011	1	209	3.643	3.051	3.700	2.807
RP11-2	PP11-2	MH31	11.493	Pipe	3.00	0.011	1	209	3.619	3.082	3.700	2.737
RP12	PP12	MH33	6.320	Pipe	3.38	0.011	1	209	3.650	3.079	3.667	2.865
5.1	MH36	MH37	24.972	Pipe	0.40	0.011	1	335	3.864	2.464	3.714	2.364
5.2	MH37	MH38	25.031	Pipe	0.40	0.011	1	335	3.714	2.364	3.588	2.264
5.3	MH38	MH39	24.992	Pipe	0.40	0.011	1	335	3.588	2.264	3.589	2.164
5.4	MH39	MH40	24.999	Pipe	0.40	0.011	1	335	3.589	2.164	3.677	2.064
5.5	MH40	MH41	25.034	Pipe	0.60	0.011	1	335	3.677	2.064	3.637	1.914
5.6	MH41	MH42	22.351	Pipe	0.60	0.011	1	335	3.637	1.914	3.588	1.780
7.11	MH42	MH43	14.117	Pipe	0.50	0.011	1	418	3.588	1.226	3.635	1.155
6.1	MH45	MH46	25.000	Pipe	1.25	0.011	1	335	4.164	2.000	3.960	1.688
RJ32	JLL32	MH36	12.520	Pipe	3.00	0.011	1	209	3.828	3.726	3.864	3.350
TD32	JLL32	MH36	11.843	Pipe	3.00	0.011	1	209	3.834	2.976	3.864	2.621
TD33	JLL33	MH38	18.506	Pipe	2.94	0.011	1	209	3.651	2.807	3.588	2.264
RJ33	JLL33	MH38	18.156	Pipe	3.00	0.011	1	209	3.646	3.557	3.588	3.012
RP4	PP4	MH37	2.605	Pipe	3.00	0.011	1	335	3.693	3.089	3.714	3.011
TD34	JLL34	MH39	17.506	Pipe	3.00	0.011	1	209	3.573	2.733	3.589	2.208
RJ34	JLL34	MH39	15.961	Pipe	3.00	0.011	1	209	3.576	3.483	3.589	3.004
TD35	JLL35	MH40	10.828	Pipe	3.00	0.011	1	209	3.673	2.736	3.677	2.411
RJ35	JLL35	MH40	10.724	Pipe	3.00	0.011	1	209	3.677	3.486	3.677	3.164
RP5-1	PP5-1	MH40	4.511	Pipe	3.00	0.011	1	209	3.656	3.053	3.677	2.918
RP5-2	PP5-2	MH41	3.526	Pipe	3.00	0.011	1	209	3.601	3.063	3.637	2.957
RP6-1	PP6-1	MH43	8.321	Pipe	1.23	0.011	1	209	3.679	3.063	3.635	2.961
TD37	JLL37	MH44	17.704	Pipe	3.00	0.011	1	209	3.880	3.014	3.770	2.483
RJ37	JLL37	MH44	14.783	Pipe	2.69	0.011	1	209	3.856	3.764	3.770	3.366
RJ38	JLL38	MH45	11.161	Pipe	3.00	0.011	1	209	4.142	4.035	4.164	3.700
TD38	JLL38	MH45	12.227	Pipe	3.00	0.011	1	209	4.159	3.285	4.164	2.919
TD20	JLL20	Manhole (46)	11.882	Pipe	3.00	0.011	1	209	3.147	2.386	3.001	2.030
RJ20	JLL20	Manhole (46)	13.148	Pipe	3.00	0.011	1	209	3.152	3.136	3.001	2.742
RJ21	JLL21	Manhole (47)	7.830	Pipe	3.00	0.011	1	209	3.283	3.197	3.075	2.962
TD21	JLL21	Manhole (47)	7.187	Pipe	3.00	0.011	1	209	3.252	2.447	3.075	2.232
RJ19	JLL19	Manhole (45)	14.432	Pipe	3.00	0.011	1	209	3.239	3.161	3.127	2.728
TD19	JLL19	Manhole (45)	15.755	Pipe	3.00	0.011	1	209	3.234	2.411	3.127	1.939
TD18	JLL18	Manhole (44)	11.100	Pipe	3.00	0.011	1	209	3.371	2.539	3.246	2.206
RJ18	JLL18	Manhole (44)	12.928	Pipe	3.00	0.011	1	209	3.376	3.289	3.246	2.901

Proyecto:	Date:		
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025		
	Designed by: FMA	Checked by: GGA	Approved By:
Report Details: Type: Connections Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia		

Grupo TYPSA

RJ17	JLL17	Manhole (43)	8.519	Pipe	3.00	0.011	1	209	3.571	3.475	3.378	3.219
TD17	JLL17	Manhole (43)	9.168	Pipe	3.00	0.011	1	209	3.572	2.725	3.378	2.450
TD16	JLL16	Manhole (42)	16.592	Pipe	3.00	0.011	1	209	3.741	2.897	3.626	2.399
RJ16	JLL16	Manhole (42)	19.797	Pipe	3.00	0.011	1	209	3.728	3.647	3.626	3.053
TD15	JLL15	Manhole (41)	12.061	Pipe	3.00	0.011	1	209	3.878	3.047	3.751	2.685
RJ15	JLL15	Manhole (41)	12.879	Pipe	3.00	0.011	1	209	3.877	3.797	3.751	3.411
TD14	JLL14	Manhole (40)	9.310	Pipe	3.00	0.011	1	209	4.015	3.178	3.877	2.898
RJ14	JLL14	Manhole (40)	11.362	Pipe	3.00	0.011	1	209	4.025	3.928	3.877	3.587
RJ13	JLL13	Manhole (39)	12.643	Pipe	3.00	0.011	1	209	3.938	3.865	3.629	3.486
TD13	JLL13	Manhole (39)	12.031	Pipe	3.00	0.011	1	209	3.936	3.115	3.629	2.755
TD12	JLL12	Manhole (38)	10.155	Pipe	3.00	0.011	1	209	3.513	2.676	3.297	2.371
RJ12	JLL12	Manhole (38)	9.694	Pipe	3.00	0.011	1	209	3.498	3.426	3.297	3.135
RJ23	JLL23	Manhole (48)	19.956	Pipe	3.00	0.011	1	209	3.722	3.538	3.296	2.939
TD23	JLL23	Manhole (48)	17.926	Pipe	3.00	0.011	1	209	3.773	2.878	3.296	2.340
TD55	JLL55	Manhole (38)	12.722	Pipe	3.00	0.011	1	209	3.536	2.516	3.297	2.135
RJ55	JLL55	Manhole (38)	10.353	Pipe	3.00	0.011	1	209	3.402	3.266	3.297	2.955
TD56	JLL56	Manhole (43)	9.682	Pipe	3.00	0.011	1	209	3.683	2.724	3.378	2.434
RJ56	JLL56	Manhole (43)	8.614	Pipe	3.00	0.011	1	209	3.641	3.474	3.378	3.216
RJ57	JLL57	Manhole (47)	12.483	Pipe	3.00	0.011	1	209	3.389	3.441	3.075	3.066
TD57	JLL57	Manhole (47)	10.068	Pipe	3.00	0.011	1	209	3.364	2.691	3.075	2.389
RJ10	JLL10	Manhole (28)	14.512	Pipe	3.00	0.011	1	209	3.090	3.014	3.104	2.579
TD10	JLL10	Manhole (28)	13.257	Pipe	3.00	0.011	1	209	3.073	2.264	3.104	1.867
RJ9	JLL9	Manhole (28)	11.675	Pipe	3.00	0.011	1	209	3.043	2.998	3.104	2.648
TD9	JLL9	Manhole (28)	11.441	Pipe	3.00	0.011	1	209	3.029	2.248	3.104	1.904
RJ8	JLL8	Manhole (29)	11.620	Pipe	3.00	0.011	1	209	3.075	3.032	3.158	2.683
TD8	JLL8	Manhole (29)	11.929	Pipe	3.00	0.011	1	209	3.090	2.282	3.158	1.924
RJ7	JLL7	Manhole (30)	11.694	Pipe	3.00	0.011	1	209	3.219	3.170	3.283	2.819
TD7	JLL7	Manhole (30)	12.348	Pipe	3.00	0.011	1	209	3.225	2.420	3.283	2.049
RJ6	JLL6	Manhole (31)	16.700	Pipe	7.67	0.011	1	209	3.393	3.336	3.533	2.056
TD6	JLL6	Manhole (31)	17.682	Pipe	3.00	0.011	1	209	3.390	2.586	3.533	2.056
TD5	JLL5	Manhole (32)	13.172	Pipe	3.00	0.011	1	209	3.551	2.742	3.658	2.347
RJ5	JLL5	Manhole (32)	12.888	Pipe	3.00	0.011	1	209	3.556	3.492	3.658	3.105
RJ4	JLL4	Manhole (33)	12.903	Pipe	3.00	0.011	1	209	3.679	3.630	3.784	3.243
TD4	JLL4	Manhole (33)	11.979	Pipe	3.00	0.011	1	209	3.687	2.880	3.784	2.521
RJ3	JLL3	Manhole (34)	12.611	Pipe	3.00	0.011	1	209	3.809	3.768	3.908	3.390
TD3	JLL3	Manhole (34)	11.494	Pipe	3.00	0.011	1	209	3.824	3.018	3.908	2.673

Proyecto:	Date:		
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025		
	Designed by: FMA	Checked by: GGA	Approved By:
Report Details: Type: Connections Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia		

Grupo TYPSA

RJ1	JLL1	Manhole (36)	15.673	Pipe	8.19	0.011	1	209	3.249	3.140	3.465	1.856
TD1	JLL1	Manhole (36)	17.773	Pipe	3.00	0.011	1	209	3.201	2.390	3.465	1.856
RJ11	JLL11	Manhole (26)	15.972	Pipe	3.00	0.011	1	209	3.296	3.130	3.292	2.651
TD11	JLL11	Manhole (26)	16.866	Pipe	3.00	0.011	1	209	3.283	2.380	3.292	1.874
RJ58	JLL58	Manhole (27)	6.992	Pipe	3.00	0.011	1	209	3.434	3.220	3.242	3.010
TD58	JLL58	Manhole (27)	7.039	Pipe	3.00	0.011	1	209	3.115	2.470	3.242	2.259
RJ61	JLL61	Manhole (50)	14.979	Pipe	3.00	0.011	1	209	3.500	3.285	3.315	2.836
TD61	JLL61	Manhole (50)	13.734	Pipe	3.00	0.011	1	209	3.512	2.525	3.315	2.113
RJ60	JLL60	Manhole (27)	10.743	Pipe	3.00	0.011	1	209	3.222	3.139	3.242	2.817
TD60	JLL60	Manhole (27)	10.228	Pipe	3.00	0.011	1	209	3.152	2.389	3.242	2.082
7.14	MH47	Vertido2	21.975	Pipe	0.85	0.011	2	335	3.576	0.795	3.055	0.608
RZB1	ZBIO1	Manhole	10.608	Pipe	3.00	0.011	1	335	2.691	2.588	2.724	2.270
DZB1	ZBIO1	Manhole	11.691	Pipe	3.00	0.011	1	335	2.697	1.222	2.724	0.872
TDB26	BJLL-26	Manhole (1)	23.936	Pipe	3.00	0.011	1	209	2.756	1.826	2.545	1.108
RBB26	BJLL-26	Manhole (1)	24.382	Pipe	3.00	0.011	1	209	2.724	2.626	2.545	1.895
7.10	MH57	MH42	15.985	Pipe	0.40	0.011	1	335	3.546	1.373	3.588	1.309
RJ59	JLL59	Manhole (10)	21.869	Pipe	3.00	0.011	1	209	3.131	3.068	3.200	2.412
TD59	JLL59	Manhole (10)	20.995	Pipe	3.00	0.011	1	209	3.404	2.318	3.200	1.689
RB65	JLL65	Manhole (11)	10.881	Pipe	3.00	0.011	1	209	3.505	3.452	4.053	3.126
TD65	JLL65	Manhole (11)	10.177	Pipe	3.00	0.011	1	209	3.509	2.752	4.053	2.447
RB64	JLL64	Manhole (12)	6.931	Pipe	3.00	0.011	1	209	3.490	3.416	3.872	3.208
TD64	JLL64	Manhole (12)	8.659	Pipe	3.00	0.011	1	209	3.482	2.716	3.872	2.457
RB63	JLL63	Manhole (13)	16.034	Pipe	3.00	0.011	1	209	3.116	3.033	3.509	2.552
TD63	JLL63	Manhole (13)	11.644	Pipe	3.00	0.011	1	209	3.115	2.333	3.509	1.984
TD62	JLL62	Manhole (14)	7.404	Pipe	3.00	0.011	1	209	2.768	2.036	3.327	1.814
RB62	JLL62	Manhole (14)	8.566	Pipe	3.00	0.011	1	209	2.748	2.736	3.327	2.479
RJ26	JLL26	MH15	12.133	Pipe	3.00	0.011	1	209	3.933	3.844	3.949	3.480
TD26	JLL26	MH15	13.086	Pipe	3.00	0.011	1	209	3.932	3.094	3.949	2.702
7.1	MH48	MH49	25.084	Pipe	0.40	0.011	1	335	3.700	2.240	3.700	2.140
7.2	MH49	MH50	24.969	Pipe	0.40	0.011	1	335	3.700	2.140	3.700	2.040
7.3	MH50	MH51	24.703	Pipe	0.40	0.011	1	335	3.700	2.040	3.650	1.941
7.4	MH51	MH52	24.686	Pipe	0.40	0.011	1	335	3.650	1.941	3.600	1.842
7.5	MH52	MH53	24.945	Pipe	0.40	0.011	1	335	3.600	1.842	3.550	1.742
7.8	MH55	MH56	23.574	Pipe	0.40	0.011	1	335	3.600	1.558	3.600	1.464
7.9	MH56	MH57	19.267	Pipe	0.40	0.011	1	335	3.600	1.464	3.546	1.387
8.6	MH63	MH64	24.981	Pipe	0.45	0.011	1	335	3.700	1.630	3.650	1.518

RBB8	BJLL-8	MH63	15.028	Pipe	10.04	0.011	1	209	3.717	3.650	3.700	2.140
TDB8	BJLL-8	MH63	13.758	Pipe	3.00	0.011	1	209	3.727	2.850	3.700	2.437
RBB7	BJLL-7	MH57	16.362	Pipe	2.49	0.011	1	209	3.629	3.450	3.546	3.042
TDB7	BJLL-7	MH57	16.528	Pipe	3.00	0.011	1	209	3.637	2.700	3.546	2.204
RBB14	BJLL-14	Manhole (9)	29.271	Pipe	2.61	0.011	1	209	3.128	2.850	2.880	2.087
TDB14	BJLL-14	Manhole (9)	29.811	Pipe	3.06	0.011	1	209	3.118	2.050	2.880	1.138
RBB18	BJLL-18	Manhole (2)	8.274	Pipe	1.94	0.011	1	209	2.521	2.421	2.755	2.260
TDB18	BJLL-18	Manhole (2)	7.173	Pipe	3.00	0.011	1	209	2.509	1.621	2.755	1.406
RBB17	BJLL-17	Manhole (3)	13.599	Pipe	3.18	0.011	1	209	2.696	2.450	3.070	2.017
TDB17	BJLL-17	Manhole (3)	13.446	Pipe	3.00	0.011	1	209	2.722	1.650	3.070	1.247
TDB22	BJLL-22	Manhole (4)	6.559	Pipe	3.00	0.011	1	209	3.623	1.900	3.605	1.703
RBB22	BJLL-22	Manhole (4)	6.092	Pipe	3.00	0.011	1	209	3.616	2.750	3.605	2.567
TDB25	BJLL-25	Manhole (5)	8.044	Pipe	3.00	0.011	1	209	3.969	2.950	4.000	2.709
RBB25	BJLL-25	Manhole (5)	9.245	Pipe	3.00	0.011	1	209	3.969	3.750	4.000	3.473
TDB24	BJLL-24	Manhole (6)	3.390	Pipe	3.00	0.011	1	209	3.356	2.300	3.300	2.198
RBB24	BJLL-24	Manhole (6)	4.376	Pipe	3.00	0.011	1	209	3.356	3.150	3.300	3.019
RBB13	BJLL-13	Manhole (15)	18.787	Pipe	1.22	0.011	1	209	3.408	2.250	3.373	2.021
TDB13	BJLL-13	Manhole (15)	19.254	Pipe	3.00	0.011	1	209	3.386	1.450	3.373	0.872
RBB21	BJLL-21	Manhole (16)	5.238	Pipe	3.00	0.011	1	209	2.896	2.550	2.993	2.393
TDB21	BJLL-21	Manhole (16)	4.610	Pipe	3.00	0.011	1	209	2.994	1.750	2.993	1.612
RBB23	BJLL-23	Manhole (17)	13.904	Pipe	3.00	0.011	1	209	3.179	2.550	3.788	2.133
TDB23	BJLL-23	Manhole (17)	14.185	Pipe	3.00	0.011	1	209	2.957	1.800	3.788	1.374
RBB12	BJLL-12	Manhole (18)	11.225	Pipe	2.81	0.011	1	209	3.567	2.750	3.000	2.435
TDB12	BJLL-12	Manhole (18)	11.861	Pipe	3.00	0.011	1	209	3.567	2.650	3.000	2.294
9.1	MH65	MH66	23.112	Pipe	0.50	0.011	1	335	2.850	1.380	3.044	1.264
10.6	MH66	Manhole (19)	27.756	Pipe	0.40	0.011	1	335	3.044	0.715	3.049	0.604
RBB19	BJLL-19	MH65	14.966	Pipe	1.91	0.011	1	209	2.945	2.650	2.850	2.363
TDB19	BJLL-19	MH65	13.738	Pipe	3.06	0.011	1	209	2.930	1.800	2.850	1.380
RBB16	BJLL-16	MH69	10.154	Pipe	1.98	0.011	1	209	2.760	2.550	2.896	2.349
TDB16	BJLL-16	MH69	10.126	Pipe	3.00	0.011	1	209	2.738	1.650	2.896	1.347
RBB20	BJLL-20	MH67	10.041	Pipe	3.00	0.011	1	209	2.752	1.828	2.759	1.527
TDB20	BJLL-20	MH67	9.410	Pipe	3.00	0.011	1	209	2.745	2.623	2.759	2.341
RBB2	BJLL-2	Manhole (24)	12.407	Pipe	3.00	0.011	1	209	3.194	3.052	3.091	2.680
TDB2	BJLL-2	Manhole (24)	13.419	Pipe	3.00	0.011	1	209	3.216	2.315	3.091	1.912
RBB27	BJLL-27	Manhole (25)	6.473	Pipe	3.00	0.011	1	209	3.573	3.250	3.503	3.056
TDB27	BJLL-27	Manhole (25)	6.462	Pipe	11.51	0.011	1	209	3.569	3.000	3.503	2.256

RBB1	BJLL-1	Manhole (37)	25.739	Pipe	3.00	0.011	1	209	3.683	3.250	3.421	2.478
TDB1	BJLL-1	Manhole (37)	25.195	Pipe	3.00	0.011	1	209	3.674	2.400	3.421	1.644
RBB11	BJLL-11	Manhole (49)	15.806	Pipe	2.04	0.011	1	209	2.839	2.650	2.759	2.328
TDB11	BJLL-11	Manhole (49)	14.991	Pipe	3.00	0.011	1	209	2.836	1.800	2.759	1.350
RBB15	BJLL-15	Manhole (8)	12.869	Pipe	8.16	0.011	1	209	2.167	2.450	2.606	1.400
TDB15	BJLL-15	Manhole (8)	12.917	Pipe	1.94	0.011	1	209	2.172	1.650	2.606	1.400
10.1	MH67	MH68	25.033	Pipe	0.40	0.011	1	335	2.759	1.195	2.672	1.095
10.2	MH68	MH69	24.163	Pipe	0.40	0.011	1	335	2.672	1.095	2.896	0.998
10.3	MH69	MH70	24.978	Pipe	0.40	0.011	1	335	2.896	0.998	2.948	0.898
10.4	MH70	MH71	24.549	Pipe	0.40	0.011	1	335	2.948	0.898	3.010	0.800
10.5	MH71	MH66	21.220	Pipe	0.40	0.011	1	335	3.010	0.800	3.044	0.715
RJ2	JLL2	Manhole (36)	24.662	Pipe	3.00	0.011	1	209	3.652	3.443	3.465	2.703
TD2	JLL2	Manhole (36)	22.863	Pipe	3.00	0.011	1	209	3.607	2.693	3.465	2.007
RJ22	JLL22	Manhole (38)	18.141	Pipe	3.00	0.011	1	209	3.577	2.761	3.297	2.217
TD22	JLL22	Manhole (38)	17.885	Pipe	3.00	0.011	1	209	3.605	2.761	3.297	2.224
RP6-2	PP6-2	MH45	2.130	Pipe	3.00	0.011	1	209	4.121	3.495	4.164	3.431
7.6	MH53	MH54	24.986	Pipe	0.40	0.011	1	335	3.550	1.742	3.500	1.642
7.7	MH54	MH55	21.048	Pipe	0.40	0.011	1	335	3.500	1.642	3.600	1.558
TDB3	BJLL-3	MH48	12.006	Pipe	3.00	0.011	1	209	3.363	2.600	3.700	2.240
RBB3	BJLL-3	MH48	12.481	Pipe	1.66	0.011	1	209	3.357	3.450	3.700	3.243
RBB4	BJLL-4	MH51	9.828	Pipe	5.05	0.011	1	209	3.254	3.450	3.650	2.953
TDB4	BJLL-4	MH51	9.144	Pipe	3.00	0.011	1	209	3.259	2.600	3.650	2.326
TDB5	BJLL-5	MH53	7.738	Pipe	4.47	0.011	1	209	3.336	2.550	3.550	2.204
RBB5	BJLL-5	MH53	6.267	Pipe	6.20	0.011	1	209	3.335	3.350	3.550	2.962
RBB10	BJLL-10	MH58	7.932	Pipe	3.00	0.011	1	209	3.163	3.200	3.400	2.962
TDB10	BJLL-10	MH58	7.133	Pipe	3.00	0.011	1	209	3.170	2.400	3.400	2.186
8.1	MH58	MH59	24.963	Pipe	0.45	0.011	1	335	3.400	2.186	3.400	2.074
8.2	MH59	MH60	24.986	Pipe	0.45	0.011	1	335	3.400	2.074	3.303	1.961
8.3	MH60	MH61	25.187	Pipe	0.45	0.011	1	335	3.303	1.961	3.503	1.848
8.4	MH61	MH62	24.660	Pipe	0.45	0.011	1	335	3.503	1.848	3.574	1.737
8.5	MH62	MH63	23.612	Pipe	0.45	0.011	1	335	3.574	1.737	3.700	1.630
RBB9	BJLL-9	MH61	13.782	Pipe	3.22	0.011	1	209	3.411	3.350	3.503	2.906
TDB9	BJLL-9	MH61	12.365	Pipe	3.00	0.011	1	209	3.425	2.550	3.503	2.179
8.7	MH64	MH57	29.911	Pipe	0.45	0.011	1	335	3.650	1.518	3.546	1.383
RJ39	JLL39	MH1	8.381	Pipe	3.00	0.011	1	209	4.430	4.326	4.355	4.075
TD39	JLL39	MH1	6.221	Pipe	3.00	0.011	1	209	4.432	3.576	4.355	3.390

6.2	MH46	MH44	19.147	Pipe	1.25	0.011	1	335	3.960	1.688	3.770	1.449
4.1	MH35	MH 35.1	24.999	Pipe	2.00	0.011	1	335	4.210	2.647	4.006	2.147
4.2	MH 35.1	MH34	16.476	Pipe	2.00	0.011	1	335	4.006	2.147	3.869	1.817
6.3	MH44	MH43	16.300	Pipe	1.25	0.011	1	335	3.770	1.449	3.635	1.245
4.3	MH34	MH33	24.242	Pipe	2.50	0.011	1	335	3.869	1.817	3.667	1.211
7.12	MH43	MH33	19.976	Pipe	0.50	0.011	1	418	3.635	1.155	3.667	1.055
7.13	MH33	MH47	18.185	Pipe	0.85	0.011	2	335	3.667	0.950	3.576	0.795
RJ36	JLL36	MH57	3.064	Pipe	3.00	0.011	1	209	3.559	3.497	3.546	3.405
TD36	JLL36	MH57	3.315	Pipe	3.00	0.011	1	209	3.572	2.747	3.546	2.647
RBB6	BJLL-6	MH57	11.407	Pipe	3.00	0.011	1	209	3.599	3.350	3.546	3.008
TDB6	BJLL-6	MH57	10.450	Pipe	3.00	0.011	1	209	3.602	2.550	3.546	2.236

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
	Designed by: FMA	Checked by: GGA	Approved By:	
Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH1	4.355 2.900	Diameter / Length: 1.000	{1} RJ39	Pipe	4.075	Diam/Width:209	Manhole
E:728803.008 N:4370590.143	1.455		{2} TD39	Pipe	3.390	Diam/Width:209	
			{a} 1.1	Pipe	2.900	Diam/Width:335	Not Applicable
MH2	4.232 2.801	Diameter / Length: 1.000	{1} 1.1	Pipe	2.801	Diam/Width:335	Manhole
E:728823.363 N:4370592.827	1.431						
			{a} 1.2	Pipe	2.801	Diam/Width:335	Not Applicable
MH3	4.077 2.701	Diameter / Length: 1.000	{1} 1.2	Pipe	2.701	Diam/Width:335	Manhole
E:728848.121 N:4370596.649	1.376						
			{a} 1.3	Pipe	2.701	Diam/Width:335	Not Applicable

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
	Designed by: FMA	Checked by: GGA	Approved By:	
Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH4	3.981 2.601	Diameter / Length: 1.000	{1} 1.3	Pipe	2.601	Diam/Width:335	Manhole
E:728872.714 N:4370600.768	1.380		{2} RP8	Pipe	3.261	Diam/Width:209 Diam/Width:209	
			{3} RJ40	Pipe	3.679	Diam/Width:209 Diam/Width:209	
			{4} RP7	Pipe	3.285		
			{5} TD40	Pipe	2.938		
			{a} 1.4	Pipe	2.601	Diam/Width:335	Not Applicable
MH5	3.978 2.502	Diameter / Length: 1.000	{1} 1.4	Pipe	2.502	Diam/Width:335	Manhole
E:728897.147 N:4370604.965	1.476						
			{a} 1.5	Pipe	2.502	Diam/Width:335	Not Applicable
MH6	4.087 2.402	Diameter / Length: 1.000	{1} 1.5	Pipe	2.402	Diam/Width:335	Manhole
E:728921.667 N:4370609.555	1.685		{2} TD41	Pipe	2.767	Diam/Width:209 Diam/Width:209	
			{3} RJ41	Pipe	3.517		
			{a} 1.6	Pipe	2.402	Diam/Width:335	Not Applicable

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
	Designed by: FMA	Checked by: GGA	Approved By:	
Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH7	4.208 2.278	Diameter / Length: 1.000	{1} 1.6	Pipe	2.278	Diam/Width:335	Manhole
E:728946.101 N:4370614.189	1.930		{2} RP9-1	Pipe	3.532	Diam/Width:209	
			{3} TD42	Pipe	3.108	Diam/Width:209	
			{4} RJ42	Pipe	3.757	Diam/Width:209	
			{a} 1.7	Pipe	2.278	Diam/Width:335	Not Applicable
MH8	4.310 2.154	Diameter / Length: 1.000	{1} 1.7	Pipe	2.154	Diam/Width:335	Manhole
E:728970.489 N:4370618.920	2.156						
			{a} 1.8	Pipe	2.154	Diam/Width:335	Not Applicable
MH9	4.333 2.029	Diameter / Length: 1.000	{1} 1.8	Pipe	2.029	Diam/Width:335	Manhole
E:728994.965 N:4370623.928	2.304		{2} RJ43	Pipe	3.965	Diam/Width:209	
			{3} TD43	Pipe	3.213	Diam/Width:209	
			{a} 1.9	Pipe	2.029	Diam/Width:335	Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH10	4.243 1.904	Diameter / Length: 1.000	{1} 1.9	Pipe	1.904	Diam/Width:335	Manhole
E:729019.371 N:4370629.302	2.339						
			{a} 1.10	Pipe	1.904	Diam/Width:335	Not Applicable
MH11	4.084 1.779	Diameter / Length: 1.000	{1} 1.10 {2} RP9-2	Pipe Pipe	1.779 3.245	Diam/Width:335 Diam/Width:209	Manhole
E:729043.830 N:4370634.486	2.305						
			{a} 1.11	Pipe	1.779	Diam/Width:335	Not Applicable
MH24	3.944 1.463	Diameter / Length: 1.000	{1} 1.11 {2} 2.12	Pipe Pipe	1.662 1.655	Diam/Width:335 Diam/Width:418	Manhole
E:729066.577 N:4370639.995	2.481						
			{a} 1.12	Pipe	1.463	Diam/Width:527	Not Applicable
MH25	4.028 0.900	Diameter / Length: 1.500	{1} 1.12	Pipe	1.422	Diam/Width:527	Manhole
E:729068.541 N:4370631.952	3.128						
			{a} 1.13	Pipe	0.900	Diam/Width:335	Not Applicable

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
	Designed by: FMA	Checked by: GGA	Approved By:	
Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Vertido1	3.086 0.702	Diameter / Length: 1.600	{1} 1.13	Pipe	0.702	Diam/Width:335	Manhole
E:729073.545 N:4370612.803	2.384	Width: 3.600					Not Applicable
MH12	4.145 2.795	Diameter / Length: 1.000	{1} RJ24 {2} TD24	Pipe Pipe	3.548 2.875	Diam/Width:209 Diam/Width:209	Manhole
E:728825.241 N:4370613.214	1.350		{a} 2.1	Pipe	2.795	Diam/Width:335	Not Applicable
MH13	4.047 2.683	Diameter / Length: 1.000	{1} 2.1	Pipe	2.683	Diam/Width:335	Manhole
E:728845.309 N:4370616.343	1.364		{a} 2.2	Pipe	2.683	Diam/Width:335	Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH14	3.958 2.594	Diameter / Length: 1.000	{1} 2.2	Pipe	2.594	Diam/Width:335	Manhole
E:728867.273 N:4370620.046	1.364		{2} TD25	Pipe	2.716	Diam/Width:209	
			{3} RP2-2	Pipe	3.239	Diam/Width:209	
			{4} RJ25	Pipe	3.521	Diam/Width:209	
			{5} RP2-1	Pipe	3.302	Diam/Width:209	
			{a} 2.3	Pipe	2.594	Diam/Width:335	Not Applicable
MH15	3.949 2.506	Diameter / Length: 1.000	{1} 2.3	Pipe	2.506	Diam/Width:335	Manhole
E:728888.987 N:4370623.657	1.443		{2} RJ27	Pipe	3.533	Diam/Width:209	
			{3} TD27	Pipe	2.772	Diam/Width:209	
			{4} RJ26	Pipe	3.480	Diam/Width:209	
			{5} TD26	Pipe	2.702	Diam/Width:209	
			{a} 2.4	Pipe	2.506	Diam/Width:335	Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH16	4.039 2.407	Diameter / Length: 1.000	{1} 2.4	Pipe	2.407	Diam/Width:335	Manhole
E:728913.397 N:4370628.169	1.633		{2} TD28	Pipe	2.875	Diam/Width:209 Diam/Width:209	
			{3} RJ28	Pipe	3.624		
			{a} 2.5	Pipe	2.407	Diam/Width:335	Not Applicable
MH17	4.164 2.307	Diameter / Length: 1.000	{1} 2.5	Pipe	2.307	Diam/Width:335	Manhole
E:728937.915 N:4370632.893	1.857		{2} RJ29	Pipe	3.742	Diam/Width:209 Diam/Width:209	
			{3} TD29	Pipe	2.954		
			{a} 2.6	Pipe	2.307	Diam/Width:335	Not Applicable
MH18	4.275 2.126	Diameter / Length: 1.000	{1} 2.6	Pipe	2.209	Diam/Width:335	Manhole
E:728961.980 N:4370637.875	2.149		{2} RP3-1	Pipe	3.080	Diam/Width:209	
			{a} 2.7	Pipe	2.126	Diam/Width:418	Not Applicable

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH19	4.319 2.027	Diameter / Length: 1.000	{1} 2.7	Pipe	2.027	Diam/Width:418	Manhole
E:728986.180 N:4370642.920	2.292						
			{a} 2.8	Pipe	2.027	Diam/Width:418	Not Applicable
MH20	4.255 1.930	Diameter / Length: 1.000	{1} 2.8	Pipe	1.930	Diam/Width:418	Manhole
E:729009.802 N:4370648.252	2.325						
			{a} 2.9	Pipe	1.930	Diam/Width:418	Not Applicable
MH21	4.129 1.842	Diameter / Length: 1.000	{1} 2.9	Pipe	1.842	Diam/Width:418	Manhole
E:729031.296 N:4370653.181	2.287		{2} RJ30	Pipe	3.644	Diam/Width:209	
			{3} TD30	Pipe	2.850	Diam/Width:209	
			{a} 2.10	Pipe	1.842	Diam/Width:418	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH22	4.009 1.762	Diameter / Length: 1.000	{1} 2.10	Pipe	1.762	Diam/Width:418	Manhole
E:729050.663 N:4370657.800	2.247		{2} TD31	Pipe	2.863	Diam/Width:209	
			{3} RJ31	Pipe	3.631	Diam/Width:209	
			{4} RP3-2	Pipe	3.255	Diam/Width:209	
			{a} 2.11	Pipe	1.762	Diam/Width:418	Not Applicable
MH23	3.992 1.707	Diameter / Length: 1.000	{1} 2.11	Pipe	1.707	Diam/Width:418	Manhole
E:729054.348 N:4370644.631	2.285						
			{a} 2.12	Pipe	1.707	Diam/Width:418	Not Applicable
MH28	3.624 2.224	Diameter / Length: 1.000	{1} RP10	Pipe	2.886	Diam/Width:209	Manhole
E:729118.774 N:4370653.043	1.400		{2} RJ45	Pipe	3.226	Diam/Width:209	
			{3} TD45	Pipe	2.495	Diam/Width:209	
			{a} 3.1	Pipe	2.224	Diam/Width:335	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH29	3.574 2.099	Diameter / Length: 1.000	{1} 3.1	Pipe	2.099	Diam/Width:335	Manhole
E:729142.712 N:4370659.765	1.476		{2} TD46	Pipe	2.556	Diam/Width:209 Diam/Width:209	
			{3} RJ46	Pipe	3.273		
			{a} 3.2	Pipe	2.099	Diam/Width:335	Not Applicable
MH30	3.664 1.974	Diameter / Length: 1.000	{1} 3.2	Pipe	1.974	Diam/Width:335	Manhole
E:729166.457 N:4370667.278	1.690						
			{a} 3.3	Pipe	1.974	Diam/Width:335	Not Applicable
MH31	3.700 1.849	Diameter / Length: 1.000	{1} 3.3	Pipe	1.849	Diam/Width:335	Manhole
E:729190.336 N:4370674.683	1.851		{2} RP11-1	Pipe	2.807	Diam/Width:209 Diam/Width:209	
			{3} RP11-2	Pipe	2.737		
			{a} 3.4	Pipe	1.849	Diam/Width:335	Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH32	3.616 1.724	Diameter / Length: 1.000	{1} 3.4	Pipe	1.724	Diam/Width:335	Manhole
E:729214.214 N:4370682.088	1.892		{2} RJ48	Pipe	3.258	Diam/Width:209	
			{3} TD48	Pipe	2.465	Diam/Width:209	
			{a} 3.5	Pipe	1.724	Diam/Width:335	Not Applicable
MH33	3.667 0.950	Diameter / Length: 1.500	{1} 3.5	Pipe	1.599	Diam/Width:335	Manhole
E:729236.734 N:4370688.984	2.717		{2} RP12	Pipe	2.865	Diam/Width:209	
			{3} 4.3	Pipe	1.211	Diam/Width:335	
			{4} 7.12	Pipe	1.055	Diam/Width:418	
			{a} 7.13	Pipe	0.950	Diam/Width:335	Not Applicable
MH34	3.869 1.817	Diameter / Length: 1.000	{1} RJ49	Pipe	3.518	Diam/Width:209	Manhole
E:729259.905 N:4370696.111	2.052		{2} TD49	Pipe	2.768	Diam/Width:209	
			{3} 4.2	Pipe	1.817	Diam/Width:335	
			{a} 4.3	Pipe	1.817	Diam/Width:335	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH47	3.576 0.795	Diameter / Length: 1.500	{1} 7.13	Pipe	0.795	Diam/Width:335	Manhole
E:729243.459 N:4370672.088	2.780						
			{a} 7.14	Pipe	0.795	Diam/Width:335	Not Applicable
Vertido2	3.055 0.608	Diameter / Length: 1.600	{1} 7.14	Pipe	0.608	Diam/Width:335	Manhole
E:729251.657 N:4370651.699	2.447						
		Width: 3.600					Not Applicable
MH35	4.210 2.647	Diameter / Length: 1.000	{1} RJ50	Pipe	3.959	Diam/Width:209	Manhole
E:729299.120 N:4370709.608	1.563		{2} TD50	Pipe	3.188	Diam/Width:209	
			{a} 4.1	Pipe	2.647	Diam/Width:335	Not Applicable
MH36	3.864 2.464	Diameter / Length: 1.000	{1} RJ32	Pipe	3.350	Diam/Width:209	Manhole
E:729074.271 N:4370663.572	1.400		{2} TD32	Pipe	2.621	Diam/Width:209	
			{a} 5.1	Pipe	2.464	Diam/Width:335	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH37	3.714 2.364	Diameter / Length: 1.000	{1} 5.1	Pipe	2.364	Diam/Width:335	Manhole
E:729098.455 N:4370669.794	1.350		{2} RP4	Pipe	3.011	Diam/Width:335	
			{a} 5.2	Pipe	2.364	Diam/Width:335	Not Applicable
MH38	3.588 2.264	Diameter / Length: 1.000	{1} 5.2	Pipe	2.264	Diam/Width:335	Manhole
E:729122.598 N:4370676.402	1.324		{2} TD33	Pipe	2.264	Diam/Width:209	
			{3} RJ33	Pipe	3.012	Diam/Width:209	
			{a} 5.3	Pipe	2.264	Diam/Width:335	Not Applicable
MH39	3.589 2.164	Diameter / Length: 1.000	{1} 5.3	Pipe	2.164	Diam/Width:335	Manhole
E:729146.724 N:4370682.920	1.425		{2} TD34	Pipe	2.208	Diam/Width:209	
			{3} RJ34	Pipe	3.004	Diam/Width:209	
			{a} 5.4	Pipe	2.164	Diam/Width:335	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH40	3.677 2.064	Diameter / Length: 1.000	{1} 5.4	Pipe	2.064	Diam/Width:335	Manhole
E:729170.752 N:4370689.818	1.613		{2} TD35	Pipe	2.411	Diam/Width:209	
			{3} RJ35	Pipe	3.164	Diam/Width:209	
			{4} RP5-1	Pipe	2.918	Diam/Width:209	
			{a} 5.5	Pipe	2.064	Diam/Width:335	Not Applicable
MH41	3.637 1.914	Diameter / Length: 1.000	{1} 5.5	Pipe	1.914	Diam/Width:335	Manhole
E:729194.749 N:4370696.949	1.723		{2} RP5-2	Pipe	2.957	Diam/Width:209	
			{a} 5.6	Pipe	1.914	Diam/Width:335	Not Applicable
MH42	3.588 1.226	Diameter / Length: 1.000	{1} 5.6	Pipe	1.780	Diam/Width:335	Manhole
E:729216.121 N:4370703.491	2.362		{2} 7.10	Pipe	1.309	Diam/Width:335	
			{a} 7.11	Pipe	1.226	Diam/Width:418	Not Applicable

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Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH43	3.635 1.155	Diameter / Length: 1.000	{1} 7.11	Pipe	1.155	Diam/Width:418	Manhole
E:729229.613 N:4370707.647	2.480		{2} RP6-1	Pipe	2.961	Diam/Width:209	
			{3} 6.3	Pipe	1.245	Diam/Width:335	
			{a} 7.12	Pipe	1.155	Diam/Width:418	Not Applicable
MH44	3.770 1.449	Diameter / Length: 1.000	{1} TD37	Pipe	2.483	Diam/Width:209	Manhole
E:729245.126 N:4370712.651	2.322		{2} RJ37	Pipe	3.366	Diam/Width:209	
			{3} 6.2	Pipe	1.449	Diam/Width:335	
			{a} 6.3	Pipe	1.449	Diam/Width:335	Not Applicable
MH46	3.960 1.688	Diameter / Length: 1.000	{1} 6.1	Pipe	1.688	Diam/Width:335	Manhole
E:729263.341 N:4370718.553	2.273						
			{a} 6.2	Pipe	1.688	Diam/Width:335	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH45	4.164 2.000	Diameter / Length: 1.000	{1} RJ38 {2} TD38 {3} RP6-2	Pipe Pipe Pipe	3.700 2.919 3.431	Diam/Width:209 Diam/Width:209 Diam/Width:209	Manhole
E:729287.005 N:4370726.617	2.164		{a} 6.1	Pipe	2.000	Diam/Width:335	Not Applicable
Manhole (26)	3.292 1.874	Diameter / Length: 1.000	{1} RJ11 {2} TD11	Pipe Pipe	2.651 1.874	Diam/Width:209 Diam/Width:209	Manhole
E:728978.678 N:4370925.509	1.417						Not Applicable
Manhole (27)	3.242 2.082	Diameter / Length: 1.000	{1} RJ58 {2} TD58 {3} RJ60 {4} TD60	Pipe Pipe Pipe Pipe	3.010 2.259 2.817 2.082	Diam/Width:209 Diam/Width:209 Diam/Width:209 Diam/Width:209	Manhole
E:728971.568 N:4370904.118	1.160						Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (28)	3.104 1.867	Diameter / Length: 1.000	{1} RJ10	Pipe	2.579	Diam/Width:209	Manhole
E:729085.088	1.237		{2} RJ9	Pipe	2.648	Diam/Width:209	
N:4370896.219			{3} TD10	Pipe	1.867	Diam/Width:209	
			{4} TD9	Pipe	1.904	Diam/Width:209	
							Not Applicable
Manhole (29)	3.158 1.924	Diameter / Length: 1.000	{1} RJ8	Pipe	2.683	Diam/Width:209	Manhole
E:729109.348	1.234		{2} TD8	Pipe	1.924	Diam/Width:209	
N:4370890.181							
							Not Applicable
Manhole (30)	3.283 2.049	Diameter / Length: 1.000	{1} RJ7	Pipe	2.819	Diam/Width:209	Manhole
E:729133.607	1.234		{2} TD7	Pipe	2.049	Diam/Width:209	
N:4370884.143							
							Not Applicable
Manhole (31)	3.533 2.056	Diameter / Length: 1.000	{1} RJ6	Pipe	2.056	Diam/Width:209	Manhole
E:729182.127	1.477		{2} TD6	Pipe	2.056	Diam/Width:209	
N:4370872.068							
							Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (32)	3.658 2.347	Diameter / Length: 1.000	{1} TD5	Pipe	2.347	Diam/Width:209	Manhole
E:729206.387	1.311		{2} RJ5	Pipe	3.105	Diam/Width:209	
N:4370866.030							
							Not Applicable
Manhole (33)	3.784 2.521	Diameter / Length: 1.000	{1} RJ4	Pipe	3.243	Diam/Width:209	Manhole
E:729230.647	1.263		{2} TD4	Pipe	2.521	Diam/Width:209	
N:4370859.993							
							Not Applicable
Manhole (34)	3.908 2.673	Diameter / Length: 1.000	{1} RJ3	Pipe	3.390	Diam/Width:209	Manhole
E:729254.907	1.236		{2} TD3	Pipe	2.673	Diam/Width:209	
N:4370853.955							
							Not Applicable
Manhole (36)	3.465 1.856	Diameter / Length: 1.000	{1} RJ1	Pipe	1.856	Diam/Width:209	Manhole
E:729331.734	1.609		{2} TD1	Pipe	1.856	Diam/Width:209	
N:4370832.453			{3} RJ2	Pipe	2.703	Diam/Width:209	
			{4} TD2	Pipe	2.007	Diam/Width:209	
							Not Applicable

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
	Designed by: FMA	Checked by: GGA	Approved By:	
Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (38)	3.297 2.135	Diameter / Length: 1.000	{1} TD12	Pipe	2.371	Diam/Width:209	Manhole
E:729333.901	1.162		{2} RJ12	Pipe	3.135	Diam/Width:209	
N:4370811.810			{3} TD55	Pipe	2.135	Diam/Width:209	
			{4} RJ55	Pipe	2.955	Diam/Width:209	
			{5} RJ22	Pipe	2.217	Diam/Width:209	
			{6} TD22	Pipe	2.224	Diam/Width:209	
							Not Applicable
Manhole (39)	3.629 2.755	Diameter / Length: 1.000	{1} RJ13	Pipe	3.486	Diam/Width:209	Manhole
E:729309.636	0.874		{2} TD13	Pipe	2.755	Diam/Width:209	
N:4370817.826							
							Not Applicable
Manhole (40)	3.877 2.898	Diameter / Length: 1.000	{1} TD14	Pipe	2.898	Diam/Width:209	Manhole
E:729261.106	0.978		{2} RJ14	Pipe	3.587	Diam/Width:209	
N:4370829.860							
							Not Applicable

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
	Designed by: FMA	Checked by: GGA	Approved By:	
Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (41)	3.751 2.685	Diameter / Length: 1.000	{1} TD15 {2} RJ15	Pipe Pipe	2.685 3.411	Diam/Width:209 Diam/Width:209	Manhole
E:729236.826 N:4370835.842	1.066						Not Applicable
Manhole (42)	3.626 2.399	Diameter / Length: 1.000	{1} TD16 {2} RJ16	Pipe Pipe	2.399 3.053	Diam/Width:209 Diam/Width:209	Manhole
E:729212.574 N:4370841.885	1.227						Not Applicable
Manhole (43)	3.378 2.434	Diameter / Length: 1.000	{1} RJ17 {2} TD17 {3} TD56 {4} RJ56	Pipe Pipe Pipe Pipe	3.219 2.450 2.434 3.216	Diam/Width:209 Diam/Width:209 Diam/Width:209 Diam/Width:209	Manhole
E:729164.074 N:4370854.038	0.944						Not Applicable
Manhole (44)	3.246 2.206	Diameter / Length: 1.000	{1} TD18 {2} RJ18	Pipe Pipe	2.206 2.901	Diam/Width:209 Diam/Width:209	Manhole
E:729139.778 N:4370859.738	1.040						Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (45)	3.127 1.939	Diameter / Length: 1.000	{1} RJ19 {2} TD19	Pipe Pipe	2.728 1.939	Diam/Width:209 Diam/Width:209	Manhole
E:729115.549 N:4370866.087	1.189						
							Not Applicable
Manhole (46)	3.001 2.030	Diameter / Length: 1.000	{1} TD20 {2} RJ20	Pipe Pipe	2.030 2.742	Diam/Width:209 Diam/Width:209	Manhole
E:729091.273 N:4370872.059	0.971						
							Not Applicable
Manhole (47)	3.075 2.232	Diameter / Length: 1.000	{1} RJ21 {2} TD21 {3} RJ57 {4} TD57	Pipe Pipe Pipe Pipe	2.962 2.232 3.066 2.389	Diam/Width:209 Diam/Width:209 Diam/Width:209 Diam/Width:209	Manhole
E:729066.945 N:4370878.032	0.843						
							Not Applicable
Manhole (48)	3.296 2.340	Diameter / Length: 1.000	{1} RJ23 {2} TD23	Pipe Pipe	2.939 2.340	Diam/Width:209 Diam/Width:209	Manhole
E:729363.517 N:4370797.124	0.956						
							Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (50)	3.315 2.113	Diameter / Length: 1.000	{1} RJ61	Pipe	2.836	Diam/Width:209	Manhole
E:728956.505 N:4370907.968	1.202		{2} TD61	Pipe	2.113	Diam/Width:209	
							Not Applicable
Manhole	2.724 0.872	Diameter / Length: 1.000	{1} RZB1	Pipe	2.270	Diam/Width:335	Manhole
E:729384.695 N:4370831.058	1.852		{2} DZB1	Pipe	0.872	Diam/Width:335	
							Not Applicable
Manhole (1)	2.545 1.108	Diameter / Length: 1.000	{1} TDB26	Pipe	1.108	Diam/Width:209	Manhole
E:728891.725 N:4370786.436	1.437		{2} RBB26	Pipe	1.895	Diam/Width:209	
							Not Applicable
MH55	3.600 1.558	Diameter / Length: 1.000	{1} 7.7	Pipe	1.558	Diam/Width:335	Manhole
E:729180.964 N:4370733.999	2.042		{a} 7.8	Pipe	1.558	Diam/Width:335	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH57	3.546 1.373	Diameter / Length: 1.000	{1} 7.9	Pipe	1.387	Diam/Width:335	Manhole
E:729205.729 N:4370715.638	2.173		{2} RBB7	Pipe	3.042	Diam/Width:209 Diam/Width:209	
			{3} TDB7	Pipe	2.204	Diam/Width:335 Diam/Width:209	
			{4} 8.7	Pipe	1.383	Diam/Width:209 Diam/Width:209	
			{5} RJ36	Pipe	3.405	Diam/Width:209 Diam/Width:209	
			{6} TD36	Pipe	2.647		
			{7} RBB6	Pipe	3.008		
			{8} TDB6	Pipe	2.236		
			{a} 7.10	Pipe	1.373	Diam/Width:335	Not Applicable
Manhole (8)	2.606 1.400	Diameter / Length: 1.000	{1} RBB15	Pipe	1.400	Diam/Width:209	Manhole
E:729407.350 N:4370933.298	1.206		{2} TDB15	Pipe	1.400	Diam/Width:209	
							Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (9)	2.880 1.138	Diameter / Length: 1.000	{1} RBB14	Pipe	2.087	Diam/Width:209	Manhole
E:729565.359 N:4370978.360	1.742		{2} TDB14	Pipe	1.138	Diam/Width:209	
							Not Applicable
Manhole (10)	3.200 1.689	Diameter / Length: 1.000	{1} RJ59	Pipe	2.412	Diam/Width:209	Manhole
E:729002.938 N:4370919.472	1.512		{2} TD59	Pipe	1.689	Diam/Width:209	
							Not Applicable
Manhole (11)	4.053 2.447	Diameter / Length: 1.000	{1} RB65	Pipe	3.126	Diam/Width:209	Manhole
E:728831.007 N:4370873.800	1.606		{2} TD65	Pipe	2.447	Diam/Width:209	
							Not Applicable
Manhole (12)	3.872 2.457	Diameter / Length: 1.000	{1} RB64	Pipe	3.208	Diam/Width:209	Manhole
E:728855.267 N:4370867.762	1.416		{2} TD64	Pipe	2.457	Diam/Width:209	
							Not Applicable
Manhole (13)	3.509 1.984	Diameter / Length: 1.000	{1} RB63	Pipe	2.552	Diam/Width:209	Manhole
E:728903.787 N:4370855.687	1.525		{2} TD63	Pipe	1.984	Diam/Width:209	
							Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (14)	3.327 1.814	Diameter / Length: 1.000	{1} TD62	Pipe	1.814	Diam/Width:209	Manhole
E:728928.047 N:4370849.650	1.514		{2} RB62	Pipe	2.479	Diam/Width:209	
							Not Applicable
MH48	3.700 2.240	Diameter / Length: 1.000	{1} TDB3	Pipe	2.240	Diam/Width:209	Manhole
E:729015.633 N:4370724.156	1.460		{2} RBB3	Pipe	3.243	Diam/Width:209	
			{a} 7.1	Pipe	2.240	Diam/Width:335	Not Applicable
MH49	3.700 2.140	Diameter / Length: 1.000	{1} 7.1	Pipe	2.140	Diam/Width:335	Manhole
E:729040.336 N:4370728.511	1.560						
			{a} 7.2	Pipe	2.140	Diam/Width:335	Not Applicable
MH50	3.700 2.040	Diameter / Length: 1.000	{1} 7.2	Pipe	2.040	Diam/Width:335	Manhole
E:729064.705 N:4370733.950	1.660						
			{a} 7.3	Pipe	2.040	Diam/Width:335	Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH51	3.650 1.941	Diameter / Length: 1.000	{1} 7.3	Pipe	1.941	Diam/Width:335	Manhole
E:729089.058 N:4370738.092	1.709		{2} RBB4	Pipe	2.953	Diam/Width:209 Diam/Width:209	
			{3} TDB4	Pipe	2.326		
			{a} 7.4	Pipe	1.941	Diam/Width:335	Not Applicable
MH52	3.600 1.842	Diameter / Length: 1.000	{1} 7.4	Pipe	1.842	Diam/Width:335	Manhole
E:729113.199 N:4370743.254	1.758						
			{a} 7.5	Pipe	1.842	Diam/Width:335	Not Applicable
MH53	3.550 1.742	Diameter / Length: 1.000	{1} 7.5	Pipe	1.742	Diam/Width:335	Manhole
E:729137.561 N:4370748.615	1.808		{2} TDB5	Pipe	2.204	Diam/Width:209 Diam/Width:209	
			{3} RBB5	Pipe	2.962		
			{a} 7.6	Pipe	1.742	Diam/Width:335	Not Applicable
MH56	3.600 1.464	Diameter / Length: 1.000	{1} 7.8	Pipe	1.464	Diam/Width:335	Manhole
E:729186.978 N:4370711.205	2.136						
			{a} 7.9	Pipe	1.464	Diam/Width:335	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH63	3.700 1.630	Diameter / Length: 1.000	{1} RBB8	Pipe	2.140	Diam/Width:209	Manhole
E:729230.913 N:4370753.314	2.070		{2} TDB8	Pipe	2.437	Diam/Width:209	
			{3} 8.5	Pipe	1.630	Diam/Width:335	
			{a} 8.6	Pipe	1.630	Diam/Width:335	Not Applicable
MH64	3.650 1.518	Diameter / Length: 1.000	{1} 8.6	Pipe	1.518	Diam/Width:335	Manhole
E:729232.779 N:4370728.403	2.132						
			{a} 8.7	Pipe	1.518	Diam/Width:335	Not Applicable
Manhole (2)	2.755 1.406	Diameter / Length: 1.000	{1} RBB18	Pipe	2.260	Diam/Width:209	Manhole
E:729431.729 N:4370791.098	1.350		{2} TDB18	Pipe	1.406	Diam/Width:209	
							Not Applicable
Manhole (3)	3.070 1.247	Diameter / Length: 1.000	{1} RBB17	Pipe	2.017	Diam/Width:209	Manhole
E:729471.678 N:4370789.105	1.824		{2} TDB17	Pipe	1.247	Diam/Width:209	
							Not Applicable

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Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (4)	3.605 1.703	Diameter / Length: 1.000	{1} TDB22	Pipe	1.703	Diam/Width:209	Manhole
E:729517.931 N:4370777.256	1.902		{2} RBB22	Pipe	2.567	Diam/Width:209	
							Not Applicable
Manhole (5)	4.000 2.709	Diameter / Length: 1.000	{1} TDB25	Pipe	2.709	Diam/Width:209	Manhole
E:729630.848 N:4370621.593	1.291		{2} RBB25	Pipe	3.473	Diam/Width:209	
							Not Applicable
Manhole (6)	3.300 2.198	Diameter / Length: 1.000	{1} TDB24	Pipe	2.198	Diam/Width:209	Manhole
E:729572.814 N:4370660.888	1.102		{2} RBB24	Pipe	3.019	Diam/Width:209	
							Not Applicable
Manhole (15)	3.373 0.872	Diameter / Length: 1.000	{1} RBB13	Pipe	2.021	Diam/Width:209	Manhole
E:729574.388 N:4370797.581	2.501		{2} TDB13	Pipe	0.872	Diam/Width:209	
							Not Applicable
Manhole (16)	2.993 1.612	Diameter / Length: 1.000	{1} RBB21	Pipe	2.393	Diam/Width:209	Manhole
E:729585.914 N:4370819.667	1.381		{2} TDB21	Pipe	1.612	Diam/Width:209	
							Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (17)	3.788 1.374	Diameter / Length: 1.000	{1} RBB23	Pipe	2.133	Diam/Width:209	Manhole
E:729562.106	2.414		{2} TDB23	Pipe	1.374	Diam/Width:209	
N:4370723.998							Not Applicable
Manhole (18)	3.000 2.294	Diameter / Length: 1.000	{1} RBB12	Pipe	2.435	Diam/Width:209	Manhole
E:729713.142	0.706		{2} TDB12	Pipe	2.294	Diam/Width:209	
N:4370698.137							Not Applicable
MH65	2.850 1.380	Diameter / Length: 1.000	{1} RBB19	Pipe	2.363	Diam/Width:209	Manhole
E:729558.335	1.470		{2} TDB19	Pipe	1.380	Diam/Width:209	
N:4370871.652			{a} 9.1	Pipe	1.380	Diam/Width:335	Not Applicable
MH66	3.044 0.715	Diameter / Length: 1.000	{1} 9.1	Pipe	1.264	Diam/Width:335	Manhole
E:729573.414	2.329		{2} 10.5	Pipe	0.715	Diam/Width:335	
N:4370854.136			{a} 10.6	Pipe	0.715	Diam/Width:335	Not Applicable
Manhole (19)	3.049 0.604	Diameter / Length: 1.000	{1} 10.6	Pipe	0.604	Diam/Width:335	Manhole
E:729591.703	2.445						
N:4370833.258							Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH69	2.896 0.998	Diameter / Length: 1.000	{1} RBB16	Pipe	2.349	Diam/Width:209	Manhole
E:729503.099 N:4370849.869	1.898		{2} TDB16	Pipe	1.347	Diam/Width:209	
			{3} 10.2	Pipe	0.998	Diam/Width:335	
			{a} 10.3	Pipe	0.998	Diam/Width:335	Not Applicable
MH67	2.759 1.195	Diameter / Length: 1.000	{1} RBB20	Pipe	1.527	Diam/Width:209	Manhole
E:729490.914 N:4370897.532	1.564		{2} TDB20	Pipe	2.341	Diam/Width:209	
			{a} 10.1	Pipe	1.195	Diam/Width:335	Not Applicable
Manhole (24)	3.091 1.912	Diameter / Length: 1.000	{1} RBB2	Pipe	2.680	Diam/Width:209	Manhole
E:728943.813 N:4370747.780	1.179		{2} TDB2	Pipe	1.912	Diam/Width:209	
							Not Applicable
Manhole (25)	3.503 2.256	Diameter / Length: 1.000	{1} RBB27	Pipe	3.056	Diam/Width:209	Manhole
E:728894.260 N:4370694.285	1.247		{2} TDB27	Pipe	2.256	Diam/Width:209	
							Not Applicable

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
Manhole (37)	3.421 1.644	Diameter / Length: 1.000	{1} RBB1	Pipe	2.478	Diam/Width:209	Manhole
E:728916.190 N:4370705.682	1.777		{2} TDB1	Pipe	1.644	Diam/Width:209	
							Not Applicable
Manhole (49)	2.759 1.350	Diameter / Length: 1.000	{1} RBB11	Pipe	2.328	Diam/Width:209	Manhole
E:728991.756 N:4370832.367	1.409		{2} TDB11	Pipe	1.350	Diam/Width:209	
							Not Applicable
MH68	2.672 1.095	Diameter / Length: 1.000	{1} 10.1	Pipe	1.095	Diam/Width:335	Manhole
E:729497.010 N:4370873.252	1.577						
			{a} 10.2	Pipe	1.095	Diam/Width:335	Not Applicable
MH70	2.948 0.898	Diameter / Length: 1.000	{1} 10.3	Pipe	0.898	Diam/Width:335	Manhole
E:729527.865 N:4370853.123	2.050						
			{a} 10.4	Pipe	0.898	Diam/Width:335	Not Applicable
MH71	3.010 0.800	Diameter / Length: 1.000	{1} 10.4	Pipe	0.800	Diam/Width:335	Manhole
E:729552.263 N:4370855.843	2.210						
			{a} 10.5	Pipe	0.800	Diam/Width:335	Not Applicable

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Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH54	3.500 1.642	Diameter / Length: 1.200	{1} 7.6	Pipe	1.642	Diam/Width:335	Manhole
E:729161.880 N:4370742.878	1.858						
			{a} 7.7	Pipe	1.642	Diam/Width:335	Not Applicable
MH58	3.400 2.186	Diameter / Length: 1.200	{1} RBB10 {2} TDB10	Pipe Pipe	2.962 2.186	Diam/Width:209 Diam/Width:209	Manhole
E:729121.139 N:4370796.983	1.214						
			{a} 8.1	Pipe	2.186	Diam/Width:335	Not Applicable
MH59	3.400 2.074	Diameter / Length: 1.200	{1} 8.1	Pipe	2.074	Diam/Width:335	Manhole
E:729145.434 N:4370791.249	1.326						
			{a} 8.2	Pipe	2.074	Diam/Width:335	Not Applicable
MH60	3.303 1.961	Diameter / Length: 1.200	{1} 8.2	Pipe	1.961	Diam/Width:335	Manhole
E:729169.623 N:4370784.988	1.342						
			{a} 8.3	Pipe	1.961	Diam/Width:335	Not Applicable

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
	Designed by: FMA	Checked by: GGA	Approved By:	
Report Details: Type: Manhole Schedule Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Name	Cover Elevation (m) Invert Elevation (m)	Manhole Size (m)	Connection Details				Type
Coordinates (m)	Depth (m)		Incoming Connections	Connection Type	Connection Invert (m)	Connection Size (mm)	Junction Type
			Outgoing Connections				Cover
MH62	3.574 1.737	Diameter / Length: 1.200	{1} 8.4	Pipe	1.737	Diam/Width:335	Manhole
E:729218.031 N:4370773.102	1.837						
			{a} 8.5	Pipe	1.737	Diam/Width:335	Not Applicable
MH61	3.503 1.848	Diameter / Length: 1.200	{1} 8.3	Pipe	1.848	Diam/Width:335	Manhole
E:729194.091 N:4370779.015	1.655		{2} RBB9	Pipe	2.906	Diam/Width:209	
			{3} TDB9	Pipe	2.179	Diam/Width:209	
			{a} 8.4	Pipe	1.848	Diam/Width:335	Not Applicable
MH 35.1	4.006 2.147	Diameter / Length: 1.200	{1} 4.1	Pipe	2.147	Diam/Width:335	Manhole
E:729275.551 N:4370701.277	1.859						
			{a} 4.2	Pipe	2.147	Diam/Width:335	Not Applicable

Proyecto:	Date:		
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025		
	Designed by: FMA	Checked by: GGA	Approved By:
Report Details: Type: Stormwater Controls Summary Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia		

Grupo TYPSA

Critical Storm Per Item: Rank By: Max. Resident Volume

Stormwater Control	Storm Event	Max. US Elevation (m)	Max. DS Elevation (m)	Max. US Depth (m)	Max. DS Depth (m)	Max. Inflow (L/s)	Max. Resident Volume (m³)	Max. Flooded Volume (m³)	Total Lost Volume (m³)	Max. Outflow (L/s)	Total Discharge Volume (m³)	Percentage Available (%)	Status
JLL55	T25 Valencia: +0 %: T25 Valencia90	2.719	2.516	0.000	0.000	0.6	5.944	0.000	0.000	0.0	0.000	96.409	OK
JLL56	T25 Valencia: +0 %: T25 Valencia90	3.212	2.724	0.000	0.000	1.5	14.371	0.000	0.000	0.0	0.000	96.431	OK
JLL57	T25 Valencia: +0 %: T25 Valencia90	3.136	2.691	0.000	0.000	1.3	13.107	0.000	0.000	0.0	0.000	96.433	OK
JLL58	T25 Valencia: +0 %: T25 Valencia90	2.709	2.470	0.000	0.000	0.7	6.936	0.000	0.000	0.0	0.000	96.421	OK
JLL2	T25 Valencia: +0 %: T25 Valencia20	3.478	3.468	0.659	0.775	10.7	6.873	0.000	0.000	10.3	12.580	46.165	OK
JLL1	T25 Valencia: +0 %: T25 Valencia30	3.166	3.160	0.651	0.770	7.8	7.143	0.000	0.000	7.6	13.854	48.366	OK
JLL3	T25 Valencia: +0 %: T25 Valencia20	3.808	3.799	0.727	0.781	14.2	9.071	0.000	0.000	13.7	16.678	34.454	OK
JLL4	T25 Valencia: +0 %: T25 Valencia30	3.655	3.651	0.712	0.771	8.2	8.539	0.000	0.000	8.0	14.398	38.298	OK
JLL5	T25 Valencia: +0 %: T25 Valencia30	3.517	3.513	0.712	0.771	8.3	8.549	0.000	0.000	8.0	14.558	38.224	OK
JLL6	T25 Valencia: +0 %: T25 Valencia30	3.366	3.360	0.708	0.774	10.1	9.953	0.000	0.000	9.8	17.829	38.012	OK
JLL7	T25 Valencia: +0 %: T25 Valencia30	3.198	3.193	0.715	0.773	9.6	8.696	0.000	0.000	9.3	16.878	37.163	OK
JLL8	T25 Valencia: +0 %: T25 Valencia30	3.057	3.053	0.712	0.771	8.2	8.540	0.000	0.000	8.0	14.413	38.289	OK
JLL9	T25 Valencia: +0 %: T25 Valencia30	3.023	3.019	0.713	0.771	8.3	8.585	0.000	0.000	8.0	14.554	37.965	OK
JLL10	T25 Valencia: +0 %: T25 Valencia20	3.048	3.040	0.674	0.776	11.2	7.417	0.000	0.000	10.9	13.260	44.583	OK
JLL22	T25 Valencia: +0 %: T25 Valencia75	3.564	3.539	0.559	0.779	12.4	16.348	0.000	0.000	11.8	55.221	48.424	OK
JLL23	T25 Valencia: +0 %: T25 Valencia75	3.563	3.558	0.604	0.680	8.0	7.469	0.000	0.000	7.9	35.742	59.157	OK
JLL11	T25 Valencia: +0 %: T25 Valencia90	3.153	3.149	0.583	0.769	8.9	39.209	0.000	0.000	7.8	46.090	40.718	OK
JLL12	T25 Valencia: +0 %: T25 Valencia20	3.466	3.446	0.565	0.771	8.2	5.427	0.000	0.000	7.9	9.605	60.612	OK
JLL13	T25 Valencia: +0 %: T25 Valencia30	3.878	3.878	0.722	0.762	3.9	5.302	0.000	0.000	3.8	6.835	39.291	OK

JLL14	T25 Valencia: +0 %: T25 Valencia60	3.941	3.940	0.700	0.762	4.0	8.244	0.000	0.000	3.9	14.268	40.409	OK
JLL15	T25 Valencia: +0 %: T25 Valencia45	3.814	3.812	0.704	0.765	5.3	8.324	0.000	0.000	5.2	14.187	39.829	OK
JLL16	T25 Valencia: +0 %: T25 Valencia45	3.664	3.662	0.704	0.765	5.3	8.324	0.000	0.000	5.2	14.187	39.829	OK
JLL17	T25 Valencia: +0 %: T25 Valencia45	3.492	3.491	0.704	0.765	5.3	8.323	0.000	0.000	5.2	14.187	39.835	OK
JLL18	T25 Valencia: +0 %: T25 Valencia30	3.314	3.311	0.712	0.771	8.4	8.555	0.000	0.000	8.1	14.718	38.158	OK
JLL19	T25 Valencia: +0 %: T25 Valencia45	3.178	3.176	0.704	0.765	5.3	8.324	0.000	0.000	5.2	14.187	39.829	OK
JLL20	T25 Valencia: +0 %: T25 Valencia45	3.153	3.151	0.704	0.765	5.3	8.324	0.000	0.000	5.2	14.187	39.829	OK
JLL21	T25 Valencia: +0 %: T25 Valencia30	3.212	3.211	0.713	0.764	4.6	5.192	0.000	0.000	4.5	8.131	40.554	OK
JLL25	T25 Valencia: +0 %: T25 Valencia30	3.907	3.903	0.717	0.769	6.9	6.771	0.000	0.000	6.8	12.165	39.117	OK
JLL26	T25 Valencia: +0 %: T25 Valencia30	3.865	3.863	0.716	0.769	6.8	7.471	0.000	0.000	6.6	12.023	38.424	OK
JLL27	T25 Valencia: +0 %: T25 Valencia30	3.877	3.875	0.715	0.769	6.8	7.460	0.000	0.000	6.6	12.008	38.518	OK
JLL28	T25 Valencia: +0 %: T25 Valencia30	3.967	3.965	0.717	0.770	7.7	7.562	0.000	0.000	7.6	13.660	37.674	OK
JLL24	T25 Valencia: +0 %: T25 Valencia90	4.089	4.088	0.692	0.764	5.2	12.566	0.000	0.000	5.0	27.695	34.274	OK
JLL39	T25 Valencia: +0 %: T25 Valencia75	4.349	4.347	0.674	0.771	9.0	28.599	0.000	0.000	8.4	39.709	30.042	OK
JLL40	T25 Valencia: +0 %: T25 Valencia75	3.898	3.892	0.672	0.778	15.1	54.081	0.000	0.000	12.9	64.007	27.188	OK
JLL41	T25 Valencia: +0 %: T25 Valencia75	3.728	3.726	0.674	0.771	9.1	21.704	0.000	0.000	8.6	40.479	32.106	OK
JLL29	T25 Valencia: +0 %: T25 Valencia15	4.144	4.127	0.735	0.781	14.3	6.704	0.000	0.000	13.7	11.202	34.797	OK
JLL30	T25 Valencia: +0 %: T25 Valencia20	4.156	4.134	0.711	0.782	16.0	11.316	0.000	0.000	14.7	18.715	36.841	OK
JLL31	T25 Valencia: +0 %: T25 Valencia30	3.977	3.971	0.712	0.772	9.0	8.433	0.000	0.000	8.8	15.863	38.245	OK
JLL32	T25 Valencia: +0 %: T25 Valencia30	3.752	3.748	0.714	0.772	8.9	8.621	0.000	0.000	8.7	15.709	37.707	OK
JLL33	T25 Valencia: +0 %: T25 Valencia30	3.580	3.577	0.711	0.770	7.7	8.490	0.000	0.000	7.5	13.603	38.665	OK
JLL34	T25 Valencia: +0 %: T25 Valencia30	3.507	3.504	0.711	0.771	8.0	8.523	0.000	0.000	7.8	14.127	38.425	OK
JLL35	T25 Valencia: +0 %: T25 Valencia30	3.543	3.518	0.699	0.782	15.4	13.516	0.000	0.000	14.8	26.709	37.286	OK

JLL42	T25 Valencia: +0 %: T25 Valencia75	4.115	4.111	0.681	0.769	7.7	16.194	0.000	0.000	7.4	34.279	32.619	OK
JLL36	T25 Valencia: +0 %: T25 Valencia20	3.583	3.535	0.705	0.788	21.2	14.049	0.000	0.000	18.8	24.681	35.524	OK
JLL37	T25 Valencia: +0 %: T25 Valencia30	3.813	3.791	0.646	0.777	12.1	10.224	0.000	0.000	11.7	21.497	47.311	OK
JLL38	T25 Valencia: +0 %: T25 Valencia30	4.068	4.059	0.650	0.774	9.8	9.683	0.000	0.000	9.5	17.321	47.267	OK
JLL43	T25 Valencia: +0 %: T25 Valencia75	4.209	4.202	0.678	0.772	9.5	16.870	0.000	0.000	9.1	42.260	34.422	OK
JLL45	T25 Valencia: +0 %: T25 Valencia75	3.551	3.544	0.639	0.786	20.9	69.426	0.000	0.000	18.6	88.959	28.327	OK
JLL46	T25 Valencia: +0 %: T25 Valencia90	3.490	3.490	0.649	0.759	6.6	31.837	0.000	0.000	3.3	34.337	34.104	OK
JLL48	T25 Valencia: +0 %: T25 Valencia75	3.570	3.558	0.609	0.792	23.8	43.035	0.000	0.000	22.6	105.349	33.123	OK
JLL49	T25 Valencia: +0 %: T25 Valencia30	3.808	3.798	0.655	0.780	14.0	14.264	0.000	0.000	13.4	24.510	47.714	OK
JLL50	T25 Valencia: +0 %: T25 Valencia90	4.158	4.158	0.636	0.763	5.2	22.400	0.000	0.000	4.9	27.500	36.076	OK
JLL60	T25 Valencia: +0 %: T25 Valencia30	3.159	3.156	0.670	0.767	6.3	7.462	0.000	0.000	6.0	11.069	46.059	OK
JLL61	T25 Valencia: +0 %: T25 Valencia45	3.301	3.299	0.676	0.774	4.8	7.881	0.000	0.000	4.7	12.844	43.031	OK
PP2	T25 Valencia: +0 %: T25 Valencia45	3.861	3.470	0.140	0.058	14.8	18.089	0.000	0.000	10.6	39.920	44.526	OK
PP3-2	T25 Valencia: +0 %: T25 Valencia45	3.982	3.565	0.167	0.058	16.1	20.079	0.000	0.000	11.3	43.457	38.445	OK
PP4	T25 Valencia: +0 %: T25 Valencia45	3.599	3.146	0.196	0.056	17.8	22.692	0.000	0.000	12.0	47.880	31.467	OK
PP5-1	T25 Valencia: +0 %: T25 Valencia45	3.564	3.115	0.163	0.061	17.3	23.135	0.000	0.000	11.3	46.403	36.867	OK
PP6-1	T25 Valencia: +0 %: T25 Valencia30	3.563	3.137	0.090	0.074	16.1	13.702	0.000	0.000	11.2	28.922	49.175	OK
PP8	T25 Valencia: +0 %: T25 Valencia30	3.822	3.495	0.076	0.054	13.8	12.753	0.000	0.000	9.5	24.585	60.419	OK
PP9-2	T25 Valencia: +0 %: T25 Valencia45	3.907	3.577	0.074	0.052	11.5	12.897	0.000	0.000	9.1	30.834	60.474	OK
PP10	T25 Valencia: +0 %: T25 Valencia45	3.510	3.157	0.092	0.053	12.5	14.661	0.000	0.000	9.3	33.738	55.681	OK
PP11-1	T25 Valencia: +0 %: T25 Valencia45	3.471	3.103	0.069	0.052	12.1	14.931	0.000	0.000	9.1	32.561	59.678	OK
PP12	T25 Valencia: +0 %: T25 Valencia45	3.945	3.136	0.064	0.058	18.0	25.863	0.000	0.000	11.3	48.491	51.010	OK
PP1	T25 Valencia: +0 %: T25 Valencia30	3.763	3.480	0.124	0.058	13.8	10.720	0.000	0.000	10.1	24.785	53.353	OK

PP7	T25 Valencia: +0 %: T25 Valencia30	3.718	3.491	0.055	0.050	9.7	7.119	0.000	0.000	8.1	17.299	69.637	OK
PP3-1	T25 Valencia: +0 %: T25 Valencia30	4.020	3.712	0.127	0.054	14.7	11.976	0.000	0.000	10.4	26.350	51.830	OK
PP9-1	T25 Valencia: +0 %: T25 Valencia30	3.968	3.727	0.057	0.051	10.2	7.846	0.000	0.000	8.3	18.188	68.391	OK
PP5-2	T25 Valencia: +0 %: T25 Valencia15	3.314	3.120	0.053	0.057	10.4	3.207	0.000	0.000	9.6	9.369	75.214	OK
PP11-2	T25 Valencia: +0 %: T25 Valencia15	3.319	3.127	0.043	0.045	7.4	2.417	0.000	0.000	7.0	6.669	80.792	OK
JLL59	T25 Valencia: +0 %: T25 Valencia90	3.090	3.090	0.667	0.771	9.6	36.955	0.000	0.000	9.3	50.551	27.659	OK
JLL62	T25 Valencia: +0 %: T25 Valencia90	2.749	2.746	0.593	0.710	3.3	6.773	0.000	0.000	3.2	17.394	48.731	OK
JLL63	T25 Valencia: +0 %: T25 Valencia90	3.046	3.043	0.592	0.710	3.1	6.748	0.000	0.000	3.0	16.479	48.925	OK
JLL64	T25 Valencia: +0 %: T25 Valencia90	3.428	3.426	0.592	0.710	3.2	6.744	0.000	0.000	3.1	16.909	48.948	OK
JLL65	T25 Valencia: +0 %: T25 Valencia30	3.473	3.467	0.632	0.715	5.1	4.113	0.000	0.000	5.0	9.079	48.108	OK
ZBIO1	T25 Valencia: +0 %: T25 Valencia90	2.617	2.617	1.384	1.479	39.1	69.521	0.000	0.000	37.6	206.625	20.603	OK
BJLL-2	T25 Valencia: +0 %: T25 Valencia90	2.971	2.832	0.553	0.517	4.8	27.213	0.000	0.000	1.6	20.973	79.228	OK
BJLL-3	T25 Valencia: +0 %: T25 Valencia75	3.257	3.257	0.597	0.657	2.1	8.048	0.000	0.000	0.6	9.138	78.740	OK
BJLL-4	T25 Valencia: +0 %: T25 Valencia75	3.481	3.475	0.765	0.875	13.8	53.871	0.000	0.000	11.0	60.254	32.899	OK
BJLL-5	T25 Valencia: +0 %: T25 Valencia45	3.400	3.370	0.743	0.820	15.4	28.154	0.000	0.000	14.4	31.753	40.792	OK
BJLL-9	T25 Valencia: +0 %: T25 Valencia75	3.171	3.132	0.517	0.582	3.8	14.780	0.000	0.000	1.0	15.329	80.551	OK
BJLL-10	T25 Valencia: +0 %: T25 Valencia75	3.011	2.980	0.515	0.580	3.4	13.200	0.000	0.000	1.0	13.941	81.624	OK
BJLL-11	T25 Valencia: +0 %: T25 Valencia90	2.448	2.408	0.526	0.608	8.0	38.908	0.000	0.000	1.7	37.035	77.350	OK
BJLL-8	T25 Valencia: +0 %: T25 Valencia65	3.407	3.386	0.506	0.536	3.6	11.838	0.000	0.000	1.4	11.921	82.652	OK
BJLL-1	T25 Valencia: +0 %: T25 Valencia90	2.974	2.600	0.490	0.200	5.9	28.539	0.000	0.000	1.7	25.528	83.830	OK
BJLL-6	T25 Valencia: +0 %: T25 Valencia65	3.148	3.119	0.507	0.569	2.3	6.998	0.000	0.000	1.1	8.102	83.872	OK
BJLL-7	T25 Valencia: +0 %: T25 Valencia75	3.091	2.900	0.344	0.200	1.5	5.010	0.000	0.000	0.9	6.088	86.282	OK
BJLL-16	T25 Valencia: +0 %: T25 Valencia75	2.282	2.282	0.566	0.632	4.6	18.278	0.000	0.000	1.1	19.408	77.880	OK

BJLL-13	T25 Valencia: +0 %: T25 Valencia90	2.070	1.650	0.489	0.200	6.7	31.963	0.000	0.000	2.0	31.946	80.002	OK
BJLL-12	T25 Valencia: +0 %: T25 Valencia75	3.245	3.244	0.527	0.594	2.4	9.046	0.000	0.000	0.8	10.202	80.240	OK
BJLL-14	T25 Valencia: +0 %: T25 Valencia90	2.634	2.250	0.512	0.200	4.3	19.490	0.000	0.000	1.5	20.414	81.360	OK
BJLL-19	T25 Valencia: +0 %: T25 Valencia75	2.387	2.386	0.525	0.586	4.5	17.592	0.000	0.000	1.3	18.641	79.296	OK
BJLL-15	T25 Valencia: +0 %: T25 Valencia90	2.384	2.298	0.536	0.648	6.4	31.515	0.000	0.000	1.1	30.513	77.222	OK
BJLL-26	T25 Valencia: +0 %: T25 Valencia90	2.368	2.308	0.515	0.532	8.0	38.776	0.000	0.000	2.0	34.934	79.309	OK
BJLL-27	T25 Valencia: +0 %: T25 Valencia90	3.093	3.053	0.500	0.553	2.0	11.185	0.000	0.000	0.1	0.233	82.737	OK
BJLL-18	T25 Valencia: +0 %: T25 Valencia75	2.246	2.143	0.503	0.522	5.1	19.479	0.000	0.000	1.7	20.716	80.423	OK
BJLL-20	T25 Valencia: +0 %: T25 Valencia75	2.387	2.341	0.509	0.514	4.3	15.843	0.000	0.000	1.6	17.067	81.592	OK
BJLL-21	T25 Valencia: +0 %: T25 Valencia90	2.523	2.345	0.519	0.595	8.8	42.658	0.000	0.000	2.0	41.928	75.478	OK
BJLL-25	T25 Valencia: +0 %: T25 Valencia75	3.627	3.533	0.508	0.583	4.3	16.532	0.000	0.000	1.3	17.725	79.940	OK
BJLL-17	T25 Valencia: +0 %: T25 Valencia65	2.217	2.217	0.528	0.567	2.1	6.424	0.000	0.000	1.0	7.487	82.258	OK
BJLL-22	T25 Valencia: +0 %: T25 Valencia90	2.564	2.488	0.532	0.588	11.5	57.370	0.000	0.000	2.1	45.538	77.752	OK
BJLL-23	T25 Valencia: +0 %: T25 Valencia75	2.672	2.389	0.514	0.589	5.5	22.161	0.000	0.000	1.2	22.546	78.630	OK
BJLL-24	T25 Valencia: +0 %: T25 Valencia75	2.967	2.933	0.511	0.633	5.1	20.094	0.000	0.000	1.3	21.410	78.188	OK
PP6-2	T25 Valencia: +0 %: T25 Valencia30	3.957	3.558	0.067	0.063	14.4	11.444	0.000	0.000	10.5	25.843	55.922	OK

Proyecto:	Date:			
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025			Grupo TYPSA
	Designed by: FMA	Checked by: GGA	Approved By:	
Report Details: Type: Connections Summary Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia			

Critical Storm Per Item: Rank By: Max. Flow

Connection	Storm Event	Connection Type	From	To	Upstream Cover Elevation (m)	Max. US Water Elevation (m)	Max. Flow Depth (m)	Discharge Volume (m³)	Max. Velocity (m/s)	Flow / Capacity	Max. Flow (L/s)	Status
1.1	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH1	MH2	4.355	2.968	0.082	28.959	0.6	0.09	9.7	OK
1.2	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH2	MH3	4.232	2.898	0.095	47.392	0.8	0.17	16.3	OK
1.3	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH3	MH4	4.077	2.796	0.132	47.370	0.6	0.16	15.8	OK
1.4	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH4	MH5	3.981	2.771	0.170	136.558	1.0	0.45	43.2	OK
1.5	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH5	MH6	3.978	2.673	0.178	136.450	0.9	0.44	43.0	OK
1.6	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH6	MH7	4.087	2.587	0.203	167.287	1.0	0.5	53.8	OK
1.7	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH7	MH8	4.208	2.498	0.222	216.670	1.1	0.65	70.6	OK
1.8	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH8	MH9	4.310	2.378	0.235	216.561	1.1	0.65	70.4	OK
1.9	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH9	MH10	4.333	2.276	0.248	249.616	1.2	0.75	81.8	OK
1.10	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH10	MH11	4.243	2.153	0.253	249.481	1.1	0.75	81.9	OK
1.11	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH11	MH24	4.084	2.036	0.243	280.163	1.3	0.84	90.6	OK
1.12	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH24	MH25	3.944	1.790	0.306	478.404	1.6	0.57	205.6	OK
1.13	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH25	Vertido1	4.028	1.124	0.212	478.303	1.7	0.67	205.5	OK
RP7	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP7	MH4	4.042	3.533	0.048	17.299	1.4	0.11	8.1	OK
RP8	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP8	MH4	4.016	3.561	0.052	24.585	1.4	0.13	9.5	OK
RJ40	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL40	MH4	3.971	3.840	0.040	16.435	0.0	0.16	11.9	OK
TD40	T25 Valencia: +0 %: T25 Valencia15	Pipe	JLL40	MH4	3.954	3.754	0.018	14.097	0.8	0.01	1.1	Surcharged
TD41	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL41	MH6	4.069	3.677	0.015	21.242	0.7	0.01	0.8	Surcharged
RJ41	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL41	MH6	4.083	3.686	0.039	8.117	0.0	0.16	11.9	OK

RP9-1	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP9-1	MH7	4.234	3.772	0.049	18.188	1.4	0.11	8.3	OK
TD42	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL42	MH7	4.234	4.068	0.014	16.250	0.7	0.01	0.7	Surch arged
RJ42	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL42	MH7	4.243	4.077	0.028	8.444	0.0	0.15	11.0	OK
TD43	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL43	MH9	4.366	4.155	0.014	16.383	0.7	0.01	0.7	Surch arged
RJ43	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL43	MH9	4.370	4.169	0.040	13.325	0.0	0.19	14.0	OK
2.1	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH12	MH13	4.145	2.898	0.115	38.826	0.8	0.19	21.3	OK
2.2	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH13	MH14	4.047	2.809	0.159	38.829	0.6	0.22	21.2	OK
2.3	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH14	MH15	3.958	2.787	0.207	107.733	0.9	0.5	48.9	OK
2.4	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH15	MH16	3.949	2.728	0.231	131.729	1.0	0.64	62.0	OK
2.5	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH16	MH17	4.039	2.646	0.245	145.355	1.0	0.72	69.4	OK
2.6	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH17	MH18	4.164	2.557	0.232	165.699	1.2	0.83	80.7	OK
2.7	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH18	MH19	4.275	2.368	0.244	192.038	1.1	0.52	91.0	OK
2.8	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH19	MH20	4.319	2.273	0.252	192.000	1.1	0.52	91.1	OK
2.9	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH20	MH21	4.255	2.189	0.274	191.964	1.0	0.52	91.0	OK
2.10	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH21	MH22	4.129	2.130	0.299	216.292	1.0	0.59	104.1	OK
2.11	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH22	MH23	4.009	2.072	0.299	266.981	1.2	0.71	124.1	OK
2.12	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH23	MH24	3.992	1.996	0.270	266.932	1.3	0.71	124.2	OK
RJ24	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL24	MH12	4.219	4.063	0.020	6.171	0.0	0.12	8.7	OK
TD24	T25 Valencia: +0 %: T25 Valencia60	Pipe	JLL24	MH12	4.177	4.057	0.014	12.241	0.7	0.01	0.6	Surch arged
TD25	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL25	MH14	3.983	3.871	0.021	6.957	0.6	0	0.4	Surch arged
RJ25	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL25	MH14	3.973	3.879	0.022	3.515	0.0	0.1	7.2	OK
RP2-1	T25 Valencia: +0 %: T25 Valencia20	Pipe	PP1	MH14	3.928	3.552	0.056	19.054	1.4	0.14	10.4	OK
RP2-2	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP2	MH14	3.926	3.573	0.056	32.000	1.5	0.15	10.9	OK

RJ27	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL27	MH15	3.947	3.848	0.022	2.764	0.0	0.09	6.5	OK
TD27	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL27	MH15	3.953	3.840	0.011	8.141	0.6	0.01	0.4	Surch arged
RJ28	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL28	MH16	4.039	3.940	0.025	4.018	0.0	0.11	8.1	OK
TD28	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL28	MH16	4.060	3.929	0.011	8.148	0.6	0.01	0.4	Surch arged
RJ29	T25 Valencia: +0 %: T25 Valencia15	Pipe	JLL29	MH17	4.191	4.107	0.031	7.584	0.0	0.18	13.6	OK
TD29	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL29	MH17	4.209	4.088	0.010	6.141	0.5	0	0.3	Surch arged
RP3-1	T25 Valencia: +0 %: T25 Valencia20	Pipe	PP3-1	MH18	4.176	3.791	0.054	20.266	1.5	0.14	10.7	OK
TD30	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL30	MH21	4.217	4.080	0.012	10.901	0.6	0.01	0.5	Surch arged
RJ30	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL30	MH21	4.195	4.101	0.028	10.365	0.0	0.19	14.6	OK
TD31	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL31	MH22	4.042	3.931	0.012	8.917	0.6	0.01	0.5	Surch arged
RJ31	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL31	MH22	4.025	3.944	0.027	5.156	0.0	0.13	9.5	OK
RP3-2	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP3-2	MH22	4.035	3.684	0.057	34.859	1.5	0.15	11.6	OK
RP9-2	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP9-2	MH11	4.059	3.644	0.051	24.721	1.4	0.13	9.5	OK
3.1	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH28	MH29	3.624	2.347	0.124	89.106	1.0	0.26	28.1	OK
3.2	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH29	MH30	3.574	2.226	0.126	164.119	1.0	0.27	29.7	OK
3.3	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH30	MH31	3.664	2.101	0.140	164.084	0.8	0.27	29.7	OK
3.4	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH31	MH32	3.700	2.006	0.183	157.628	0.9	0.39	42.2	OK
3.5	T25 Valencia: +0 %: T25 Valencia45	Pipe	MH32	MH33	3.616	1.934	0.202	237.216	1.3	0.63	70.9	OK
RP10	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP10	MH28	3.641	3.235	0.053	27.017	1.4	0.13	9.8	OK
RJ45	T25 Valencia: +0 %: T25 Valencia45	Pipe	JLL45	MH28	3.728	3.471	0.039	15.861	0.0	0.23	17.6	OK
TD45	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL45	MH28	3.728	3.430	0.020	29.055	0.9	0.02	1.5	Surch arged
TD46	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL46	MH29	3.611	3.390	0.017	17.061	0.8	0.01	1.0	Surch arged
RJ46	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL46	MH29	3.621	3.435	0.017	1.315	0.0	0.03	2.3	OK

RJ48	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL48	MH32	3.566	3.486	0.056	36.453	0.0	0.44	33.5	Flood
TD48	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL48	MH32	3.568	3.444	0.019	15.507	0.8	0.02	1.2	Surch arged
RJ49	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL49	MH34	3.879	3.736	0.039	7.897	0.0	0.16	13.1	OK
TD49	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL49	MH34	3.909	3.722	0.014	14.142	0.7	0.01	0.6	Surch arged
RJ50	T25 Valencia: +0 %: T25 Valencia60	Pipe	JLL50	MH35	4.213	4.095	0.024	2.452	0.0	0.06	4.2	OK
TD50	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL50	MH35	4.223	4.095	0.017	23.022	0.8	0.01	1.0	Surch arged
RP11-1	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP11-1	MH31	3.643	3.170	0.051	26.038	1.4	0.12	9.4	OK
RP11-2	T25 Valencia: +0 %: T25 Valencia15	Pipe	PP11-2	MH31	3.619	3.140	0.044	6.669	1.3	0.09	7.0	OK
RP12	T25 Valencia: +0 %: T25 Valencia20	Pipe	PP12	MH33	3.650	3.195	0.056	29.806	1.6	0.14	11.6	OK
5.1	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH36	MH37	3.864	2.534	0.091	12.013	0.5	0.1	9.4	OK
5.2	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH37	MH38	3.714	2.476	0.123	41.546	0.8	0.22	21.6	OK
5.3	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH38	MH39	3.588	2.397	0.144	51.944	0.8	0.3	28.9	OK
5.4	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH39	MH40	3.589	2.319	0.173	62.729	0.8	0.38	36.4	OK
5.5	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH40	MH41	3.677	2.256	0.198	111.728	1.2	0.53	62.8	OK
5.6	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH41	MH42	3.637	2.118	0.196	123.278	1.3	0.6	71.7	OK
7.11	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH42	MH43	3.588	1.506	0.290	263.505	1.0	0.53	103.0	OK
6.1	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH45	MH46	4.164	2.081	0.080	33.152	1.2	0.12	20.3	OK
RJ32	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL32	MH36	3.828	3.721	0.024	4.830	0.0	0.12	9.3	OK
TD32	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL32	MH36	3.834	3.709	0.012	9.182	0.6	0.01	0.5	Surch arged
TD33	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL33	MH38	3.651	3.539	0.058	9.173	0.3	0.01	0.5	Surch arged
RJ33	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL33	MH38	3.646	3.548	0.018	3.215	0.0	0.1	7.3	OK
RP4	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP4	MH37	3.693	3.284	0.053	38.383	1.4	0.05	12.4	OK
TD34	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL34	MH39	3.573	3.465	0.042	9.180	0.6	0.01	0.5	Surch arged

RJ34	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL34	MH39	3.576	3.475	0.020	3.632	0.0	0.1	7.8	OK
TD35	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL35	MH40	3.673	3.462	0.012	12.165	0.6	0.01	0.5	Surch arged
RJ35	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL35	MH40	3.677	3.481	0.034	11.006	0.0	0.2	15.3	OK
RP5-1	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP5-1	MH40	3.656	3.231	0.059	37.181	1.5	0.15	11.6	OK
RP5-2	T25 Valencia: +0 %: T25 Valencia15	Pipe	PP5-2	MH41	3.601	3.138	0.054	9.369	1.4	0.13	9.6	OK
RP6-1	T25 Valencia: +0 %: T25 Valencia30	Pipe	PP6-1	MH43	3.679	3.217	0.071	28.922	1.1	0.23	11.2	OK
TD37	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL37	MH44	3.880	3.710	0.013	10.397	0.6	0.01	0.6	Surch arged
RJ37	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL37	MH44	3.856	3.731	0.026	8.695	0.0	0.17	12.5	OK
RJ38	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL38	MH45	4.142	3.999	0.026	5.438	0.0	0.13	9.7	OK
TD38	T25 Valencia: +0 %: T25 Valencia60	Pipe	JLL38	MH45	4.159	3.990	0.013	9.330	0.6	0.01	0.6	Surch arged
TD20	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL20	Manhole (46)	3.147	3.116	0.012	9.154	1.1	0.01	0.5	Surch arged
RJ20	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL20	Manhole (46)	3.152	3.123	0.019	3.833	0.0	0.08	5.9	OK
RJ21	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL21	Manhole (47)	3.283	3.186	0.021	1.553	0.0	0.06	4.4	OK
TD21	T25 Valencia: +0 %: T25 Valencia65	Pipe	JLL21	Manhole (47)	3.252	3.182	0.010	5.434	1.0	0	0.3	Surch arged
RJ19	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL19	Manhole (45)	3.239	3.148	0.018	3.833	0.0	0.08	5.9	OK
TD19	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL19	Manhole (45)	3.234	3.141	0.012	9.155	1.1	0.01	0.5	Surch arged
TD18	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL18	Manhole (44)	3.371	3.272	0.012	9.173	1.1	0.01	0.5	Surch arged
RJ18	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL18	Manhole (44)	3.376	3.283	0.023	4.080	0.0	0.11	8.4	OK
RJ17	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL17	Manhole (43)	3.571	3.462	0.023	3.833	0.0	0.08	5.9	OK
TD17	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL17	Manhole (43)	3.572	3.455	0.012	9.155	0.6	0.01	0.5	Surch arged
TD16	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL16	Manhole (42)	3.741	3.627	0.012	9.154	1.1	0.01	0.5	Surch arged
RJ16	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL16	Manhole (42)	3.728	3.634	0.015	3.833	0.0	0.08	5.9	OK
TD15	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL15	Manhole (41)	3.878	3.777	0.012	9.155	1.1	0.01	0.5	Surch arged

RJ15	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL15	Manhole (41)	3.877	3.784	0.019	3.833	0.0	0.08	5.9	OK
TD14	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL14	Manhole (40)	4.015	3.907	0.012	9.145	1.1	0.01	0.5	Surch arged
RJ14	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL14	Manhole (40)	4.025	3.912	0.018	2.455	0.0	0.06	4.8	OK
RJ13	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL13	Manhole (39)	3.938	3.858	0.015	1.868	0.0	0.05	3.6	OK
TD13	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL13	Manhole (39)	3.936	3.852	0.009	5.993	0.9	0	0.3	Surch arged
TD12	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL12	Manhole (38)	3.513	3.329	0.012	5.956	0.6	0.01	0.5	Surch arged
RJ12	T25 Valencia: +0 %: T25 Valencia15	Pipe	JLL12	Manhole (38)	3.498	3.342	0.025	3.369	0.0	0.1	7.8	OK
RJ23	T25 Valencia: +0 %: T25 Valencia15	Pipe	JLL23	Manhole (48)	3.722	3.538	0.025	8.813	0.0	0.2	15.0	OK
TD23	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL23	Manhole (48)	3.773	3.520	0.016	8.326	1.3	0.01	0.8	Surch arged
TD55	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL55	Manhole (38)	3.536	2.516	0.000	0.000	0.0	0	0.0	OK
RJ55	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL55	Manhole (38)	3.402	2.516	0.000	0.000	0.0	0	0.0	OK
TD56	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL56	Manhole (43)	3.683	2.724	0.000	0.000	0.0	0	0.0	OK
RJ56	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL56	Manhole (43)	3.641	2.724	0.000	0.000	0.0	0	0.0	OK
RJ57	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL57	Manhole (47)	3.389	2.691	0.000	0.000	0.0	0	0.0	OK
TD57	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL57	Manhole (47)	3.364	2.691	0.000	0.000	0.0	0	0.0	OK
RJ10	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL10	Manhole (28)	3.090	2.990	0.024	7.140	0.0	0.14	10.7	OK
TD10	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL10	Manhole (28)	3.073	2.976	0.009	7.936	1.1	0.01	0.5	Surch arged
RJ9	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL9	Manhole (28)	3.043	2.991	0.024	3.913	0.0	0.11	8.2	OK
TD9	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL9	Manhole (28)	3.029	2.981	0.012	9.213	0.6	0.01	0.5	Surch arged
RJ8	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL8	Manhole (29)	3.075	3.025	0.024	3.847	0.0	0.11	8.1	OK
TD8	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL8	Manhole (29)	3.090	3.015	0.012	9.178	1.1	0.01	0.5	Surch arged
RJ7	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL7	Manhole (30)	3.219	3.167	0.027	5.735	0.0	0.14	10.2	OK
TD7	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL7	Manhole (30)	3.225	3.154	0.012	9.188	1.1	0.01	0.5	Surch arged

RJ6	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL6	Manhole (31)	3.393	3.329	0.022	5.519	0.0	0.09	10.3	OK
TD6	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL6	Manhole (31)	3.390	3.316	0.012	10.468	1.1	0.01	0.5	Surch arged
TD5	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL5	Manhole (32)	3.551	3.475	0.012	9.178	1.1	0.01	0.5	Surch arged
RJ5	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL5	Manhole (32)	3.556	3.485	0.023	3.957	0.0	0.11	8.3	OK
RJ4	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL4	Manhole (33)	3.679	3.623	0.022	3.838	0.0	0.11	8.1	OK
TD4	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL4	Manhole (33)	3.687	3.612	0.012	9.178	1.1	0.01	0.5	Surch arged
RJ3	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL3	Manhole (34)	3.809	3.773	0.030	9.453	0.0	0.18	13.6	OK
TD3	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL3	Manhole (34)	3.824	3.756	0.012	9.203	1.1	0.01	0.5	Surch arged
RJ1	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL1	Manhole (36)	3.249	3.103	0.021	4.585	0.0	0.07	8.3	OK
TD1	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL1	Manhole (36)	3.201	3.091	0.010	7.918	1.1	0.01	0.5	Surch arged
RJ11	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL11	Manhole (26)	3.296	3.056	0.019	6.944	0.0	0.09	6.8	OK
TD11	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL11	Manhole (26)	3.283	3.033	0.018	21.675	0.8	0.01	1.1	Surch arged
RJ58	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL58	Manhole (27)	3.434	2.470	0.000	0.000	0.0	0	0.0	OK
TD58	T25 Valencia: +0 %: T25 Valencia10	Pipe	JLL58	Manhole (27)	3.115	2.470	0.000	0.000	0.0	0	0.0	OK
RJ61	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL61	Manhole (50)	3.500	3.251	0.017	3.065	0.0	0.07	5.2	OK
TD61	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL61	Manhole (50)	3.512	3.245	0.012	8.824	1.1	0.01	0.5	Surch arged
RJ60	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL60	Manhole (27)	3.222	3.107	0.021	4.327	0.0	0.08	5.8	OK
TD60	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL60	Manhole (27)	3.152	3.100	0.012	8.376	1.1	0.01	0.5	Surch arged
7.14	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH47	Vertido2	3.576	1.058	0.249	611.576	1.7	0.84	237.0	OK
RZB1	T25 Valencia: +0 %: T25 Valencia20	Pipe	ZBIO1	Manhole	2.691	2.591	0.078	44.368	0.0	0.3	80.9	OK
DZB1	T25 Valencia: +0 %: T25 Valencia90	Pipe	ZBIO1	Manhole	2.697	2.570	0.017	63.272	1.5	0.01	1.3	Surch arged
TDB26	T25 Valencia: +0 %: T25 Valencia90	Pipe	BJLL-26	Manhole (1)	2.756	2.299	0.024	34.870	0.9	0.03	2.0	Surch arged
RBB26	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-26	Manhole (1)	2.724	2.295	0.000	0.000	0.0	0	0.0	OK

7.10	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH57	MH42	3.546	1.534	0.161	228.896	1.0	0.39	37.6	OK
RJ59	T25 Valencia: +0 %: T25 Valencia45	Pipe	JLL59	Manhole (10)	3.131	3.041	0.019	6.248	0.0	0.13	9.9	OK
TD59	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL59	Manhole (10)	3.404	3.029	0.020	25.694	1.2	0.02	1.5	Surch arged
RB65	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL65	Manhole (11)	3.505	3.429	0.020	3.435	0.0	0.07	5.5	OK
TD65	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL65	Manhole (11)	3.509	3.418	0.011	4.966	1.0	0.01	0.4	Surch arged
RB64	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL64	Manhole (12)	3.490	3.377	0.025	2.498	0.0	0.07	5.3	OK
TD64	T25 Valencia: +0 %: T25 Valencia60	Pipe	JLL64	Manhole (12)	3.482	3.371	0.013	6.927	1.1	0.01	0.6	Surch arged
RB63	T25 Valencia: +0 %: T25 Valencia30	Pipe	JLL63	Manhole (13)	3.116	2.993	0.016	4.311	0.0	0.07	5.1	OK
TD63	T25 Valencia: +0 %: T25 Valencia60	Pipe	JLL63	Manhole (13)	3.115	2.987	0.013	6.938	1.1	0.01	0.6	Surch arged
TD62	T25 Valencia: +0 %: T25 Valencia60	Pipe	JLL62	Manhole (14)	2.768	2.691	0.013	6.944	1.1	0.01	0.6	Surch arged
RB62	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL62	Manhole (14)	2.748	2.698	0.023	2.709	0.0	0.07	5.5	OK
RJ26	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL26	MH15	3.933	3.836	0.021	2.755	0.0	0.09	6.5	OK
TD26	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL26	MH15	3.932	3.828	0.011	8.150	0.6	0.01	0.4	Surch arged
7.1	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH48	MH49	3.700	2.259	0.020	9.138	0.3	0.01	0.6	OK
7.2	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH49	MH50	3.700	2.159	0.019	9.138	0.3	0.01	0.6	OK
7.3	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH50	MH51	3.700	2.059	0.050	9.138	0.2	0.01	0.6	OK
7.4	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH51	MH52	3.650	2.022	0.079	69.381	0.7	0.12	11.6	OK
7.5	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH52	MH53	3.600	1.920	0.097	69.356	0.6	0.12	11.5	OK
7.8	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH55	MH56	3.600	1.674	0.117	120.635	0.8	0.23	22.4	OK
7.9	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH56	MH57	3.600	1.582	0.132	120.632	0.7	0.23	22.4	OK
8.6	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH63	MH64	3.700	1.672	0.042	35.111	0.5	0.03	3.4	OK
RBB8	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-8	MH63	3.717	3.367	0.000	0.000	0.0	0	0.0	OK
TDB8	T25 Valencia: +0 %: T25 Valencia60	Pipe	BJLL-8	MH63	3.727	3.371	0.020	11.243	0.9	0.02	1.4	Surch arged

RBB7	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-7	MH57	3.629	3.211	0.000	0.000	0.0	0	0.0	OK
TDB7	T25 Valencia: +0 %: T25 Valencia65	Pipe	BJLL-7	MH57	3.637	2.946	0.016	5.550	0.7	0.01	0.9	Surch arged
RBB14	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-14	Manhole (9)	3.128	2.567	0.000	0.000	0.0	0	0.0	OK
TDB14	T25 Valencia: +0 %: T25 Valencia60	Pipe	BJLL-14	Manhole (9)	3.118	2.569	0.021	15.349	0.9	0.02	1.6	Surch arged
RBB18	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-18	Manhole (2)	2.521	2.138	0.000	0.000	0.0	0	0.0	OK
TDB18	T25 Valencia: +0 %: T25 Valencia65	Pipe	BJLL-18	Manhole (2)	2.509	2.137	0.022	18.416	0.9	0.02	1.7	Surch arged
RBB17	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-17	Manhole (3)	2.696	2.176	0.000	0.000	0.0	0	0.0	OK
TDB17	T25 Valencia: +0 %: T25 Valencia90	Pipe	BJLL-17	Manhole (3)	2.722	2.178	0.017	8.363	0.8	0.01	1.0	Surch arged
TDB22	T25 Valencia: +0 %: T25 Valencia90	Pipe	BJLL-22	Manhole (4)	3.623	2.452	0.025	45.531	0.9	0.03	2.1	Surch arged
RBB22	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-22	Manhole (4)	3.616	2.426	0.000	0.000	0.0	0	0.0	OK
TDB25	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-25	Manhole (5)	3.969	3.484	0.019	17.724	0.8	0.02	1.3	Surch arged
RBB25	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-25	Manhole (5)	3.969	3.473	0.000	0.000	0.0	0	0.0	OK
TDB24	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-24	Manhole (6)	3.356	2.863	0.019	21.409	0.8	0.02	1.3	Surch arged
RBB24	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-24	Manhole (6)	3.356	2.832	0.000	0.000	0.0	0	0.0	OK
RBB13	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-13	Manhole (15)	3.408	1.963	0.000	0.000	0.0	0	0.0	OK
TDB13	T25 Valencia: +0 %: T25 Valencia45	Pipe	BJLL-13	Manhole (15)	3.386	1.968	0.024	19.141	1.0	0.03	2.1	Surch arged
RBB21	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-21	Manhole (16)	2.896	2.273	0.000	0.000	0.0	0	0.0	OK
TDB21	T25 Valencia: +0 %: T25 Valencia90	Pipe	BJLL-21	Manhole (16)	2.994	2.290	0.024	41.922	0.9	0.03	2.0	Surch arged
RBB23	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-23	Manhole (17)	3.179	2.324	0.000	0.000	0.0	0	0.0	OK
TDB23	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-23	Manhole (17)	2.957	2.339	0.018	22.543	0.8	0.02	1.2	Surch arged
RBB12	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-12	Manhole (18)	3.567	3.181	0.000	0.000	0.0	0	0.0	Surch arged
TDB12	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-12	Manhole (18)	3.567	3.210	0.016	10.201	0.7	0.01	0.8	Surch arged
9.1	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH65	MH66	2.850	1.406	0.026	18.635	0.4	0.01	1.3	OK

10.6	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH66	Manhole (19)	3.044	0.763	0.047	46.550	0.5	0.04	4.1	OK
RBB19	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-19	MH65	2.945	2.329	0.000	0.000	0.0	0	0.0	OK
TDB19	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-19	MH65	2.930	2.355	0.023	18.639	0.7	0.02	1.3	Surch arged
RBB16	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-16	MH69	2.760	2.193	0.000	0.000	0.0	0	0.0	OK
TDB16	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-16	MH69	2.738	2.249	0.018	19.406	0.8	0.01	1.1	Surch arged
RBB20	T25 Valencia: +0 %: T25 Valencia60	Pipe	BJLL-20	MH67	2.752	2.347	0.022	14.196	0.9	0.02	1.7	Surch arged
TDB20	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-20	MH67	2.745	2.344	0.000	0.000	0.0	0	0.0	OK
RBB2	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-2	Manhole (24)	3.194	2.838	0.000	0.000	0.0	0	0.0	OK
TDB2	T25 Valencia: +0 %: T25 Valencia90	Pipe	BJLL-2	Manhole (24)	3.216	2.850	0.021	20.968	0.9	0.02	1.6	Surch arged
RBB27	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-27	Manhole (25)	3.573	3.011	0.000	0.000	0.0	0	0.0	OK
TDB27	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-27	Manhole (25)	3.569	3.011	0.000	0.000	0.0	0	0.0	OK
RBB1	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-1	Manhole (37)	3.683	2.911	0.000	0.000	0.0	0	0.0	OK
TDB1	T25 Valencia: +0 %: T25 Valencia45	Pipe	BJLL-1	Manhole (37)	3.674	2.912	0.022	13.682	0.9	0.02	1.8	Surch arged
RBB11	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-11	Manhole (49)	2.839	2.329	0.000	0.000	0.0	0	0.0	OK
TDB11	T25 Valencia: +0 %: T25 Valencia90	Pipe	BJLL-11	Manhole (49)	2.836	2.358	0.021	37.030	0.9	0.02	1.7	Surch arged
RBB15	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-15	Manhole (8)	2.167	2.185	0.000	0.000	0.0	0	0.0	OK
TDB15	T25 Valencia: +0 %: T25 Valencia90	Pipe	BJLL-15	Manhole (8)	2.172	2.227	0.020	30.507	0.7	0.02	1.1	Surch arged
10.1	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH67	MH68	2.759	1.226	0.031	14.188	0.4	0.02	1.7	OK
10.2	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH68	MH69	2.672	1.125	0.035	14.172	0.3	0.02	1.7	OK
10.3	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH69	MH70	2.896	1.037	0.039	30.876	0.5	0.03	2.8	OK
10.4	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH70	MH71	2.948	0.937	0.039	30.855	0.5	0.03	2.8	OK
10.5	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH71	MH66	3.010	0.839	0.043	30.831	0.4	0.03	2.8	OK
RJ2	T25 Valencia: +0 %: T25 Valencia15	Pipe	JLL2	Manhole (36)	3.652	3.411	0.018	4.575	0.0	0.13	10.2	OK

TD2	T25 Valencia: +0 %: T25 Valencia90	Pipe	JLL2	Manhole (36)	3.607	3.396	0.012	7.570	0.6	0.01	0.5	Surch arged
RJ22	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL22	Manhole (38)	3.577	3.448	0.031	15.185	0.0	0.28	21.1	Surch arged
TD22	T25 Valencia: +0 %: T25 Valencia60	Pipe	JLL22	Manhole (38)	3.605	3.431	0.016	15.166	0.7	0.01	0.9	Surch arged
RP6-2	T25 Valencia: +0 %: T25 Valencia20	Pipe	PP6-2	MH45	4.121	3.618	0.058	19.877	1.4	0.14	10.5	OK
7.6	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH53	MH54	3.550	1.857	0.116	120.658	0.8	0.23	22.4	OK
7.7	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH54	MH55	3.500	1.758	0.116	120.644	0.8	0.23	22.4	OK
TDB3	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-3	MH48	3.363	3.227	0.017	9.138	0.5	0.01	0.6	Surch arged
RBB3	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-3	MH48	3.357	3.156	0.000	0.000	0.0	0	0.0	OK
RBB4	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-4	MH51	3.254	3.420	0.030	10.968	0.0	0.1	10.2	OK
TDB4	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-4	MH51	3.259	3.255	0.015	10.286	0.7	0.01	0.8	Surch arged
TDB5	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-5	MH53	3.336	3.322	0.012	25.407	0.7	0.01	0.5	Surch arged
RBB5	T25 Valencia: +0 %: T25 Valencia30	Pipe	BJLL-5	MH53	3.335	3.331	0.043	9.759	0.0	0.13	14.2	OK
RBB10	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-10	MH58	3.163	2.925	0.000	0.000	0.0	0	0.0	OK
TDB10	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-10	MH58	3.170	2.943	0.020	13.939	0.6	0.01	1.0	Surch arged
8.1	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH58	MH59	3.400	2.209	0.023	13.938	0.4	0.01	1.0	OK
8.2	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH59	MH60	3.400	2.097	0.023	13.935	0.4	0.01	1.0	OK
8.3	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH60	MH61	3.303	1.984	0.028	13.928	0.3	0.01	1.0	OK
8.4	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH61	MH62	3.503	1.880	0.032	29.252	0.5	0.02	2.0	OK
8.5	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH62	MH63	3.574	1.769	0.037	29.241	0.4	0.02	2.0	OK
RBB9	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-9	MH61	3.411	3.075	0.000	0.000	0.0	0	0.0	OK
TDB9	T25 Valencia: +0 %: T25 Valencia75	Pipe	BJLL-9	MH61	3.425	3.094	0.017	15.327	0.8	0.01	1.0	Surch arged
8.7	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH64	MH57	3.650	1.559	0.096	35.060	0.4	0.03	3.4	OK
RJ39	T25 Valencia: +0 %: T25 Valencia45	Pipe	JLL39	MH1	4.430	4.302	0.029	6.543	0.0	0.12	8.9	OK

TD39	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL39	MH1	4.432	4.299	0.017	27.902	0.7	0.01	1.0	Surch arged
6.2	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH46	MH44	3.960	1.768	0.092	33.147	1.1	0.12	20.4	OK
4.1	T25 Valencia: +0 %: T25 Valencia65	Pipe	MH35	MH 35.1	4.210	2.683	0.036	24.715	1.0	0.02	5.1	OK
4.2	T25 Valencia: +0 %: T25 Valencia75	Pipe	MH 35.1	MH34	4.006	2.182	0.045	26.390	0.7	0.02	5.1	OK
6.3	T25 Valencia: +0 %: T25 Valencia20	Pipe	MH44	MH43	3.770	1.553	0.145	49.608	1.0	0.19	33.2	OK
4.3	T25 Valencia: +0 %: T25 Valencia60	Pipe	MH34	MH33	3.869	1.874	0.056	59.057	1.5	0.06	14.6	OK
7.12	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH43	MH33	3.635	1.455	0.284	356.935	1.5	0.74	145.1	OK
7.13	T25 Valencia: +0 %: T25 Valencia30	Pipe	MH33	MH47	3.667	1.228	0.270	611.815	1.6	0.84	236.6	OK
RJ36	T25 Valencia: +0 %: T25 Valencia20	Pipe	JLL36	MH57	3.559	3.499	0.071	15.729	0.0	0.25	18.6	OK
TD36	T25 Valencia: +0 %: T25 Valencia75	Pipe	JLL36	MH57	3.572	3.473	0.012	11.458	0.6	0.01	0.5	Surch arged
RBB6	T25 Valencia: +0 %: T25 Valencia10	Pipe	BJLL-6	MH57	3.599	3.071	0.000	0.000	0.0	0	0.0	OK
TDB6	T25 Valencia: +0 %: T25 Valencia65	Pipe	BJLL-6	MH57	3.602	3.081	0.018	8.101	0.8	0.02	1.1	Surch arged

Proyecto:	Date:		
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025		
	Designed by: FMA	Checked by: GGA	Approved By:
Report Details: Type: Phase Management Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia		

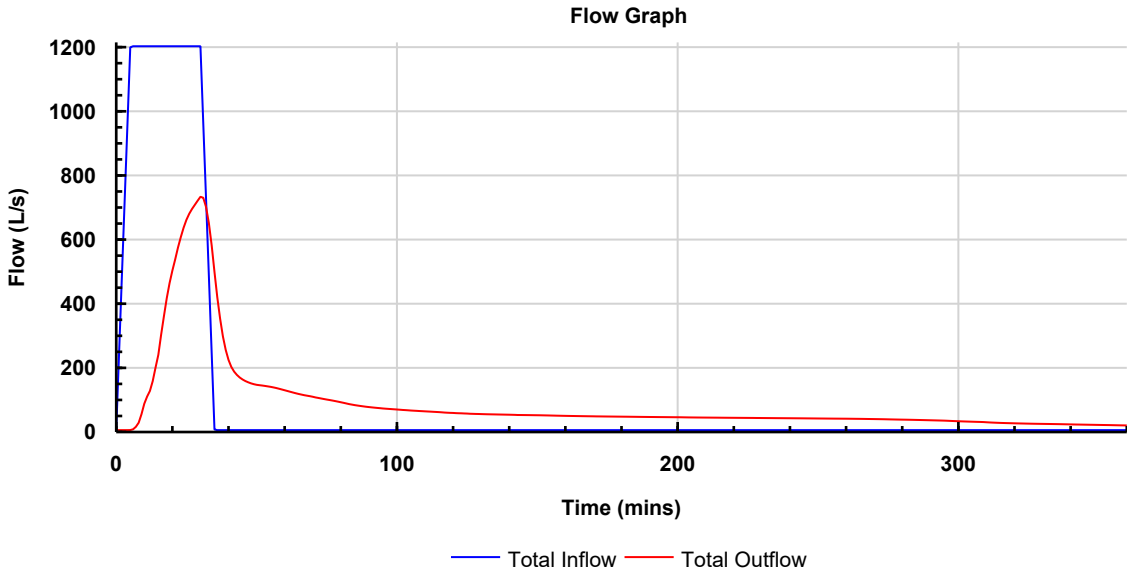
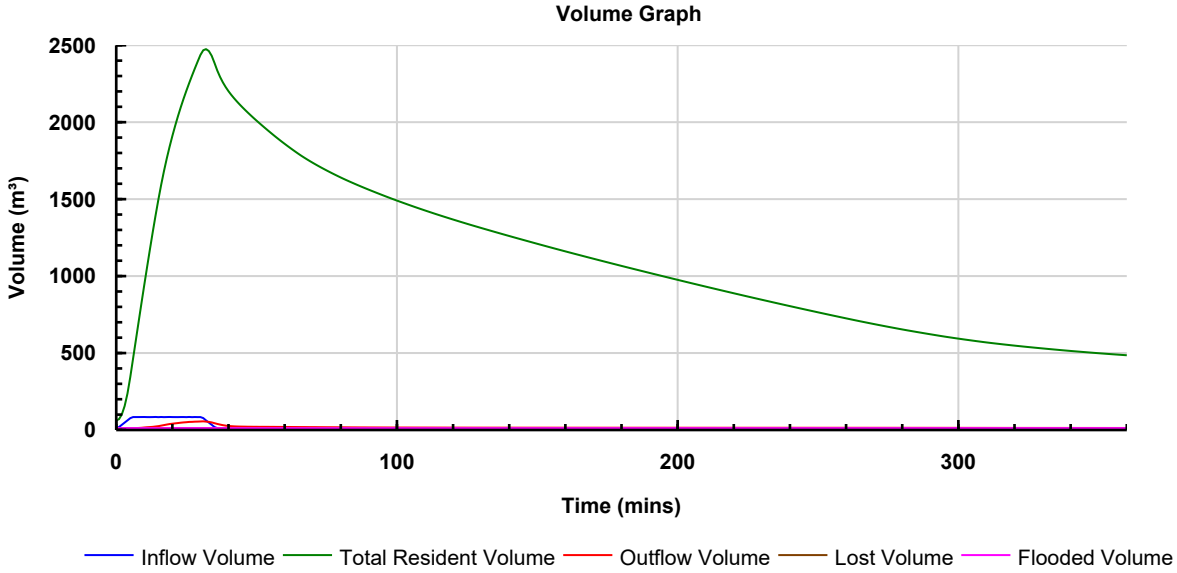
Grupo TYPSA

Fase
T25 Valencia: Increase Rainfall (%): +0: T25 Valencia30

Tables

Name	Max. Inflow (L/s)	Total Inflow Volume (m³)	Max. Outflow (L/s)	Total Outflow Volume (m³)
Vertido1			205.5	478.303
Vertido2			237.0	611.576
Manhole (26)			1.1	21.675
Manhole (27)			6.0	11.067
Manhole (28)			17.6	31.835
Manhole (29)			8.0	14.409
Manhole (30)			9.3	16.875
Manhole (31)			9.8	17.825
Manhole (32)			8.0	14.555
Manhole (33)			8.0	14.394
Manhole (34)			12.0	21.716
Manhole (36)			16.7	30.263
Manhole (38)			26.0	47.636
Manhole (39)			3.8	6.833
Manhole (40)			5.0	9.876
Manhole (41)			6.1	11.262
Manhole (42)			6.1	11.262
Manhole (43)			6.1	11.262
Manhole (44)			8.1	14.714
Manhole (45)			6.1	11.262
Manhole (46)			6.1	11.262
Manhole (47)			4.5	8.129
Manhole (48)			12.5	22.914
Manhole (50)			5.5	10.238
Manhole			70.2	97.279
Manhole (1)			1.9	13.387
Manhole (8)			1.1	12.233
Manhole (9)			1.5	8.842
Manhole (10)			4.6	27.028
Manhole (11)			5.0	9.079
Manhole (12)			5.5	10.366
Manhole (13)			5.4	10.095
Manhole (14)			5.7	10.652
Manhole (2)			1.6	10.350
Manhole (3)			1.0	4.680
Manhole (4)			2.0	15.894
Manhole (5)			1.3	9.290
Manhole (6)			1.3	11.466
Manhole (15)			1.9	13.483
Manhole (16)			2.0	16.992
Manhole (17)			1.2	10.255
Manhole (18)			0.8	5.694
Manhole (19)			3.8	28.112
Manhole (24)			1.1	6.689
Manhole (25)			0.0	0.000
Manhole (37)			1.6	9.350
Manhole (49)			1.7	14.605
TOTAL	1202.6	2164.565	731.2	1816.966

Graphs

Proyecto:	Date:		
Proyecto de ejecución de las obras de urbanización del Sector Grao (València)	26/06/2025		
	Designed by: FMA	Checked by: GGA	Approved By:
Report Details: Type: Phase Management Storm Phase: Fase	Dirección de la empresa: C. Botiguers 5, 5a P.E. Táctica Paterna, Valencia		

Grupo TYPSA